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# STRUCTURAL ANALYSIS for the ROOFTOP PV SOLAR INSTALLATION

Project: Abdelrahman Abuayyash, 223 Se Victoria Glen, Lake City, FL 32025

Prepared for:



Sunergy

7625 Little Rd Ste 200a - New Port Richey, FL 34654

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Project Number: 66.400399.1, Rev. 0 Report Date: 11/08/2023

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Report Prepared by:



Richard Pantel, P.E. FL License No. 73222 Sealed 11/08/2023



Cover

Richard Digitally signed by Richard Pantel DN: c=US, st=Virginia, I=Round Hill, o=TectoniCorp, P.C. cn=Richard Pantel email=rpantel@princeton-engineering.com Date: 2023.11.08 21:58:18

## **Loading Summary**

Exposure and Occupancy Categories							
В		Exposure Category (ASCE 7-16 Table 26.7.3, Page 266)					
II		Building Use Occupancy / Risk Category (ASCE 7-16 Table 1.5-1, Page 4)					

	Wind Loading:							
V	165	mph	Over-ridden per client request. Original data from Municipality					
V	105	πρπ	provided wind / snow loadings.					
qz	41.47	psf	Velocity qz, calculated at height z [ASD]					

	Snow Loading								
Ī	20		0	nof	Ground Snow Load pg (Over-ridden per client request. Original				
	pg		U	psf	data from Municipality provided wind / snow loadings.)				

Module Data						
Mission Solar E	nergy LLC:	MSE385S	X5R			
Dimensions	mm	ft	in			
Length	1,905	6.25	75.00			
Width	1,041	3.42	41.00			
Area (m^2, ft^2)	2.0	21.35				
Weight	kg	lb				
Module	22.23	49.00				

Roof Panel (Cladding) Loading Sum	Module Loading Summary				
Support Point Loads		Upward	Upward	Upward	Downward
Roof Zones		1,2e	2n,2r,3e	3r	All
Net load per module	lb	-442	-688	-788	100

Positive values indicate net downward force

Stanc	hion Faste	ner Pull-ou	it and Space	cing Calcul
Framing spacing			ft	2.00
Rails / Module			ea	2
Max proposed stanchic	on span		ft	4.00
# fasteners per stanch	ion			2
Screw thread embedm	ent depth		in	2
Safety Factor				1.10
Pull-out for M5 threade	ed fasteners	3	lb/in	103
Factored max fastener	uplift capa	city	lb	376
Fastener details	Material	Stainless	Size	M5
Max stanchion uplift ca	lb	400		
Max support point uplif	t capacity		lb	376

Roof Zones		1,2e	2n,2r,3e	3r
Net lift per module	lb	442	688	788
Min tot screw thread embedment depth rq'd	in	2.35	3.66	4.19
Net uplift pressure 7. 0.60D - 0.6W	psf	-17.69	-27.53	-31.51
Allowable lift area / support point	sf	21.27	13.67	11.94
Max rail span per framing spacing	ft	4.00	4.00	4.00
Landscape Modules				
Length along rafter	ft	3.42		
Lift calc'ed max stanchion EW spacing	ft	> 6	6.00	6.00
Max stanchion EW spacing	ft	4.00	4.00	4.00
Maximum module area / support point	sf	6.83	6.83	6.83
Factored lift per support point	lb	-121	-188	-215
Portrait Modules				
Length along rafter	ft	6.25		
Lift calc'ed max stanchion EW spacing	ft	6.00	4.00	2.00
Max stanchion EW spacing	ft	4.00	4.00	2.00
Maximum module area / support point	sf	12.50	12.50	6.25
Factored lift per support point	lb	-221	-344	-197

Stanchion support threaded fastener sizes are indicated in the Module Loading Summary table above. Lift forces were determined from GCp and other coefficients contained in the ASCE nomographs

#### **Conclusions**

Princeton Engineering was asked to review the roof of Abdelrahman Abuayyash, located at 223 Se Victoria Glen, Lake City, FL, by Sunergy, to determine its suitability to support a PV solar system installation.

The referenced building's roof structure was field measured by Sunergy. The attached framing analyses reflect the results of those field measurements combined with the PV solar module locations shown on the PV solar roof layout design prepared by Sunergy. Loads are calculated to combine the existing building and environmental loads with the proposed new PV array loads.

Sunergy selected the K2-Systems CrossRail 44-X racking with K2-Systems Splice Foot XL w/2 bolts stanchions for this project. The racking and support stanchions shall be placed as shown on their plans, dated 11/08/2023, and shall be fastened to the roof framing using fastener sizes indicated in this report. Rack support spacing shall be no more than that shown above. Note that support points for alternating rows shall share the same truss.

Intermediate rows shall move the support points laterally to the next truss.



Google Location Map

#### Framing Summary

Based upon the attached calculations and in accordance with the FBC 2020 Section R324.4 and the FBC's reference to IRC 2018 Section 1607.12.5.2, the existing roofs' framing systems are capable of supporting the additional loading for the proposed PV solar system along with the existing building and environmental loads. No supplemental roof framing structural supports are required. Minimum required anchorage fastening is described above.

Wood fastener notes: 1) Fastener threads must be embedded in the side grain of a roof support structural member or other structural member integrated into the building's structure. 2) Fastener must be located in the middle third of the structural member. 3) Install fasteners with head and where required, washer, flush to material surface (no gap). Do not over-torque.

#### References and Codes:

- 1) ASCE 7-16 Minimum Design Loads for Buildings and Other Structures
- 2) IBC 2018
- 3) FBC 2020
- 4) 2022 Florida Statues and 2023 Florida Administrative Codes
- 5) American Wood Council, NDS 2018, Table 12.2A, 12.3.3A.
- 6) American Wood Council, Wood Structural Design, 1992, Figure 6.

Location: MP 1

Member: Truss - Total Length 19.67 ft, Unsupported 19.67 ft

Geometric Data					
Θ	deg.	22.00	Angle of roof plane from horizontal, in degrees		
ω	deg.	0.00	Angle the solar panel makes with the roof surface		
L	ft.	51.67	Length of roof plane, in feet (meters)		
W	ft.	18.67	Plan view width of roof plane, in feet (meters)		
h	ft.	15.00	Average height of roof above grade, in feet (meters)		

Roof Wind Zone Width				
	use, a =	3.00	ft	

Wind Veloc	Wind Velocity Pressure, $q_z$ evaluated at the height z							
$q_z =$	$q_z$ = 41.47 psf Vasd $q_z$ = 24.96 psf Basic wind pressure							
V=	165	mph						

Framing Data						
Wood type	US S	oruce				
Wood source, moisture content	White	0.12%				
# Framing Members / Support		1				
Rafter / Truss OC	in	24.00				
Member Total Length	ft	19.67				

2	# Rafters / Rack Support Width
4.00	Rack Support Spacing (ft)
48	Max. Rack Support Spacing (in)
3	Max # of mod's / Top truss chord

Member Properties	Member
Name	(1) 2x4
Repetitive Member Factor (Cr)	1.15

\* Mem properties based upon field measurements

Top truss chord

Module Physical Data					
Weight	kg	lb	psf load		
Module	22.23	49.00	2.29		
4 Stanchions	1.27	2.8	0.13		
Existing Dead Loads	Units	Value	Description		
Roof Deck & Surface	psf	4.40	Truss memb	pers' self weight added to FEA analys	

Rack Support Spacing					
Across rafters	ft	4.0			
Along rafter slope	ft	6.3			
Area / support point	sf	12.5			
Uphill gap between modules	in	1.0	0.08	ft	

Member Total Length	ft	19.67	
Maximum member free span	ft	19.67	Top truss chord span

#### ASCE 7-16 Method for Calculating Uplift on PV Modules

Notation

Lp = Panel chord length.

p = uplift wind pressure

γa = Solar panel pressure equalization factor, defined in Fig. 29.4-8.

γE = Array edge factor as defined in Section 29.4.4.

 $\theta$  = Angle of plane of roof from horizontal, in degrees.

### 29.4.4 Rooftop Solar Panels Parallel to the Roof Surface on Buildings of All Heights and Roof Slopes.

$$\Theta >= 7 \text{ deg}$$
 TRUE

Min.d1: Exposed Max.d1: Exposed TRUE

1.5(Lp) = 5.13

Use EXPOSED for uplift calculations

 $\gamma E = 1.5$   $\gamma a = 0.67$ 

 $p = qh(GCp) (\gamma_E) (\gamma_a) (lb/ft2)$  (29.4-7)

Zones	1,2e	2n,2r,3e	3r
p, Windload (psf)	-37.09	-53.49	-60.12

ASCE 7-16 Chapter 2 Combinations of Loads, Table 2.4, Page 8 (in psf)						
Zones	1,2e	2n,2r,3e	3r	All Zones		
2.2 SYMBOLS AND NOTATION	Module	Module	Module	Downward		
2.2 STINIBOLS AND INCTATION	Upward	Upward	Upward	Downward		
D = dead load of PV Module + Stanchion	2.43	2.43	2.43	2.43		
W = wind load	-37.09	-53.49	-60.12	11.32		

### 2.4 Combining Nominal Loads Using Allowable Stress Design (in psf)

2.4.1 Basic Combinations. Loads listed herein shall be considered to act in the following combinations; whichever produces the most unfavorable effect in the building, foundation, or structural member being considered. Effects of one or more loads not acting shall be considered.

Combination Formulae	Upward	Upward	Upward	Downward	
Use this loading combination for DOWNWARD for Proposed PV Dead Load					
5. D - 0.6W	2.43	2.43	2.43	9.22	
Module Support point load (lb)	30	30	30	115	
Cr Factored Module Support point load (lb)	26	26	26	100	

Use this loading combination for UPWARD for Proposed PV Dead Load						
7. 0.60D - 0.6W -17.69 -27.53 -31.51 7.61						
Module Support point load (lb)	-221	-344	-394	95		

#### **DOWNWARD**

Presume loading directly over member.

	Combined Dead and Wind Pressure Downward Loading							
	Тор	truss chord	span					
PV Module Row	Point load loc's from Left support		Module Support Point Load	Comment	Module Orientation			

	ft from left	lb		
1	0.42	100		Portrait
1	6.67		Support placed on adjoining truss	Portrait
2	6.75		Support placed on adjoining truss	Portrait
2	13.00	100		Portrait
3	13.09	100		Portrait
3	19.34		Support placed on adjoining truss	Portrait

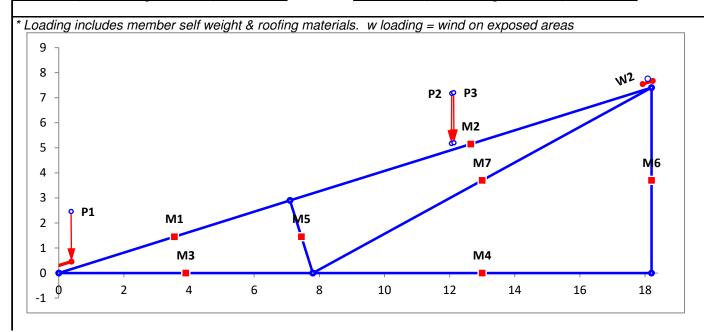
### Truss Data and Loading for MP 1

Roof slope (degrees)	22.00
Top ridge height above floor plane	7.37

Length of roof plane	19.67
Length of floor plane	18.25

			ır
Roof Plane		Floor	Plane
Mem #	Mem Type	Mem #	Mem Type
1	2x4	3	2x4
2	2x4	4	2x4

russ Segments								
	Diago	onals	Diag	onals				
	Mem #	Mem Type	Mem #	Mem Type				
	5	2x4	7	2x4				
]	6	2x4						



Location: MP 2

Member: Truss - Total Length 15.25 ft, Unsupported 15.25 ft

Geometric Data				
Θ	deg.	22.00	Angle of roof plane from horizontal, in degrees	
ω	deg.	0.00	Angle the solar panel makes with the roof surface	
L	ft.	49.92	Length of roof plane, in feet (meters)	
W	ft.	16.25	Plan view width of roof plane, in feet (meters)	
h	ft.	15.00	Average height of roof above grade, in feet (meters)	

Roof Wind Zone Width						
	use, a =	3.00	ft			

Wind Velocity Pressure, $q_z$ evaluated at the height z								
$q_z =$	41.47	psf	psf $Vasd q_z = 24.96$ psf Basic wind pressure					
V=	165		mph					

Framing Data					
Wood type	US Spruce				
Wood source, moisture content White 0.12		0.12%			
# Framing Members / Support		1			
Rafter / Truss OC	in	24.00			
Member Total Length	ft	15.25			

2	# Rafters / Rack Support Width		
4.00	Rack Support Spacing (ft)		
48	Max. Rack Support Spacing (in)		
2	Max # of mod's / Top truss chord		

Member Properties	Member
Name	(1) 2x4
Repetitive Member Factor (Cr)	1.15

\* Mem properties based upon field measurements

Top truss chord

Module Physical Data				
Weight	kg	lb	psf load	
Module	22.23	49.00	2.29	
4 Stanchions	1.27	2.8	0.13	
Existing Dead Loads	Units	Value		Description
Roof Deck & Surface	psf	4.40	Truss memb	pers' self weight added to FEA analys

15.25

Top truss chord span

Rack Support Spacing					
Across rafters	ft	4.0			
Along rafter slope	ft	6.3			
Area / support point	sf	12.5			
Uphill gap between modules	in	1.0	0.08	ft	
	•			•	
Member Total Length	ft	15.25			

Maximum member free span

#### **ASCE 7-16 Method for Calculating Uplift on PV Modules**

Notation

Lp = Panel chord length.

p = uplift wind pressure

γa = Solar panel pressure equalization factor, defined in Fig. 29.4-8.

yE = Array edge factor as defined in Section 29.4.4.

 $\theta$  = Angle of plane of roof from horizontal, in degrees.

#### 29.4.4 Rooftop Solar Panels Parallel to the Roof Surface on Buildings of All Heights and Roof Slopes. TRUE

Min.d1: Exposed **FALSE** Max.d1: Exposed **TRUE** 1.5(Lp) =5.13

Use EXPOSED for uplift calculations

γE = 1.5 0.67 γa =

 $p = qh(GCp) (\gamma_E) (\gamma_a) (lb/ft2)$ (29.4-7)

Zones	1,2e	2n,2r,3e	3r
p, Windload (psf)	-37.09	-53.49	-60.12

ASCE 7-16 Chapter 2 Combinations of Loads, Table 2.4, Page 8 (in psf)							
Zones	1,2e	2n,2r,3e	3r	All Zones			
2.2 SYMBOLS AND NOTATION		Module	Module	Downword			
		Upward	Upward	Downward			
D = dead load of PV Module + Stanchion	2.43	2.43	2.43	2.43			
W = wind load	-37.09	-53.49	-60.12	11.32			

### 2.4 Combining Nominal Loads Using Allowable Stress Design (in psf)

2.4.1 Basic Combinations. Loads listed herein shall be considered to act in the following combinations; whichever produces the most unfavorable effect in the building, foundation, or structural member being considered. Effects of one or more loads not acting shall be considered.

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Use this loading combination for DOWNWARD for Proposed PV Dead Load					
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Module Support point load (lb)	30	30	30	115	
Cr Factored Module Support point load (lb)	26	26	26	100	

Use this loading combination for UPWARD for Proposed PV Dead Load						
7. 0.60D - 0.6W	-17.69	-27.53	-31.51	7.61		
Module Support point load (lb)	-221	-344	-394	95		

#### **DOWNWARD**

Presume loading directly over member.

	Combined Dead and Wind Pressure Downward Loading						
	Тор	truss chord	span				
PV Module Row	Point load loc's from Left support		Module Support Point Load	Comment	Module Orientation		

	ft from left	lb		
1	0.42	100		Portrait
1	6.67		Support placed on adjoining truss	Portrait
2	6.75		Support placed on adjoining truss	Portrait
2	13.00	100		Portrait

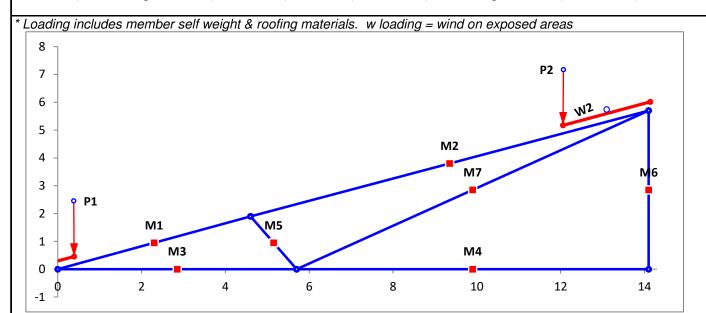
### Truss Data and Loading for MP 2

Roof slope (degrees)	22.00
Top ridge height above floor plane	5.71

Length of roof plane	15.25
Length of floor plane	14.17

			Ir
Roof	Plane	Floor	Plane
Mem #	Mem Type	Mem #	Mem Type
1	2x4	3	2x4
2	2x4	4	2x4

russ Segments							
	Diago	onals	Diag	onals			
]	Mem #	Mem Type	Mem #	Mem Type			
	5	2x4	7	2x4			
	6	2x4					



## FEA Calculation Results for Roof Plane MP 1 for Sunergy Client ABDELRAHMAN ABUAYYASH

IDSPL - 2D Frame Analysis of a 2D frame subject to distributed loads, point loads and moments

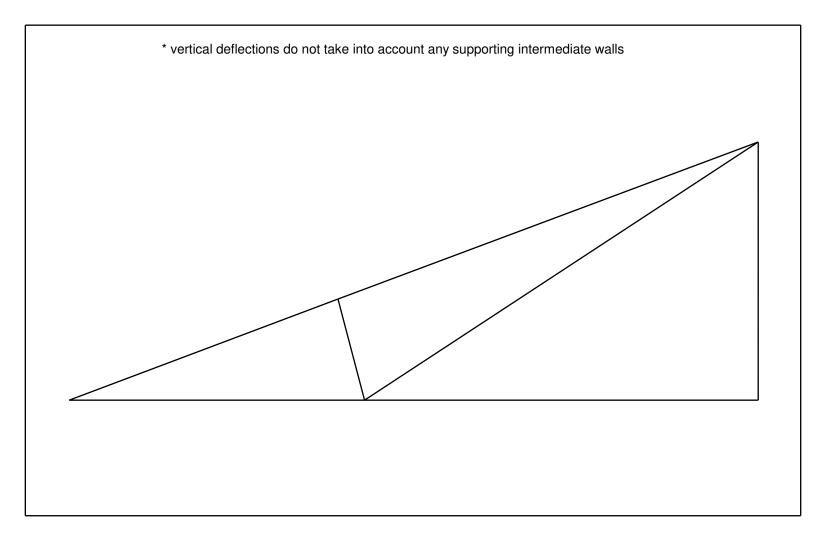
Equilibrium check	FX	FY
Total applied forces	0.00	1416
Total output reactions	0.00	-1416
Output error	1.07E-14	-6.82E-13

1.6E-05

-						
	Node Results			Bean	n End Res	ults
Direction	Deflection	Reaction	Beam	Shear	Ax	BM
DX1	0.00E+00	-39	1-1	-480	238	1235
DY1	0.00E+00	-583	1-2	-290	160	-1841
RZ1	-1.55E-04	0	2-1	-523	105	-2528
DX2	1.37E-04	0	2-2	281	-221	-4899
DY2	1.07E-04	0	3-1	-49	0	-1235
RZ2	-1.73E-04	0	3-2	158	0	-250
DX3	1.45E-04	0	4-1	0	0	0
DY3	0.00E+00	-387	4-2	0	0	0
RZ3	0.00E+00	-4705	5-1	-86	229	-429
DX4	0.00E+00	64	5-2	-88	222	-687
DY4	0.00E+00	-435	6-1	25	10	-92
RZ4	0.00E+00	145	6-2	25	-25	92
DX5	0.00E+00	-25	7-1	-18	104	34
DY5	0.00E+00	-10	7-2	58	49	102
RZ5	0.00E+00	92				

			Maximum	Deflections	
# of segments/beam	1		1.45E-04	-1.07E-04	
* vertical deflections d	o not take	into accou	unt any suppo	orting intermed	diate walls

Beam DX RZ Shear Ax DY Mom 0.00 -480 1235 238 0.00E+00 0.00E+00 -1.55E-04 7.67 -347 -1541 184 1.25E-04 -1.02E-04 -4.11E-04 2 0.00 -523 -2528 105 1.37E-04 -1.07E-04 -1.73E-04 11.98 -15 -1.79E-03 2 5.04E-05 3.83E-05 -2538 -101 3 -49 0.00E+00 0.00E+00 -1.55E-04 0.00 -1235 3 7.80 95 80 0.00E+00 -4.91E-20 -2.41E-05 0.00E+00 4 0.00 0 0 0.00E+00 0.00E+00 0.00E+00 4 0.00E+00 0.00E+00 10.40 0 0 0 -86 -429 229 0.00E+00 0.00E+00 0.00E+00 5 0.00 -87 -687 224 -1.07E-04 -1.29E-04 5 2.98 1.37E-04 25 -92 0.00E+00 6 0.00 10 0.00E+00 0.00E+00 25 3.85E-06 3.81E-07 6 7.40 92 -18 1.45E-04 0.00 -18 34 104 0.00E+00 0.00E+00 0.00E+00 12.76 107 -4.35E-07 48 1.44E-04 2.24E-07



Scaled 2X Deflected Truss Plot
Roof Plane MP 1 for Sunergy Client ABDELRAHMAN ABUAYYASH

### FEA Calculation Results for Roof Plane MP 2 for Sunergy Client ABDELRAHMAN ABUAYYASH

IDSPL - 2D Frame Analysis of a 2D frame subject to distributed loads, point loads and moments

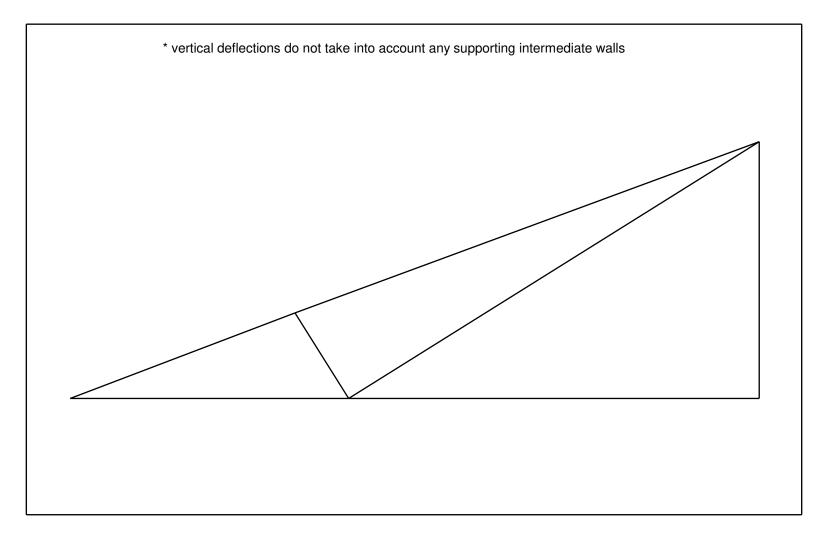
Equilibrium check	FX	FY
Total applied forces	0.00	1004
Total output reactions	0.00	-1004
Output error	-4.97E-14	-3.41E-13

1.7E-05

Ĭ	Node Results			Beam End Results		
Direction	Deflection	Reaction	Beam	Shear	Ax	BM
DX1	0.00E+00	-32	1-1	-335	173	59
DY1	0.00E+00	-524	1-2	-186	112	-1277
RZ1	1.45E-04	0	2-1	-547	101	-1446
DX2	3.49E-05	0	2-2	87	-153	-5154
DY2	1.17E-04	0	3-1	-148	0	-59
RZ2	-4.99E-05	0	3-2	-76	0	-1003
DX3	1.14E-04	0	4-1	0	0	0
DY3	0.00E+00	-153	4-2	0	0	0
RZ3	0.00E+00	-4994	5-1	46	361	-267
DX4	0.00E+00	66	5-2	43	357	-168
DY4	0.00E+00	-322	6-1	34	6	-96
RZ4	0.00E+00	-739	6-2	34	-16	96
DX5	0.00E+00	-34	7-1	-9	98	4
DY5	0.00E+00	-6	7-2	42	63	64
RZ5	0.00E+00	96				

	Maximum Deflections								
# of segments/beam	1		1.14E-04	-1.17E-04					
* vertical deflections do not take into account any supporting intermediate walls									

DX RΖ Beam Shear Ax DY Mom 0.00 -335 59 173 0.00E+00 0.00E+00 1.45E-04 4.98 -222 -1086 126 2.72E-05 -1.14E-04 -2.43E-04 2 0.00 -547 -1446 101 3.49E-05 -1.17E-04 -4.99E-05 10.23 -158 -54 -1.66E-03 2 -3177 3.57E-05 3.13E-05 3 0.00E+00 0.00E+00 1.45E-04 0.00 -148 -59 3 5.70 -121 -764 0.00E+00 7.62E-21 -1.94E-04 0.00E+00 4 0.00 0 0 0.00E+00 0.00E+00 0 0.00E+00 0.00E+00 0.00E+00 4 8.40 0 0 0 -267 0.00E+00 0.00E+00 0.00E+00 5 0.00 46 361 359 -1.17E-04 -1.23E-05 5 2.20 44 -169 3.50E-05 -96 0.00E+00 0.00E+00 6 0.00 34 6 0.00E+00 5.21E-06 1.14E-04 2.91E-07 6 5.70 34 96 -11 0.00 -9 4 98 0.00E+00 0.00E+00 0.00E+00 68 68 8.65E-08 10.15 34 1.14E-04 1.66E-07



Scaled 2X Deflected Truss Plot
Roof Plane MP 2 for Sunergy Client ABDELRAHMAN ABUAYYASH