Determine header size from FBC 2001, Tables 2308.3 A, B, & C, or 2308.5.

.oad Bearing Header Sizing Methods (BY BUILDER)

Jack Studs and King Studs (BY BUILDER)

Header Uplift Connections (BY BUILDER)

dividing by the length of the header.

5. Use one jack stud for every 3000 lb vertical load.

connection) and stud to foundation (bottom connection).

< 800 End nail or toe nail

w/6-.131"x3.25"

LSTA12, 10-10d

Option # Uplift, lb. | Top Connector

plift greater than 3885 lb requires engineering design

Supporting Roof+Ceiling (20psf+20psf)

NOTES: NJ = Number of jack studs

width is measured perpendicular to

the ridge. For widths between those

Spans are based on uniform loads on

shown, spans may be interpolated.

required to support each end. Building

2. Use supplier pubished data or Southern pine span tables.

3. For engineered lumber beams have suppliers engineer size beam.

Lookup jack studs from FBC 2001, Tables 2308.3 A, B, & C, or 2308.5.

6. Total king plus jack studs = studs needed to be there if no opening was there.

. Calculate the uplift at each end of the header by summing the moments of all truss uplifts and

LSTA18, 14-10d 1055 LTT20B, 10-16d ½" AB (2) LSTA18, 14-10d 2110 LTT131, 18-10d½" x10" AB

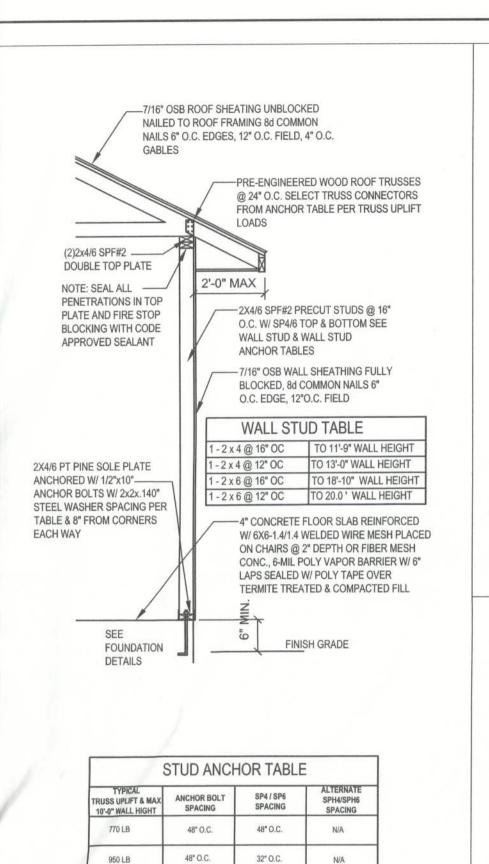
< 3885 (3) LSTA18, 14-10d 3480 HTT16, 18-16d, 18-16d,

Bottom Connector

(2) SP4, 6-10dx11/2", 1/2" AB

Header Spans Building Width / Truss Span (ft)

8. Select header connections from table below or mfg. catalog to connect header to stud (top





16" O.C.

16" O.C.

32\* O.C.

16" O.C.

STUD PACK

32" O.C.

24" O.C.

TI31 W/ 5/8" X 7

WEDGE ANCHOR

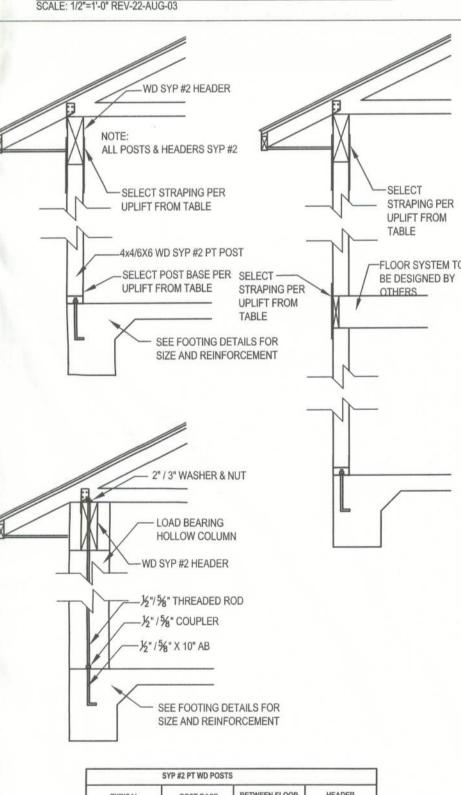
NOTE: SP2 TOP & SP1 BOTTOM ALTERNATE FOR SP4/6

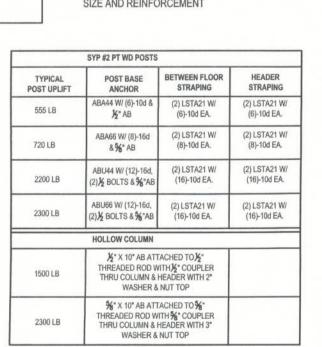
MINIMUM ANCHOR BOLT SPACING FOR WALLS WITH A HEIGHT

GREATER THAN 10'-0" AND LESS THAN 14'-0" SHALL BE 32" O.C

1270 LB

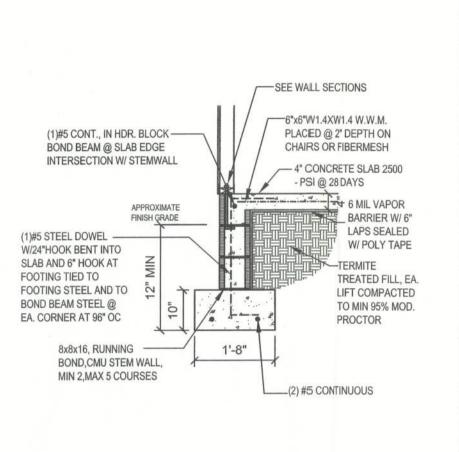
1500 LB





W12 - PORCH HEADER ANCHORS

SCALE: N.T.S. REV-18-JUL-03



F1 - STEM WALL FOUNDATION

95% MOD. PROICTOR

SYP #2 | HEADER

(4) #10X2 1/2" FULL THREAD WOOD

MIN. 3/8" EDGE SPACING PER NDS

- (4) #12X3/4"SS TEK SCREWS

- 1/8"X3"X3"X1 1/2" ALUMINUM

BRACKET W/FLANGE WINGS

- 3"X3"X.092" ALUMINUM COLUMN, 6053-T6

- 3"X3"X.092" ALUMINUM COLUMN, 6053-T6

1/8"X3"X3"X1 1/2" ALUMINUM BRACKET

- 1/2" WASHER, 410SS

- (4) #12X3/4"SS TEK SCREWS

- 1/2" THD R0D, G90 OR HDG w/ SIMPSON AT EPOXY

- 3"X3"X.092" ALUMINUM COLUMN, 6053-T6

(2) 1/4"X(2 1/2" TAPCON, 410SS OR G95 w/

Garage width, 24' Main house width, 3

ain house width, 4

Bonus Room, above garage

Deflection limits: TL=L/240, LL=L/180

SS WASHERS 2 1/4" MIN. EMBEDMENT

(PER MIAMIDADE NOA 03-0114.03)

(1) #5 CONTINUOUS IN STEMWALL

INTERSECTION w/ SLAB

MONOLITHICW/ STEM WALL

4" CONCRETE SLAB

W44 - ALUMINUM PORCH POST & HEADER ANCHORS

(4) #12X3/4"SS TEK SCREWS

SCREWS (MIN. 2" THREAD PENETRATION

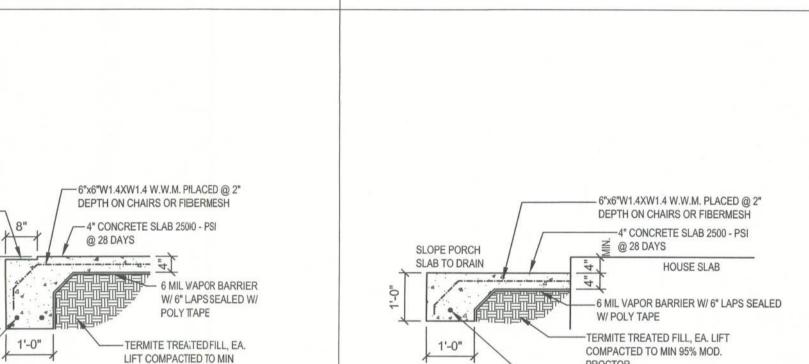
F8 - GARAGE DOOR POCKET

GARAGE DOOR -

(2) #5 CONTINUOUS -

1 3/4" MIN. EDGE SPACING

SCALE: N.T.S. REV-09-MAY-04



F2 - PORCH SLAB SCALE: 1/2"=1'-0" REV-22-AUG-03

Header Span vs Load

3 4 5 6 7 8 9 10 11 12 13 14

Duration factor, Cd = 1.25, applied to Fb and Fv. (No increase to E or Fc, for duration of load.)

2x headers are SYP#2 with OSB flitch spacer and (2) 12dS 16°OC, (strength increased 5% for OSB)

3.5° x 14° GLB is Anthony Power Header, 2600 Fb, 1.9 E, or GP (2)1.75x14 LVL, 2850 Fb, 2.0 E

3.5° x 12° LVL is Blue Linx - GP Lam, (2) 1.75° x 11.78° LVL, 2900 Fb, 2.0 E, 285 Fv.

Shear strength is increased 50% for minimal splits and checks headers cut to size on site.

Deflection has not been adjusted for creep due to long term loading, Kcr = 1.0.

Minimum bearing for SYP header, Fc = 565psi, 2500 lb per jack stud. (For SPF plate, Fc = 425psi, 2200 lb p

Header Clear Span Between Supports (ft)

Half of 7" truss span + 24" overhang Half of 8" truss span + 24" overhang

Half of 20' truss span + 24" overhang Half of 24' truss span + 24" overhang

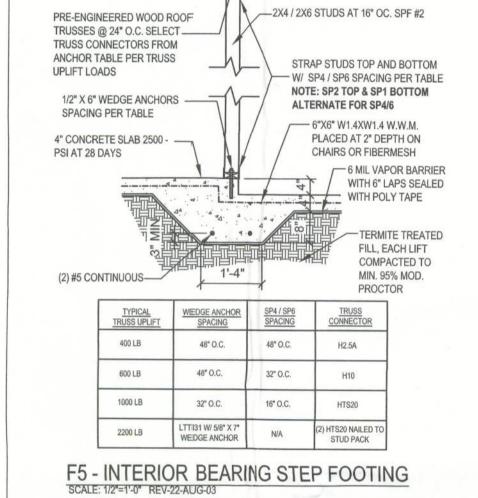
880 Half of 40' truss span + 24" overhang 1280 Half of 60' truss span + 24" overhang 1025 Half of 24' truss span and 14' bonus room

W71 - HEADER SPANS FOR ROOF/CEILING LOAD

Half of 32' truss span + 24" overhang

PROCTOR

-(1) #5 CONTINUOUS



PRE-ENGINEERED WOOD ROOF

TRUSSES @ 24" O.C. SELECT \_

TRUSS CONNECTORS FROM

ANCHOR TABLE PER TRUSS

SPACING PER TABLE

4" CONCRETE SLAB 2500 - -

(2) #5 CONTINUOUS-

600 LB

1000 LB

418° O.C.

48" O.C.

32" O.C.

WEDGIE ANCHOR

48" O.C.

32" O.C.

16" O.C.

F4 - INTERIOR BEARING FOOTING

1/2" X 6" WEDGE ANCHORS -

**UPLIFT LOADS** 

PSI AT 28 DAYS

—POST BASE SEE W12

WD PT POST -

FINISH GRADE

(1)#5 CONT., IN HDR. BLOCK \_\_

BOND BEAM @ SLAB EDGE

INTERSECTION W/

(1)#5 STEEL DOWEL -

SLAB AND 6" HOOK AT

FOOTING TIED TO

CORNER AT 96" OC

W/24"HOOK BENT INTO

FOOTING STEEL AND TO

8x8x16, RUNNING

BOND, CMU STEM

WALL, MIN 1, MAX 5

COURSES

BOND BEAM STEEL @ EA

STEMWALL

6"x6"W1.4XW1.4 W.W.M.

PLACED @ 2" DEPTH ON

CHAIRS OR FIBERMESH

- PSI @ 28 DAYS

— 4" CONCRETE SLAB 2500

HOUSE SLAB

**POLY TAPE** 

- 6 MIL VAPOR BARRIER

W/ 6" LAPS SEALED W/

TERMITE TREATED FILE

EA. LIFT COMPACTED

TO MIN 95% MOD.

20"x10" POURED

\_CONCRETE STRIP

PROCTOR

FOOTING

\_\_ (2) #5 CONTINUOUS

1'-8"

F10 - STEM WALL PORCH FOOTING

----- 2X4 / 2X6 STUDS AT 16" OC. SPF #2

STRAP STUDS TOP AND BOTTOM W/

SP4 / SP6 SPACING PER TABLE

NOTE: SP2 TOP & SP1 BOTTOM

-6"X6" W1.4XW1.4 W.W.M.

PLACED AT 2" DEPTH ON

CHAIRS OR FIBERMESH

WITH 6" LAPS SEALED

6 MIL VAPOR BARRIER

-WITH POLY TAPE

ERMITE TREATED FILL

EACH LIFT COMPACTED

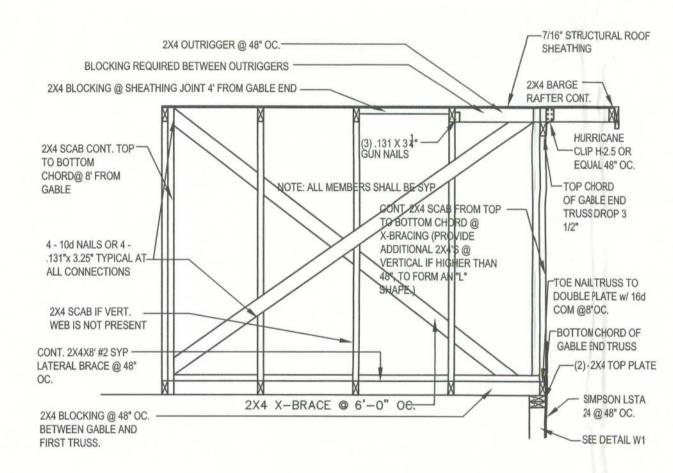
TO MIN. 95% MOD.

PROCTOR

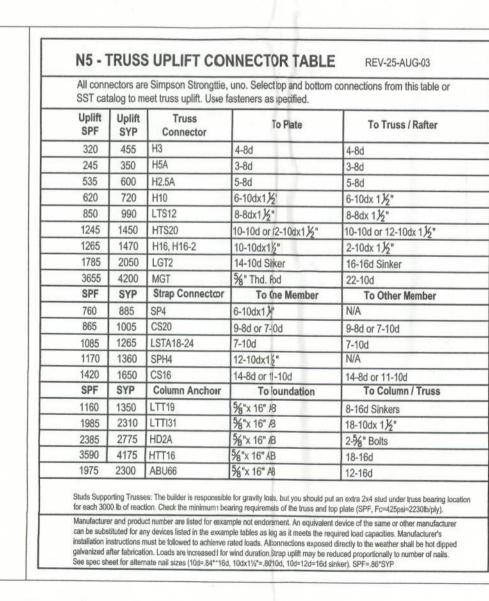
H2.5A

HTS20

**ALTERNATE FOR SP4/6** 



W10 - TYPICAL GABLE END (X-BRACING)



	N4-WIND LOAD DESIGN DATA		engineer of record for the trusses and did not design the trusses or delegate to the truss designer.	ı
	(Wind loads are per FBC 2001, Section 1606.2 for enclosed simple diaphragm buildings with mean roof height less than 60' or the least horizontal dimension; not sited on the upper half of an unobstructed 60' high hill with >10% slope.)		BUILDER'S RESPONSIBILITY: The builder and owner are responsible for the following, which are specifically not part of the wind load engineer's scope of work.	
	Basic Wind Speed	110 MPH	* Confirm that the foundation design & site conditions meet gravity load requirements (assume 1000 PSF bearing	П
	Wind Exposure	В	capacity unless visual observation or soils test proves otherwise	L
Ш	Wind Importance Factor	1.0	* Provide materials and construction techniques, which comply with FBC 2001 requirements for the stated wind velocity and design pressures.	ı
П	Building Category	II	* Provide a continuous load path from roof to foundation. If you believe the plan omits a continuous load path	L
	Internal pressure Coefficient	N/A (Enclosed)	connection, call the wind load engineer immediately.	ı
	Building not in the high velocity hurricane zone		* Verify the truss engineering includes truss design, placement plans, temporary and permanent bracing details, truss-to-truss connections, and load reactions for all bearing locations.	L
П	Building not in the wind-borne debris region		* Select uplift connections, walls, columns, and footings based on truss engineering bearing locations and reactions;	I
	Mean Roof Height	< 30 ft	including interior bearing walls.	П
	Roof Angle	10-45 degrees	* Size headers for gravity loads; headers sized by the builder for gravity loads will also satisfy wind loads.	H
	Components And Cladding Wind Pressures (FBC Table1606.2 B&C)		DOCUMENT CONTROL and PRIORITY: Structural requirements on S-1 control unless the building code or	ı
	2 2 2 2 5	Transverse   Longitudinal   100	architectural sheets have more stringent requirements. Non-structural requirements on architectural sheets control. Specific requirements take precedence over general requirements. Revision control is by the latest signature date and is the responsibility of the builder.  COPYRIGHTS AND PROPERTY RIGHTS: Mark Disosway, P.E. hereby expressly reserves its common law copyrights and property right in these instruments of service. This document is not to be reproduced, altered or copied in any form or manner without first the express written permission and consent of Mark Disosway.	
	3 3 3 3	Required 34.5' 31.5' Actual 66.5' 59.2' All exterior walls are type II shear walls ACTUAL SHEAR WALL length is the total	DIMENSIONS: Stated dimensions supercede scaled dimensions. Refer all questions to Mark Disosway, P.E. for resolution. Do not proceed wiithout clarification.	I
	3 5 2 4 5 5 5 5 5 7	of all wall segments with full height sheathing and width to height ratio greater than 1: 3.5 (plus special shear wall segments if noted.) REQUIRED SHEAR WALL length is from WFCM-2001, table 3.17A & 3.17B with table 3.17E adjustment for type II shear wall (or equivalent calculation) REV-27-Jun-03	WINDLOAID ENGINEER: Mark Disosway, PE No.53915  CERTIFICATION: The attached plans and "Windload Engineering", sheet S-1, comply with FBC 2001, Section 1606 wind loads, to the best of my knowledge.  LIMITATION: This design is valid for one building, at specified location. This drawing is not valid for construction unless raised seal is affixed.	

N4-WIND LOAD DESIGN DATA

T SIZED BY SUPPLIER OR ENGINEER -CONTINUE SPACING OF HEADER TO HEADER STUD SP4/6 STUD STRAPS OVER CONNECT TOP OF WITH (6) .131 X 3 1/4 HEADER STUDS / JACK STUDS TO HEADER PER TRUSS UPLIFT 1/2"x10" ANCHOR BOLTS W/ 2x2x.140\* STEEL W/ 2x2x.140\* STEEL TYPICAL STRAPPING WALL SECTIONS (SEE TABLE FOR SPECIFIC OPTION #2 OPTION #3 EXAMPLES BASED ON TRUSS UPLIFT) NOTE: Uplift, lb. < 1500 Uplift, lb. < 1760 ANCHOR BOLTS MAY BE LOCATED AT EITHER SIDE OF KING STUDS. PLATE MUST BE CONT. BETWEEN BOLT AND KING STUDS — CONNECT HEADER SUD PACK TO FOUNDATION PER TRUSS UPLIFT (SEE HEADER CONNECTION TABLE) W13-TYPICAL HEADER SIZING & STRAPING DETAIL **OPTION #4** OPTION #5 SCALE: N.T.S. REV 22-AUG-03 Uplift, lb. < 2500 Uplift, lb. < 3885

## COVERED LANAI BEDROOM 12 10' CLG NOOK 10' CLG 42° 4 642° GREAT ROOM lo' CLG KITCHEN MASTER SUITE STUDY 10' CLG 10' CLG ENTRY (3) 385CI (3) 383C TRANS 12) 2650 TRAHS 521 @ 18\* AFF 2 CAR GARAGE II' CLG AREA SUMMARY GARAGE AREA 481 SF LANAI AREA 172 SP ENTRY AREA 58 SF TOTAL AREA 2640 SF

FLOOR PLAN

## **N2-GENERAL NOTES:**

CONCRETE: MINIMUM COMPRESSIVE STRENGTH OF CONCRETE AT 28 DAYS SHALL BE F'C = 3000 PSI. WHERE EXCESS WATER IS ADDED TO THE CONCRETE SO THAT ITS SERVICABILITY IS DEGRADED, THE ATTAINMENT OF REQUIRED STRENGTH SHALL NOT RELEASE THE CONTRACTOR FROM PROVIDING SUCH MODIFICATIONS AS MAY BE REQUIRED BY THE ENGINEER TO PROVIDE A SERVICEABLE MEMBER OR SURFACE. ALL CONCRETE SHALL BE VIBRATED. NO REPAIR OR RUBBING OF CONCRETE SURFACES SHALL BE MADE PRIOR TO INSPECTION BY AND APPROVAL OF THE ENGINEER, OWNER OR HIS REPRESENTATIVE

WELDED WIRE REINFORCED SLAB: 6" x 6" W1.4 x W1.4, FB = 85KSI, WELDED WIRE REINFORCEMENT FABRIC (W.W.M.) CONFORMING TO ASTM A185; LOCATED IN MIDDLE OF THE SLAB; SUPPORTED WITH APPROVED MATERIALS OR SUPPORTS AT SPACINGS NOT TO EXCEED 3'.

FIBER CONCRETE SLAB: CONCRETE SLABS ON GROUND CONTAINING SYNTHETIC FIBER REINFORCEMENT. FIBER LENGTHS SHALL BE 1/2 INCH TO 2 INCHES IN LENGTH. DOSAGE AMOUNTS SHALL BE FROM 0.75 TO 1.5 POUNDS PER CUBIC YARD IN ACCORDANCE WITH THE MANUFACTURER'S RECOMMENDATIONS. SYNTHETIC FIBERS SHALL COMPLY WITH ASTM C 1116. THE MANUFACTURER OR SUPPLIER SHALL PROVIDE CERTIFICATION OF COMPLIANCE WITH ASTM C 1116 WHEN REQUESTED BY THE BUILDING OFFICIAL.

CONTROL JOINTS: WHERE SPECIFIED, SAWN CONTROL JOINTS IN SLAB-ON-GRADE SHALL BE CUT IN ACCORDANCE WITH ACI 302, JOINTS SHALL BE CUT WITHIN 12 HOURS OF SLAB PLACEMENT, THE LENGTH WIDTH RATIOS OF SLAB AREAS SHALL NOT EXCEED 1.5 AND TYPICAL SPACING OF CUTS TO BE 12FT. DO NOT CUT WWM OR REINFORCING STEEL. (RECOMMENDED LOCATION OF CONTROL JOINTS IS SUBJECT TO OWNER AND CONTRACTOR'S APPROVAL. THE CONTROL JOINTS ARE NOT INTENDED TO PREVENT CRACKS BUT RATHER TO ENCOURAGE THE SLAB TO CRACK ON A GIVEN LINE.)

REBAR: ASTM A 615, GRADE 40, DEFORMED BARS, FY = 40 KSI. ALL LAPS SPLICES 40 \* DB (25" FOR #5 BARS); UNO. ALL REINFORCEMENT SHALL BE DETAILED AND PLACED IN ACCORDANCE WITH ACI 315-95 WITH ACI 315-96 UNLESS NOTED OTHERWISE. ALL TENSION DEVELOPMENT LENGTHS SHALL BE 23

STRUCTURAL CONNECTORS: MANUFACTURERS AND PRODUCT NUMBER FOR CONNECTORS, ANCHORS, SAME OR OTHER MANUFACTURER CAN BE SUBSTITUTED FOR ANY DEVICES LISTED IN THE EXAMPLE TABLES AS LONG AS IT MEETS THE REQUIRED LOAD CAPACITIES. MANUFACTURER'S INSTALLATION INSTRUCTIONS MUST BE FOLLOWED TO ACHIEVE RATED LOADS.

ANCHOR BOLTS: A-307 ANCHOR BOLTS WITH MINIMUM EMBEDMENT AS SPECIFIED IN DRAWINGS BUT NO LESS THAN 7" IN CONCRETE OR REINFORCED BOND BEAM OR 15" IN GROUTED CMU.

 $\underline{\text{WASHERS:}} \hspace{0.2cm} \text{WASHERS USED WITH 1/2" BOLTS TO BE 2" x 2" x 9/64"; WITH 5/8" BOLTS TO BE 3" x 3" x 9/64";} \\$ WITH 3/4" BOLTS TO BE 3" x 3" x 9/64"; WITH 7/8" BOLTS TO BE 3" x 3" x 5/16"; NO.

NAILS: ALL NAILS ARE COMMON NAILS UNLESS OTHERWISE SPECIFIED OR ACCEPTED BY FBC TEST REPORTS AS HAVING EQUAL STRUCTURAL VALUES.

N3-WINDLOAD ENGINEER'S SCOPE OF WORK: The wind load engineer is engineer of record for compliance of the structure to wind load requirements of FBC 2001, Section 1606. If trusses are used, the wind load engineer is not engineer of record for the trusses and did not design the trusses or delegate to the trusses are designer.

"EVERYTHING YOU NEED FOR YOUR BUILDING PERMIT" Mark Disosway P.E.

POB 868, Lake City, FL 32056 Phone: (386) 754-5419 Fax: (386) 269-4871 Email: windloadengineer@bellsouth.net

ocation: Lot 36 Wise Estates S/D Columbia Coutny, Florida

The Nathan 4 Bed Lot 36 Wise Estates S/D

Builder: Ewpl, Inc.

Designer: DDS

Approved: FLPE#53915

Sheet S-1 of 2 Sheets Windload Engineering

OFFICE CON

Job # 509232