

DATE 11/05/2008

Columbia County Building Permit

This Permit Must Be Prominently Posted on Premises During Construction

PERMIT

000027467

APPLICANT MARLIN BARNETT PHONE 352 588-0910
ADDRESS 12630 CURLEY ST SAN ANTONIO FL 33576
OWNER TINA & JOHN KILLIN PHONE 755-9537
ADDRESS 172 NW KELLEY LAKE CT LAKE CITY FL 32055
CONTRACTOR JASON WARREN NEWMANN PHONE 352 588-0910

LOCATION OF PROPERTY 90W, TR BROWN RD, TL EMERALD LAKES DR., TR ZACK DR.
TL KELLY LAKE CT., 3RD ON RIGHT

TYPE DEVELOPMENT FOUND. STAB./SFD ESTIMATED COST OF CONSTRUCTION 72400.00

HEATED FLOOR AREA TOTAL AREA HEIGHT STORIES

FOUNDATION WALLS ROOF PITCH FLOOR

LAND USE & ZONING RSF-2 MAX. HEIGHT

Minimum Set Back Requirments: STREET-FRONT 25.00 REAR 15.00 SIDE 10.00

NO. EX.D.U. 1 FLOOD ZONE N/A DEVELOPMENT PERMIT NO.

PARCEL ID 28-3S-16-02372-445 SUBDIVISION EMERALD LAKE

LOT 145 BLOCK PHASE 4 UNIT TOTAL ACRES 0.50

CBC058155
Culvert Permit No. Culvert Waiver Contractor's License Number Applicant/Owner/Contractor
EXISTING X08-356 BK HD N
Driveway Connection Septic Tank Number LU & Zoning checked by Approved for Issuance New Resident

COMMENTS: NOC ON FILE, IMPACT FEE EXEMPT

Check # or Cash 2105

FOR BUILDING & ZONING DEPARTMENT ONLY

(footer/Slab)

Temporary Power date/app. by Foundation date/app. by Monolithic date/app. by
Under slab rough-in plumbing date/app. by Slab date/app. by Sheathing/Nailing date/app. by
Framing date/app. by Rough-in plumbing above slab and below wood floor date/app. by
Electrical rough-in date/app. by Heat & Air Duct date/app. by Peri. beam (Lintel) date/app. by
Permanent power date/app. by C.O. Final date/app. by Culvert date/app. by
M/H tie downs, blocking, electricity and plumbing date/app. by Pool date/app. by
Reconnection date/app. by Pump pole date/app. by Utility Pole date/app. by
M/H Pole date/app. by Travel Trailer date/app. by Re-roof date/app. by

BUILDING PERMIT FEE \$ 365.00 CERTIFICATION FEE \$ 0.00 SURCHARGE FEE \$ 0.00

MISC. FEES \$ 0.00 ZONING CERT. FEE \$ 50.00 FIRE FEE \$ 0.00 WASTE FEE \$

FLOOD DEVELOPMENT FEE \$ FLOOD ZONE FEE \$ CULVERT FEE \$ TOTAL FEE 415.00

INSPECTORS OFFICE CLERKS OFFICE

NOTICE: IN ADDITION TO THE REQUIREMENTS OF THIS PERMIT, THERE MAY BE ADDITIONAL RESTRICTIONS APPLICABLE TO THIS PROPERTY THAT MAY BE FOUND IN THE PUBLIC RECORDS OF THIS COUNTY. AND THERE MAY BE ADDITIONAL PERMITS REQUIRED FROM OTHER GOVERNMENTAL ENTITIES SUCH AS WATER MANAGEMENT DISTRICTS, STATE AGENCIES, OR FEDERAL AGENCIES.

"WARNING TO OWNER: YOUR FAILURE TO RECORD A NOTICE OF COMMENCEMENT MAY RESULT IN YOUR PAYING TWICE FOR IMPROVEMENTS TO YOUR PROPERTY. IF YOU INTEND TO OBTAIN FINANCING, CONSULT WITH YOUR LENDER OR AN ATTORNEY BEFORE RECORDING YOUR NOTICE OF COMMENCEMENT."

EVERY PERMIT ISSUED SHALL BECOME INVALID UNLESS THE WORK AUTHORIZED BY SUCH PERMIT IS COMMENCED WITHIN 180 DAYS AFTER ITS ISSUANCE, OR IF THE WORK AUTHORIZED BY SUCH PERMIT IS SUSPENDED OR ABANDONED FOR A PERIOD OF 180 DAYS AFTER THE TIME THE WORK IS COMMENCED. A VALID PERMIT RECIEVES AN APPROVED INSPECTION EVERY 180 DAYS. WORK SHALL BE CONSIDERED TO BE IN ACTIVE PROGRESS WHEN THE PERMIT HAS RECIEVED AN APPROVED INSPECTION WITHIN 180 DAYS.

The Issuance of this Permit Does Not Waive Compliance by Permittee with Deed Restrictions.

Melinda *CK# 2105*
Columbia County Building Permit Application

| | | | | | |
|--|----------------------|----------------------------------|-------------------------------|--------------------------|-----------------------|
| For Office Use Only | | Application # <u>0810-56</u> | Date Received <u>10/31/08</u> | By <u>LG</u> | Permit # <u>27467</u> |
| Zoning Official <u>BKK</u> | Date <u>05.11.08</u> | Flood Zone <u>N/A</u> | Land Use <u>Res Low Dg</u> | Zoning <u>RSF-2</u> | |
| FEMA Map # <u>N/A</u> | Elevation <u>N/A</u> | MFE <u>N/A</u> | River <u>N/A</u> | Plans Examiner <u>ND</u> | Date <u>11-5-08</u> |
| Comments <u>Imp</u> | | | | | |
| <input checked="" type="checkbox"/> NOC <input checked="" type="checkbox"/> EH <input type="checkbox"/> Deed or PA <input type="checkbox"/> Site Plan <input type="checkbox"/> State Road Info <input type="checkbox"/> Parent Parcel # _____ <input type="checkbox"/> Dev Permit # _____ <input type="checkbox"/> In Floodway <input type="checkbox"/> Letter of Auth. from Contractor <input type="checkbox"/> F W Comp. letter _____ | | | | | |
| IMPACT FEES: EMS _____ | | Fire _____ | Corr _____ | Road/Code _____ | |
| School _____ | | = TOTAL <u>Impact Fee Exempt</u> | | | |

Septic Permit No. N/A Fax 352.588.0911

Name Authorized Person Signing Permit MARLIN BARNETT Phone 352.588.0910

Address 12630 CURLEY STREET, SUITE 104, SAN ANTONIO, FL 33576

Owners Name KILLIN, TINA AND JOHN Phone 386.755.9537

911 Address 172 NW KELLEY LAKE COURT, LAKE CITY, 32055

Contractors Name JASON WARREN NEUMANN/W. A. NEUMANN CONSTRUCTION, INC Phone 352.588.0910

Address 12630 CURLEY STREET, SUITE 104, SAN ANTONIO, FL 33576

Fee Simple Owner Name & Address SAME AS ABOVE

Bonding Co. Name & Address N/A

Architect/Engineer Name & Address GEOHAZARDS, INC. PO BOX 14566, GAINESVILLE, FL 32604

Mortgage Lenders Name & Address N/A

Circle the correct power company - FL Power & Light - Clay Elec. - Suwannee Valley Elec. - Progress Energy

Property ID Number 28-3S-16-02372445-HX Estimated Cost of Construction \$ 72,400.00

Subdivision Name EMERALD LAKE PHASE 4 Lot 145 Block N/A Unit N/A Phase 4

Driving Directions NORTH on NE HERNANDO AVE, LEFT on NE MADISON ST., LEFT onto N MARION AVE/US-441, RIGHT onto W DUVAL ST/US-90. Continue to follow US-90 W., RIGHT on NW BROWN RD., LEFT on NW EMERALD LAKES DR., RIGHT on NW ZACK DR., LEFT on NW KELLY LAKE CT. to 172.
3rd on right

Number of Existing Dwellings on Property 1 EXISTING

Construction of FOUNDATION STABILIZATION AND/OR REPAIR Total Acreage 0.5 AC Lot Size 0.5 AC

Do you need a - ~~Culvert Permit~~ or ~~Culvert Waiver~~ or Have an Existing Drive Total Building Height NO CHANGE

Actual Distance of Structure from Property Lines - Front 35' Side 45' Side 25' Rear 35'

Number of Stories 1 Heated Floor Area 1800 SQ. FT. Total Floor Area 2674 SQ. FT. Roof Pitch N/A

Application is hereby made to obtain a permit to do work and installations as indicated. I certify that no work or installation has commenced prior to the issuance of a permit and that all work be performed to meet the standards of all laws regulating construction in this jurisdiction.

Columbia County Building Permit Application

TIME LIMITATIONS OF APPLICATION : An application for a permit for any proposed work shall be deemed to have been abandoned 180 days after the date of filing, unless such application has been pursued in good faith or a permit has been issued; except that the building official is authorized to grant one or more extensions of time for additional periods not exceeding 90 days each. The extension shall be requested in writing and justifiable cause demonstrated.

FLORIDA'S CONSTRUCTION LIEN LAW: Protect Yourself and Your Investment

According to Florida Law, those who work on your property or provide materials, and are not paid-in-full, have a right to enforce their claim for payment against your property. This claim is known as a construction lien. If your contractor fails to pay subcontractors or material suppliers or neglects to make other legally required payments, the people who are owed money may look to your property for payment, even if you have paid your contractor in full. This means if a lien is filed against your property, it could be sold against your will to pay for labor, materials or other services which your contractor may have failed to pay.

NOTICE OF RESPONSIBILITY TO BUILDING PERMITEE:

YOU ARE HEREBY NOTIFIED as the recipient of a building permit from Columbia County, Florida, you will be held responsible to the County for any damage to sidewalks and/or road curbs and gutters, concrete features and structures, together with damage to drainage facilities, removal of sod, major changes to lot grades that result in ponding of water, or other damage to roadway and other public infrastructure facilities caused by you or your contractor, subcontractors, agents or representatives in the construction and/or improvement of the building and lot for which this permit is issued. No certificate of occupancy will be issued until all corrective work to these public infrastructures and facilities has been corrected.

WARNING TO OWNER: YOUR FAILURE TO RECORD A NOTICE OF COMMENCEMENT MAY RESULT IN YOU PAYING TWICE FOR IMPROVEMENTS TO YOUR PROPERTY. A NOTICE OF COMMENCEMENT MUST BE RECORDED AND POSTED ON THE JOB SITE BEFORE THE FIRST INSPECTION. IF YOU INTEND TO OBTAIN FINANCING, CONSULT WITH YOUR LENDER OR ATTORNEY BEFORE RECORDING YOUR NOTICE OF COMMENCEMENT.

OWNERS CERTIFICATION: I hereby certify that all the foregoing information is accurate and all work will be done in compliance with all applicable laws and regulating construction and zoning. I further understand the above written responsibilities in Columbia County for obtaining this Building Permit.

John P. Keller

Owners Signature

CONTRACTORS AFFIDAVIT: By my signature I understand and agree that I have informed and provided this written statement to the owner of all the above written responsibilities in Columbia County for obtaining this Building Permit.

Marlin Barnett

Contractor's Signature (Permitee)
MARLIN BARNETT

Contractor's License Number CBC 058155

Columbia County

Competency Card Number N/A

Affirmed under penalty of perjury to by the Contractor and subscribed before me this 30TH day of OCTOBER, 2008.

Personally known X or Produced Identification _____

Melinda A. Cheatham

SEAL:

State of Florida Notary Signature (For the Contractor)
MELINDA A. CHEATHAM



Melinda A. Cheatham
My Comm. exp. June 19, 2010
Commission No. DB365754
Revised 1-10-08

Page 2 of 2 (Both Pages must be submitted together.)



FROM BUILDING DEPARTMENT TO THE
KILLIN RESIDENCE

What's your 2008 Credit Score?

☐ Excellent 😊 750 - 840 ☐

☐ Good 😊 660 - 749 ☐

☐ Fair 😊 620 - 659 ☐










☐ Poor 😊 340 - 619 ☐

☐ I Don't Know 😊 ??? ☐

Find out INSTANTLY!

Total Time: 13 minutes Total Distance: 6.61 miles

A: Columbia County Bldg & Zoning: 135 NE Hernando Ave, Lake City, FL 32055, (386) 758-1008

- | | | |
|---|---|--------|
|  | 1: Start out going NORTH on NE HERNANDO AVE toward NE JUSTICE ST. | 0.1 mi |
|  | 2: Turn LEFT onto NE MADISON ST. | 0.0 mi |
|  | 3: Turn LEFT onto N MARION AVE/US-441. | 0.1 mi |
|  | 4: Turn RIGHT onto W DUVAL ST/US-90. Continue to follow US-90 W. | 5.2 mi |
|  | 5: Turn RIGHT onto NW BROWN RD. | 0.8 mi |
|  | 6: Turn LEFT onto NW EMERALD LAKES DR. | 0.1 mi |
|  | 7: Turn RIGHT onto NW ZACK DR. | 0.2 mi |
|  | 8: Turn LEFT onto NW KELLY LAKE CT. | 0.1 mi |
|  | 9: End at 172 NW Kelly Lake Ct Lake City, FL 32055-5064 | |

B: 172 NW Kelly Lake Ct, Lake City, FL 32055-5064

Total Time: 13 minutes Total Distance: 6.61 miles



Call **1-800-FREE411** (1-800-373-3411) and get MapQuest Directions via text message.



All rights reserved. Use subject to License/Copyright Map Legend

Directions and maps are informational only. We make no warranties on the accuracy of their content, road conditions or route usability or expeditiousness. You assume all risk of use. MapQuest and its suppliers shall not be liable to you for any loss or delay resulting from your use of MapQuest. Your use of MapQuest means you agree to our [Terms of Use](#)

NOTICE OF COMMENCEMENT

Inst:200812019884 Date:10/31/2008 Time:1:30 PM
DC, P. DeWitt Cason, Columbia County Page 1 of 1 B:1161 P:1040

County Clerk's Office Stamp or Seal

Tax Parcel Identification Number 28-3S-16-02372-445 HX

THE UNDERSIGNED hereby gives notice that improvements will be made to certain real property, and in accordance with Section 713.13 of the Florida Statutes, the following information is provided in this **NOTICE OF COMMENCEMENT**.

Lot 145 Emerald Lakes Phase 4. ORB 814-1147, 901-743, 905-929, 917-177, 925-1667

1. Description of property (legal description): WD 1077-2506

a) Street (job) Address: 172 NW Kelly Lake CT. Lake City, FL. 32055

2. General description of improvements: Foundation Stabilization and/or Repair

3. Owner Information

a) Name and address: Killin, John P. and Tina R. 172 NW Kelly Lake Ct. Lake City, FL. 32055

b) Name and address of fee simple titleholder (if other than owner) Same as Above

c) Interest in property Fee Simple Titleholder

4. Contractor Information

a) Name and address: W. A. Neumann Construction, Inc., 12630 Curley Street, Suite 104 San Antonio, FL. 33576

b) Telephone No.: 352-588-0910 Fax No. (Opt.) 352-588-0911

5. Surety Information

a) Name and address: N/A

b) Amount of Bond: _____

c) Telephone No.: _____ Fax No. (Opt.) _____

6. Lender

a) Name and address: N/A

b) Phone No. _____

7. Identity of person within the State of Florida designated by owner upon whom notices or other documents may be served:

a) Name and address: _____

b) Telephone No.: _____ Fax No. (Opt.) _____

8. In addition to himself, owner designates the following person to receive a copy of the Lienor's Notice as provided in Section 713.13(l)(b), Florida Statutes:

a) Name and address: _____

b) Telephone No.: _____ Fax No. (Opt.) _____

9. Expiration date of Notice of Commencement (the expiration date is one year from the date of recording unless a different date is specified): _____

WARNING TO OWNER: ANY PAYMENTS MADE BY THE OWNER AFTER THE EXPIRATION OF THE NOTICE OF COMMENCEMENT ARE CONSIDERED IMPROPER PAYMENTS UNDER CHAPTER 713, PART I, SECTION 713.13, FLORIDA STATUTES, AND CAN RESULT IN YOUR PAYING TWICE FOR IMPROVEMENTS TO YOUR PROPERTY; A NOTICE OF COMMENCEMENT MUST BE RECORDED AND POSTED ON THE JOB SITE BEFORE THE FIRST INSPECTION. IF YOU INTEND TO OBTAIN FINANCING, CONSULT YOUR LENDER OR AN ATTORNEY BEFORE COMMENCING WORK OR RECORDING YOUR NOTICE OF COMMENCEMENT.

STATE OF FLORIDA
COUNTY OF COLUMBIA

Tina R. Killin John P. Killin
Signature of Owner or Owner's Authorized Office/Director/Partner/Manager
TINA R. KILLIN John P. Killin
Print Name

The foregoing instrument was acknowledged before me, a Florida Notary, this 7th day of OCT, 2008, by:

Tina R. Killin John P. Killin (type of authority, e.g. officer, trustee, attorney
fact) for _____ (name of party on behalf of whom instrument was executed).

Personally Known ☒ OR Produced Identification _____ Type _____

Notary Signature [Signature] Notary Stamp or Seal: _____

11. Verification pursuant to Section 92.525, Florida Statutes. Under penalties of perjury, I declare that I have read the foregoing and that the facts stated are true to the best of my knowledge and belief.



THOMAS LEE RINEHART
Notary Public, State of Florida
My commission expires September 7, 2009
Commission No. DD469180

Tina R. Killin John P. Killin
Signature of Natural Person Signing (in line #10 above.)



October 30, 2008

Columbia County Building Department
Building and Inspection Department
PO Drawer 1529
Lake City, Florida 32056

SUBJECT: Contractor Licensing and Registration
FOR: W. A. Neumann Construction, Inc.

Dear Sir or Madam,

We are pleased to submit the enclosed documentation in request for registration and licensing of W. A. Neumann Construction, Inc. with the Columbia County Building Department:

1. Power of Attorney showing authorized representatives
2. General Liability Insurance with Columbia County listed as certificate holder
3. Worker's Compensation Insurance with Columbia County listed as certificate holder
4. Our contact information is as follows:

W. A. Neumann Construction, Inc.
12630 Curley Street
Suite 105
PO Box 1207
San Antonio, FL 33576
Phone: (352) 588-0910
Fax: (352) 588-0911
E-mail: mcheatham@waneumannconstruction.com

We appreciate your help in processing these documents. If you need further assistance, please do not hesitate to call our office at (352) 588-0910.

Respectfully,

Melinda Ann Cheatham
W. A. Neumann Construction, Inc.

LETTER OF AUTHORIZATION

Date: 10/17/08

Columbia County Building Department
P.O. Drawer 1529
Lake City, FL 32056

I JASON WARREN NEUMANN, License No. CBC 058155 do hereby

Authorize THOMAS RINEHART, MARLIN BARNETT to pull and sign permits on my
VICKI DUFFY, DENISE SOLOMON, WARREN NEUMANN AND STEVEN L. GRIMES
behalf.

Sincerely,

Jason W. Neumann

Sworn to and subscribed before me this 17TH day of OCTOBER, 2008.

Notary Public: Melinda A. Cheatham

My commission expires: 6/19/2010

Personally Known x

Produced Valid Identification: _____



Melinda A. Cheatham
My Comm. exp. June 19, 2010
Commission No. DD565734



ACORD**CERTIFICATE OF LIABILITY INSURANCE**OP ID KS
WANEU-1DATE (MM/DD/YYYY)
10/30/08

| | | |
|---|--|---------------|
| PRODUCER Stahl & Associates Insurance 3939 Tampa Road Oldsmar FL 34677 Phone: 727-784-8554 Fax: 727-789-2823 | THIS CERTIFICATE IS ISSUED AS A MATTER OF INFORMATION ONLY AND CONFERS NO RIGHTS UPON THE CERTIFICATE HOLDER. THIS CERTIFICATE DOES NOT AMEND, EXTEND OR ALTER THE COVERAGE AFFORDED BY THE POLICIES BELOW. | |
| | INSURERS AFFORDING COVERAGE | NAIC # |
| INSURED W. A. Neumann Construction Inc P.O. Box 1207 San Antonio FL 33576 | INSURER A: Mid-Continent Casualty Co. | |
| | INSURER B: | |
| | INSURER C: | |
| | INSURER D: | |
| | INSURER E: | |

COVERAGES

THE POLICIES OF INSURANCE LISTED BELOW HAVE BEEN ISSUED TO THE INSURED NAMED ABOVE FOR THE POLICY PERIOD INDICATED. NOTWITHSTANDING ANY REQUIREMENT, TERM OR CONDITION OF ANY CONTRACT OR OTHER DOCUMENT WITH RESPECT TO WHICH THIS CERTIFICATE MAY BE ISSUED OR MAY PERTAIN, THE INSURANCE AFFORDED BY THE POLICIES DESCRIBED HEREIN IS SUBJECT TO ALL THE TERMS, EXCLUSIONS AND CONDITIONS OF SUCH POLICIES. AGGREGATE LIMITS SHOWN MAY HAVE BEEN REDUCED BY PAID CLAIMS.

| INSR ADD'L LTR INSR | TYPE OF INSURANCE | POLICY NUMBER | POLICY EFFECTIVE DATE (MM/DD/YY) | POLICY EXPIRATION DATE (MM/DD/YY) | LIMITS |
|---------------------|--|---------------|----------------------------------|-----------------------------------|--|
| A | GENERAL LIABILITY | 04GL000732087 | 09/28/08 | 09/28/09 | EACH OCCURRENCE \$ 1,000,000 |
| | <input checked="" type="checkbox"/> COMMERCIAL GENERAL LIABILITY | | | | DAMAGE TO RENTED PREMISES (Ea occurrence) \$ 100,000 |
| | <input type="checkbox"/> CLAIMS MADE <input checked="" type="checkbox"/> OCCUR | | | | MED EXP (Any one person) \$ Excluded |
| | | | | | PERSONAL & ADV INJURY \$ 1,000,000 |
| | | | | | GENERAL AGGREGATE \$ 2,000,000 |
| | | | | | PRODUCTS - COMP/OP AGG \$ 2,000,000 |
| | | | | | GEN'L AGGREGATE LIMIT APPLIES PER: <input type="checkbox"/> POLICY <input type="checkbox"/> PRO-JECT <input type="checkbox"/> LOC |
| | AUTOMOBILE LIABILITY | | | | COMBINED SINGLE LIMIT (Ea accident) \$ |
| | <input type="checkbox"/> ANY AUTO | | | | BODILY INJURY (Per person) \$ |
| | <input type="checkbox"/> ALL OWNED AUTOS | | | | BODILY INJURY (Per accident) \$ |
| | <input type="checkbox"/> SCHEDULED AUTOS | | | | PROPERTY DAMAGE (Per accident) \$ |
| | <input type="checkbox"/> HIRED AUTOS | | | | |
| | <input type="checkbox"/> NON-OWNED AUTOS | | | | |
| | GARAGE LIABILITY | | | | AUTO ONLY - EA ACCIDENT \$ |
| | <input type="checkbox"/> ANY AUTO | | | | OTHER THAN EA ACC \$ |
| | | | | | AUTO ONLY: AGG \$ |
| | EXCESS/UMBRELLA LIABILITY | | | | EACH OCCURRENCE \$ |
| | <input type="checkbox"/> OCCUR <input type="checkbox"/> CLAIMS MADE | | | | AGGREGATE \$ |
| | | | | | \$ |
| | <input type="checkbox"/> DEDUCTIBLE | | | | \$ |
| | <input type="checkbox"/> RETENTION \$ | | | | \$ |
| | WORKERS COMPENSATION AND EMPLOYERS' LIABILITY | | | | WC STATU-TORY LIMITS OTH-ER |
| | ANY PROPRIETOR/PARTNER/EXECUTIVE OFFICER/MEMBER EXCLUDED? | | | | E.L. EACH ACCIDENT \$ |
| | If yes, describe under SPECIAL PROVISIONS below | | | | E.L. DISEASE - EA EMPLOYEE \$ |
| | | | | | E.L. DISEASE - POLICY LIMIT \$ |
| | OTHER | | | | |

DESCRIPTION OF OPERATIONS / LOCATIONS / VEHICLES / EXCLUSIONS ADDED BY ENDORSEMENT / SPECIAL PROVISIONS

CERTIFICATE HOLDER**CANCELLATION**

LAKECTY

Lake County
Drawer 1529
Lake City FL 32056

SHOULD ANY OF THE ABOVE DESCRIBED POLICIES BE CANCELLED BEFORE THE EXPIRATION DATE THEREOF, THE ISSUING INSURER WILL ENDEAVOR TO MAIL 10 DAYS WRITTEN NOTICE TO THE CERTIFICATE HOLDER NAMED TO THE LEFT, BUT FAILURE TO DO SO SHALL IMPOSE NO OBLIGATION OR LIABILITY OF ANY KIND UPON THE INSURER, ITS AGENTS OR REPRESENTATIVES.

AUTHORIZED REPRESENTATIVE

ACORD. CERTIFICATE OF LIABILITY INSURANCE

CERTIFICATE NO. / DATE
AC08-13100438-717902
10/30/2008 9:40:17AM

PRODUCER
Highpoint Risk Services LLC
14160 Dallas Parkway #500
Dallas, TX 75254
(800) 632-5096 (972) 715-0959
Fax: (972) 404-4450

THIS CERTIFICATE IS ISSUED AS A MATTER OF INFORMATION ONLY AND CONFERS NO RIGHTS UPON THE CERTIFICATE HOLDER. THIS CERTIFICATE DOES NOT AMEND, EXTEND OR ALTER THE COVERAGE AFFORDED BY THE POLICIES BELOW.

INSURERS AFFORDING COVERAGE

INSURED: AMS I/c/E:
W.A. NEUMANN CONSTRUCTION, INC.
12630 CURLEY ST. STE 105
SAN ANTONIO, FL 33576
(352) 588-0910 Fax: (352) 588-0911

INSURER A: Companion Property and Casualty Insurance Comp
INSURER B:
INSURER C:
INSURER D:
INSURER E:

COVERAGES

THE POLICIES OF INSURANCE LISTED BELOW HAVE BEEN ISSUED TO THE INSURED NAMED ABOVE FOR THE POLICY PERIOD INDICATED. NOTWITHSTANDING ANY REQUIREMENT, TERM OR CONDITION OF ANY CONTRACT OR OTHER DOCUMENT WITH RESPECT TO WHICH THIS CERTIFICATE MAY BE ISSUED OR MAY PERTAIN, THE INSURANCE AFFORDED BY THE POLICIES DESCRIBED HEREIN IS SUBJECT TO ALL THE TERMS, EXCLUSIONS AND CONDITIONS OF SUCH POLICIES. AGGREGATE LIMITS SHOWN MAY HAVE BEEN REDUCED BY PAID CLAIMS.

| INSR LTR | TYPE OF INSURANCE | POLICY NUMBER | POLICY EFFECTIVE DATE (MM/DD/YY) | POLICY EXPIRATION DATE (MM/DD/YY) | LIMITS |
|----------|--|---------------|----------------------------------|-----------------------------------|--|
| | GENERAL LIABILITY <input type="checkbox"/> COMMERCIAL GENERAL LIABILITY <input type="checkbox"/> CLAIMS MADE <input type="checkbox"/> OCCUR GEN'L AGGREGATE LIMIT APPLIES PER <input type="checkbox"/> POLICY <input type="checkbox"/> PRO-ECT <input type="checkbox"/> LOC | | | | EACH OCCURRENCE \$ FIRE DAMAGE (Any One Fire) \$ MED EXP (Any one person) \$ PERSONAL & ADV INJURY \$ GENERAL AGGREGATE \$ PRODUCTS - COMP/OP AGG \$ |
| | AUTOMOBILE LIABILITY <input type="checkbox"/> ANY AUTO <input type="checkbox"/> ALL OWNED AUTOS <input type="checkbox"/> SCHEDULED AUTOS <input type="checkbox"/> HIRED AUTOS <input type="checkbox"/> NON-OWNED AUTOS | | | | COMBINED SINGLE LIMIT (Ea accident) \$ BODILY INJURY (Per person) \$ BODILY INJURY (Per accident) \$ PROPERTY DAMAGE (Per accident) \$ |
| | GARAGE LIABILITY <input type="checkbox"/> ANY AUTO | | | | AUTO ONLY - EA ACCIDENT \$ OTHER THAN EA ACC \$ AUTO ONLY: AGG \$ |
| | EXCESS LIABILITY <input type="checkbox"/> OCCUR <input type="checkbox"/> CLAIMS MADE DEDUCTIBLE \$ RETENTION \$ | | | | EACH OCCURRENCE \$ AGGREGATE \$ \$ \$ \$ |
| A | WORKERS COMPENSATION AND EMPLOYERS' LIABILITY | WC77779990601 | 04/01/2008 | 04/01/2009 | X WC STATUS: <input type="checkbox"/> TOY LIMITS <input type="checkbox"/> OTH-ER E.L. EACH ACCIDENT \$ 1000000 E.L. DISEASE - EA EMPLOYEE \$ 1000000 E.L. DISEASE - POLICY LIMIT \$ 1000000 |
| | OTHER <input type="checkbox"/> | | | | LIMITS \$ LIMITS \$ |

DESCRIPTION OF OPERATIONS/LOCATIONS/VEHICLES/EXCLUSIONS ADDED BY ENDORSEMENT/SPECIAL PROVISIONS
1. This certificate remains in effect, provided the client's account is in good standing with AMS. Coverage is not provided for any employee for which the client is not reporting wages to AMS. Applies to 100% of the employees of AMS leased to W.A. NEUMANN CONSTRUCTION, INC., effective 04/01/2008.
PLEASE SEE ATTACHED EMPLOYEE ROSTER.

CERTIFICATE HOLDER

ADDITIONAL INSURED; INSURER LETTER

CANCELLATION

LAKE COUNTY...
PO DRAWER 1529
LAKE CITY, FL 32056

SHOULD ANY OF THE ABOVE DESCRIBED POLICIES BE CANCELLED BEFORE THE EXPIRATION DATE THEREOF, THE ISSUING INSURER WILL ENDEAVOR TO MAIL 30 DAYS WRITTEN NOTICE TO THE CERTIFICATE HOLDER NAMED TO THE LEFT, BUT FAILURE TO DO SO SHALL IMPOSE NO OBLIGATION OR LIABILITY OF ANY KIND UPON THE INSURER, ITS AGENTS OR REPRESENTATIVES.

AUTHORIZED REPRESENTATIVE

[Signature]

AC# 3870432

STATE OF FLORIDA

DEPARTMENT OF BUSINESS AND PROFESSIONAL REGULATION
CONSTRUCTION INDUSTRY LICENSING BOARD

SEQ# L08072300765

| DATE | BATCH NUMBER | LICENSE NBR |
|------------|--------------|-------------|
| 07/23/2008 | 080032675 | CBC058155 |

The BUILDING CONTRACTOR
Named below IS CERTIFIED
Under the provisions of Chapter 489 FS.
Expiration date: AUG 31, 2010

NEUMANN, JASON WARREN
W A NEUMANN CONSTRUCTION INC
14007 12TH ST
DADE CITY FL 33525



CHARLIE CRIST
GOVERNOR

DISPLAY AS REQUIRED BY LAW

CHUCK DRAGO
INTERIM SECRETARY

Columbia County Property Appraiser

DB Last Updated: 10/21/2008

2008 Certified Values

Tax Record

Property Card

Interactive GIS Map

Print

Parcel: 28-3S-16-02372-445 HX

Owner & Property Info

Search Result: 1 of 1

| | | | |
|-------------------------|---|---------------------|----|
| Owner's Name | KILLIN JOHN P & TINA R | | |
| Site Address | KELLY LAKE | | |
| Mailing Address | 172 NW KELLY LAKE CT LAKE CITY, FL 32055 | | |
| Use Desc. (code) | SINGLE FAM (000100) | | |
| Neighborhood | 28316.05 | Tax District | 2 |
| UD Codes | MKTA06 | Market Area | 06 |
| Total Land Area | 0.500 ACRES | | |
| Description | LOT 145 EMERALD LAKES PHASE 4. ORB 814-1147, 901-743, 905-929, 917-177, 925-1667, WD 1077-2506. | | |

GIS Aerial



Property & Assessment Values

| | | |
|------------------------------|----------|--------------|
| Mkt Land Value | cnt: (1) | \$32,000.00 |
| Ag Land Value | cnt: (0) | \$0.00 |
| Building Value | cnt: (1) | \$138,919.00 |
| XFOB Value | cnt: (2) | \$4,425.00 |
| Total Appraised Value | | \$175,344.00 |

| | |
|----------------------------|------------------------|
| Just Value | \$175,344.00 |
| Class Value | \$0.00 |
| Assessed Value | \$175,344.00 |
| Exempt Value | (code: HX) \$50,000.00 |
| Total Taxable Value | \$125,344.00 |

Sales History

| Sale Date | Book/Page | Inst. Type | Sale VImp | Sale Qual | Sale RCode | Sale Price |
|------------|-----------|------------|-----------|-----------|------------|--------------|
| 3/17/2006 | 1077/2506 | WD | I | Q | | \$195,500.00 |
| 4/20/2001 | 925/1667 | WD | I | Q | | \$140,000.00 |
| 12/21/2000 | 917/177 | WD | I | U | 06 | \$115,000.00 |

Building Characteristics

| Bldg Item | Bldg Desc | Year Blt | Ext. Walls | Heated S.F. | Actual S.F. | Bldg Value |
|---|---------------------|----------|-----------------|-------------|-------------|--------------|
| 1 | SINGLE FAM (000100) | 2000 | Common BRK (19) | 1800 | 2674 | \$138,919.00 |
| Note: All S.F. calculations are based on exterior building dimensions. | | | | | | |

Extra Features & Out Buildings

| Code | Desc | Year Blt | Value | Units | Dims | Condition (% Good) |
|------|------------|----------|------------|----------|-----------|--------------------|
| 0166 | CONC,PAVMT | 2000 | \$2,475.00 | 1650.000 | 0 x 0 x 0 | (.00) |
| 0120 | CLFENCE 4 | 2007 | \$1,950.00 | 260.000 | 0 x 0 x 0 | (.00) |

Land Breakdown

| Lnd Code | Desc | Units | Adjustments | Eff Rate | Lnd Value |
|----------|-----------|---------------------|---------------------|-------------|-------------|
| 000100 | SFR (MKT) | 1.000 LT - (.500AC) | 1.00/1.00/1.00/1.00 | \$32,000.00 | \$32,000.00 |

GEOHAZARDS, INC.

Professional Geological, Geophysical and Geotechnical Engineering Services

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August 25, 2008

Geohazards, Inc., Investigation No. 2008385

CLAIM INVESTIGATION REPORT

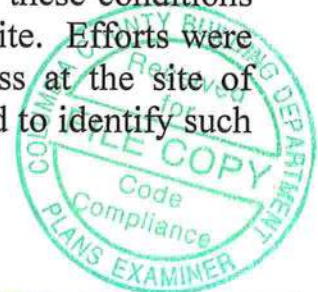
GEOTECHNICAL INVESTIGATION OF THE GEOLOGICAL SUBSURFACE
AT THE JOHN AND TINA KILLIN RESIDENCE,
172 NORTHWEST KELLEY LAKE COURT, LAKE CITY, FLORIDA

INTRODUCTION

Purpose

Geohazards, Inc. was tasked by Florida Farm Bureau Insurance Companies (Claim No. 441215) to conduct a geotechnical investigation at the above referenced locality. The purpose of the investigation was to determine the probable cause of distress at the subject property.

This investigation was conducted to provide a geophysical characterization of the geological subsurface, with verification by drilling. In particular, efforts were designed to determine the presence of subsurface cavities and subsurface zones of disruption that might contribute to subsidence. Any of these conditions could be responsible for existing or potential subsidence at the site. Efforts were also incorporated into this investigation to determine if distress at the site of investigation is attributable to causes other than geotechnical, and to identify such causes.



Scope

This investigation was conducted in accordance with the provisions of Florida Statutes Chapters 627.706 and 627.707, as amended by the Florida Legislature in 2006. In particular, definitions of scientific features and conditions as expressed in Chapter 627.706 are adopted in this report, and all testing conducted is in compliance with Chapter 627.7072. Furthermore, the scope and scientific techniques utilized are generally consistent with the protocols specified by the Florida Geological Survey, Special Publication No. 57, 2005 (Geological and Geotechnical Investigation Procedures For Evaluation of the Causes of Subsidence Damage in Florida). This report complies with the provisions of Chapter 627.7073.

The investigation conducted and reported herein included the following:

- A review of available geologic maps and other published data to establish the general probable lithology and regional conditions for the site of investigation.
- A reconnaissance of the site of investigation to recognize and identify surface conditions pertinent to the purpose of the investigation.
- An interview with the property owner to determine the nature and timing of any damage and to determine the history of the site, including photographic documentation.
- An inspection and assessment of the affected structures and a structural engineering evaluation of possible sources of distress.
- Four Hand Auger Borings to determine the nature of the near-surface materials, and to identify soil conditions at the site.
- Laboratory Analyses of selected samples to characterize specific properties of significance to the site.
- Static Cone Penetration tests to investigate the bearing capacity of the near-surface materials.
- Excavation of two test pits to determine the nature and depth of the foundation.

- A Ground Penetrating Radar (GPR) investigation of the site to determine evidence for anomalous subsurface features or conditions.
- An Electrical Resistivity (ER) investigation of the site to assist in the recognition of site-specific geological conditions at the subject property and to determine evidence for the presence of anomalous subsurface features or conditions.
- Floor elevation surveys to identify variations in elevation within the main residence and appropriate secondary buildings.
- Three Standard Penetration Test (SPT) borings to explore deeper subsurface conditions.
- A final report summarizing results and conveying professional opinions, including a possible mitigation strategy with technical specifications for subsurface stabilization.

Site Information

The initial reconnaissance and geophysical field investigation were conducted on June 18, 2008. The standard penetration test borings were conducted on June 26 and July 2, 2008.

The site of investigation is located at 172 NW Kelley Lake Court, Lake City, Florida. Based on information available from the Columbia County property appraiser's office, the legal description and property owners are as follows:

LOT 145 EMERALD LAKES PHASE 4. ORB 814-1147, 901-743, 905-929, 917-177, 925-1667, WD 1077-2506.
JOHN P. AND TINA R. KILLIN

This site includes a single-story, wood frame structure with brick and vinyl siding. For purposes of orientation the front door is assumed to be on the south side of the structure. A screened patio area is attached to north side of the structure. Buried utilities are located south and west of the structure. A buried septic system is located southeast of the structure. A well is located southwest of

the structure. A gutter system was present at the Killin residence with downspouts discharging rainwater approximately 6 inches to 3 feet away from the structure.

The homeowner, John Killin, was present for the interview portion of our site visit. According to available information, the structure was built in 2000 and Mr. and Mrs. Killin purchased the home in 2006. Mr. Killin reported that he first noticed minor distress in late 2006 as he was moving into the house. He stated that he removed the carpet in the living room in May 2008 to reveal multiple cracks in the floor slab. Mr. Killin pointed out several cracked and/or loose floor tiles and misaligned doors throughout the house.

An interior inspection of the structure revealed cracks in the floor slab (up to 1/2 inch) with up to 1/4 inch vertical displacement in the living room and closet containing the air conditioning handler. Loose floor tiles were present in the dining room. Hairline tile cracks were noted in the laundry room, kitchen, master bathroom, and east bathroom. Wall and ceiling cracks (hairline to 1/16 inch) were observed in the kitchen, laundry room, master bedroom, living room, northeast bedroom, and southeast bedroom. An inspection of the garage revealed meandering hairline cracks in the floor slab and a horizontal crack (1/16 inch) below the laundry room entrance.

An exterior inspection of the structure revealed stair-step cracks (hairline to 1/8 inch) in the east wall, cracks in the screen porch slab (1/16 to 1/8 inch), cracks in the driveway with 1/8 inch vertical displacement. The pavers located at the northeast corner of the structure appeared to be uneven. Mr. Killin reported that the pavers had shifted from their original, level position. A shallow surface depression was observed at the northeast corner of the driveway and measured approximately 8 by 13 feet at the surface. An additional surface depression was located approximately 40 feet north of the rear patio and measured approximately 4 by 12 feet at the surface. Both depressions were approximately 6 inches deep.

Copies of color photographs of the structure are attached.

REGIONAL CONDITIONS

Geology

Based on map consultations and personal inspection, the surficial geologic material at the study site is the Hawthorn Group of geological formations overlain by a cover of very young unconsolidated sands and sandy clays. These consist of fine to medium grained, unconsolidated quartz sand, silt, and clay in varying proportions and thickness. Shrink/swell clays of significant size, continuity and nearness to the surface are a particularly troublesome characteristic of the Hawthorn where they occur in significant thickness and lateral continuity. Concrete slabs and foundations can be severely damaged where such a geologic condition occurs.

The Suwannee and Ocala Limestones underlie the Hawthorn. These limestone units have experienced significant dissolution and the creation of an intricate cavernous system. Problems in the development of sinkholes are related to the size and nearness to the surface of the limestone and these underground cavities. The upper surface of the limestone is highly irregular.

Topography

The Killin property is located in Section 28 of Township 3 South and Range 16 East. Elevation information available on the U.S. Geological Survey Lake City West 7.5 minute Quadrangle 1:24,000 topographic map is shown in the Appendix. The immediate neighborhood of the Killin residence ranges from approximately 110 to 150 feet NGVD. The Killin residence is situated at approximately 135 feet NGVD.

Hydrology

Based on the U.S. Geological Survey's Map entitled Potentiometric Surface of the Upper Floridan Aquifer in the Ichetucknee River and Vicinity, Northern Florida, September 2003, the expected Floridan Aquifer potentiometric surface elevation in the area of the subject property is approximately 45 to 55 feet above mean sea level. The surficial water table was observed at 3 feet depth in two of the three standard penetration test borings.

Soils

The U.S. Department of Agriculture Soil Conservation Service (SCS) Soil Survey of Columbia County describes the soil underlying the Killin property as Alpin fine sand, 0 to 5 percent. This excessively drained soil forms on ridges on marine terraces, knolls on marine terraces, and flats on marine terraces. The typical profile is fine sand within the upper 80 inches. The parent material is eolian deposits or sandy marine deposits.

The water table is at a depth of more than 80 inches. The available water capacity is low (about 3.9 inches).

Alpin and similar soils make up 80 percent of the soil, and minor components make up the remaining 20 percent. Minor components include Albany, Chipley, Blanton and Lakeland soils.

FIELD TEST METHODS: GEOLOGICAL AND GEOTECHNICAL

Hand Auger Borings

Four hand auger borings (HA-1 through HA-4) were conducted at sites shown on the location map. The borings were performed in general accordance with ASTM standard D1452-80 (2000) entitled "Standard Practice for Soil Investigation and Sampling by Auger Borings." The borings were conducted by manually rotating the auger into the ground to termination depths of approximately 2 to 5 feet providing a continuous profile of the near-surface materials. Increments of approximately 0.5 feet are extracted for description and, if necessary, retention for later analyses. Results of the hand auger borings are shown in the Hand Auger Investigation profiles.

Laboratory Analyses

Representative samples of material collected at the site of investigation were stored in sealed bags and analyzed. The laboratory procedures followed include a sieve analysis (ASTM Standard D1140) to determine the percentage of fine-grained material (-No. 200 mesh sieve screen), determination of the natural

moisture percentage of the sample (ASTM Standard D2216), and Atterberg limits (ASTM standard D4318) to determine plasticity indexes. Results are attached.

Static Cone Penetration Tests

Static hand cone penetration tests (CPT) were completed at thirteen locations around the perimeter of the dwelling as shown on the Site Plan Map. The measurements were acquired with a Durham Geo Model S212 double rod portable static cone penetrometer. Data were collected by pushing a steel rod with a cone-shaped tip into the ground and measuring the deflection of a proving ring as the probe was advanced. Results are shown in the attached Cone Penetrometer Results Graphs.

Standard Penetration Tests

The standard penetration test (SPT) is a widely accepted method of testing subsurface materials. It is conducted in accordance with ASTM standard D1586-99 titled "Standard Test Method for Penetration Test and Split-Barrel Sampling of Soils."

With SPT borings, a rotary drilling rig is used to advance the borehole to the desired test depth. A 2 feet long, 2 inch diameter split-barrel sampler attached to the end of a string of drilling rods is then driven 18 inches into the ground by successive blows of a 140 pound hammer freely dropping 30 inches. The sum of blows required for penetration of the second and third 6 inch increments of penetration constitutes the "N" value.

Following an individual test, the sampler is extracted to allow visual classification and retention, if desired, of the core sample. Tests are usually performed at 5 feet depth intervals. N-values are generally correlated with material properties of stability to allow a conservative estimate of the behavior of subsurface materials.

Three SPT borings were conducted in this investigation at the sites shown on the location map. Race Drilling, Inc. of DeBary, Florida, and All County Drilling, LLC. of Mt. Dora, Florida, conducted the borings under the supervision of a geologist from Geohazards, Inc. Results are shown in the attached logs.

FIELD TEST METHODS: STRUCTURAL ANALYSES

Structural Assessment

A visual assessment of the structural condition of the Killin residence was completed at the time of the initial investigation and a subsequent evaluation of the structural damage was completed by a structural engineer. The evaluation was designed to address possible sources of observed distress.

Test Pit Excavation

Two test pits were excavated to determine the approximate design of the footing or foundation of the house and the depth of emplacement. The first test pit (TP-1) was excavated along the north exterior wall of the structure. The second test pit (TP-2) was excavated along the south exterior wall of the garage (see marked locations on the Site Plan map).

Floor Elevation Survey

Differential elevation of a structure may be defined as the difference in elevation between any two points on the interior floor of the structure. The American Concrete Institute (ACI) lists a tolerance of 0.5 inches over a 10 feet horizontal distance for conventional slabs. Maximum overall tolerances for tops of slabs are placed at plus or minus 0.75 inches (1.5 inches total differential). The floor elevation survey was conducted with an R & A Products "Pro-Level" manometer.

FIELD TEST METHODS: GEOPHYSICAL SURVEYS

Ground Penetrating Radar

Ground penetrating radar (GPR) is a geophysical procedure employed to detect and identify subsurface features and conditions characterized by a contrast in dielectric properties. This technique involves the transmission, from a receiver-

transmitter antenna system that is pulled along the ground surface, of microwave radiation into the ground. Subsurface contrasts in the dielectric properties of varying materials present a surface from which reflections are generated. Accordingly, contacts between rock types, physical features such as cavities or disrupted sedimentary layers, and/or man-made objects such as metallic barrels or pipes cause reflections that are recorded at the surface.

The intensity of the reflected signal is affected by the contrast in dielectric properties of materials, the electromagnetic conductivity of the medium through which the waves traverse, and the frequency of the signal. Digital signals are recorded and stored in a recorder for on-site visual color display or subsequent transferal to a computer for careful analysis and printing. The radar survey was conducted in general accordance with ASTM Standard D6432-99.

A Geophysical Survey Systems, Inc., (GSSI) SIR System-3000 radar was used. This is a portable, digital radar signal recorder. A 400-megahertz transceiver antenna was used with a two-way travel time range of 100 to 125 nanoseconds. Penetration depths for GPR signals are a function of lithology type (greater signal attenuation in clayey materials or water saturated conditions) and frequency (greater signal attenuation in higher frequency antenna systems). Actual depths of penetration vary from site to site. Based on the near-surface materials, the depth capability at this site was approximately 6 to 10 feet, but actual penetration is variable.

A total of 41 GPR traverses were conducted at the Killin residence. As shown on the GPR location map, the configuration and distribution of the traverses were designed to provide representative coverage of the site of investigation.

Electrical Resistivity

Electrical resistivity (ER) is a geophysical procedure to investigate the presence of geological conditions or features characterized by contrasts in electrical resistivity. The measurements were conducted using the Wenner electrode configuration, and were performed in general accordance with the appropriate portions of ASTM standards G57-95a entitled "Standard Test Method for Field Measurement of Soil Resistivity Using the Wenner Four-Electrode Method," and standard D6431-99 "Standard Guide for Using Direct Current Resistivity Method for Subsurface Investigations."

Electrical resistivity measurements involve the passing of an electric current underground and measuring its resistance to flow. Different earth materials (e.g. clay, sand, limestone) and subsurface cavities will resist the flow of electrical current differently. Substantially greater contrasts in the degree of resistance (anomalies) are used to identify and locate boundaries among different materials as well as the presence of cavities.

The types of ER measurements used in this investigation were Soundings and Lee-directional. Sounding measurements reveal two-dimensional detail below the surface at progressively greater depths. Lee-directional measurements determine the direction of higher or lower resistivity along a traverse line. In the field, electrodes are placed in the ground at equal distances from one another. After a measurement, this distance is increased in an orderly fashion to sequentially allow a greater depth of penetration.

Measurements of ER were made with an L and R Instruments MiniRes Earth Resistivity Meter. Four current/potential electrodes and one Lee electrode are employed. Depending on the surface space available for deployment of electrodes, a maximum depth capability of 100 feet can be achieved.

ER traverse lines were oriented to provide representative coverage of the site of investigation (see ER location map). Six traverses were measured at the Killin residence, configured as shown on the location map. Maximum depth of penetration ranged from 30 to 60 feet.

RESULTS

Hand Auger Borings

1. The locations of the hand auger borings are shown on the Site Plan map. The results of the auger borings are shown on the Hand Auger Investigation profiles in the appendix. Unless noted otherwise, each of the hand auger borings were terminated at approximately 5 feet depth.
2. Hand auger boring HA-1 penetrated brown fine sand within the upper 6 inches overlying sandy clay to 1.5 feet depth and sand to 2 feet depth. Green and blue

sandy fat clay was encountered from 2 to 5 feet depth. Sample HA-1-1 was taken at approximately 2 feet depth in boring HA-1.

3. Hand auger boring HA-2 penetrated brown fine sand within the upper 2 feet depth. Sample HA-2-1 was taken at approximately 2 feet depth. Hand auger boring HA-2 was terminated at approximately 2 feet depth due to a refusal on roots.
4. Hand auger boring HA-3 penetrated light brown fine sand within the upper 4.5 feet depth overlying light gray clayey sand. Sample HA-3-1 was taken at approximately 5 feet depth in boring HA-3.
5. Hand auger boring HA-4 penetrated light brown fine sand within the upper 2.5 feet depth overlying light brown clayey sand. Grayish green sandy clay was encountered from 4 to 4.5 feet depth overlying green fat clay with sand. Sample HA-4-1 was taken at approximately 4.5 feet depth.

Laboratory Analyses

1. The results of the laboratory analyses are shown in the Summary of Laboratory Results. Samples HA-1-1 and HA-4-1 were selected for analyses.
2. Sample HA-1-1, taken from approximately 2 feet depth in HA-1, is classified as sandy fat clay (CH) with 66.7% of the material passing the No. 200 mesh sieve, a natural moisture content of 42.9%, and a plasticity index of 44.
3. Sample HA-4-1, taken from approximately 4.5 feet depth in HA-4, is classified as fat clay with sand (CH) with 75.7% of the material passing the No. 200 mesh sieve, a natural moisture content of 44.7%, and a plasticity index of 74.
4. Materials with a plasticity index above 35 are considered to be highly plastic and a significant potential for unstable behavior. Samples HA-1-1 and HA-4-1 fall into this range.

Static Cone Penetration Tests

1. Graphical depictions of the hand cone penetrometer results are attached. The results are interpreted as indicative of very loose to loose materials (very low to low bearing strength) at the thirteen penetrometer stations.

Test Pit Excavations

1. Test Pit one (TP-1) was excavated along the north exterior wall of the structure (photograph #13). TP-1 revealed a foundation embedment of at least 16 inches below grade.
2. Test Pit two (TP-2) was excavated along the south exterior wall of the garage (photograph #14). TP-2 revealed a foundation embedment of 16 inches below grade.
3. Current standard construction practices for this area call for a minimum depth of embedment of 12 inches.

Ground Penetrating Radar

1. Ground penetrating radar (GPR) signals at the Killin residence were interpreted as generally horizontally layered reflectors throughout the depth of penetration. Attenuation of the radar signal was experienced throughout the Killin property. The attenuation is likely due to the presence of the near-surface water saturated and clayey materials.
2. No GPR signals recorded at the site were interpreted as indicative of dipping reflectors, disturbed sediments, cavities or other features consistent with possible sinkhole activity.

Electrical Resistivity

1. In general, near-surface resistivity values and sounding patterns varied slightly among the six traverses. Sounding profiles are included in the appendix.

2. The configurations of the sounding values and patterns are interpreted as indicative of surficial sand and clayey sand grading into more clayey materials at approximately 10 to 25 feet depth and back into more sandy materials at approximately 20 to 35 feet depth.
3. Electrical evidence of the underlying limestone surface was detected at approximately 60 feet depth beneath ER traverse #6.
4. Lee-directional measurements (not plotted) yielded disparities on four of the six traverses. The locations of the Lee-directional disparities are shown in yellow on the ER location map. The directional disparities were not corroborated with sounding anomalies, and may be attributed to lateral changes in soil composition and moisture, or to the presence of buried utilities.

Floor Elevation Survey

The floor elevation survey is attached. The lowest elevations of the living area occurred within the western and southern portions of the structure. These areas have a total elevation difference of 1.2 inches over an approximate 13 feet horizontal distance. This difference in elevation exceeds 0.5 inches over 10 feet horizontal distance and, accordingly, exceeds tolerances established by the American Concrete Institute.

A separate floor elevation survey was completed for the garage. The lowest elevations in the garage occurred within the northeast corner. The garage exhibited a total elevation difference of approximately 0.7 inches.

Structural Evaluation-Site Observations

For purposes of orientation in this section the front door is assumed to be on the south side.

The current homeowner purchased the house, built in 2000, in 2006. Exterior walls of the single-story structure are of wood frame construction with brick veneer on three sides and vinyl siding in the back, supported on a stemwall foundation. According to the homeowner, distress, in the form of interior cracks, was first noticed at the time of occupancy.

Interior Observations

Cracks of up to 3/8" in width with vertical displacements of up to 1/8" are visible in the floor slab of the living room and the adjacent air handler closet. Hairline cracks are visible in the floor tiles in the kitchen, the laundry room, and the bathrooms. Hairline cracks are visible in the walls and ceilings of several rooms. Cracks of up to 1/16" in width are visible in the garage floor slab.

Exterior Observations

A vertical crack of up to 3/16" in width is visible below the south window in the east wall. A crack of up to 1/16" in width is visible near the south top corner of the north window in the east wall. A hairline crack is visible near the north top corner of the north window in the east wall. A crack of up to 1/8" in width is visible near the south lower corner of the north window in the east wall. A crack of up to 1/16" in width is visible in mortar joints near the south top corner of the overhead door. A hairline crack is visible in the brick veneer near the east lower corner of the west window in the south wall. A crack of up to 1/16" in width is visible in mortar joints near the west end of the front porch header. Cracks of up to 1/16" in width are visible in the brick veneer near the northwest corner of the front porch. Cracks of up to 1/16" in width are visible in the front porch slab.

Structural Evaluation-Findings and Recommendations

- No evidence of significant loss of structural integrity is noted at this time.
- Evidence of minor structural distress is noted in the form of widespread cracking and locally excessive variations in floor elevation.
- The observed distress is consistent with distress caused by differential movements. Such movements may be attributed to the potential sinkhole activity and the presence of near-surface expansive clays identified in our investigation.
- Cosmetic repairs should be started no sooner than sixty days after completion of the recommended foundation remediation program.

Standard Penetration Tests

1. Boring B-1 was located 50 feet north and 22 feet west of the northeast corner of the structure (see Site Plan map), near the northern surface depression. This boring penetrated 18.5 feet of sand and clayey sand overlying sandy clay. Samples were not collected from 4 to 8 feet depth due to a plastic obstruction in the spoon. Silty sandy was encountered from 28.5 to 59.5 feet depth overlying limestone. A cavity was encountered from 83.5 to 85.5 feet depth within the limestone. Boring B-1 was terminated in limestone at approximately 100 feet depth.
2. N-values (blows per foot) for boring B-1 ranged from $N = 7$ to $N = 18$ within the upper 10 feet of drilling. Weight-of-rod conditions were experienced from 83.5 to 85.5 feet depth and from 88.5 to 89 feet depth. Refusal conditions ($N > 50/6$ in.) were recorded at the 55, 75 and 100 feet depth sample intervals. Complete loss of drilling fluid circulation, without recovery, was experienced at 68 feet depth.
3. Boring B-2 was located 6 feet south and 16 feet east of the northeast corner of the structure (see Site Plan map), near an area of distress. This boring penetrated 23.5 feet of sand, silty sand, sandy clay, and clay. Silty sand was penetrated from 23.5 to 63.5 feet depth overlying limestone. Boring B-2 was terminated in limestone at approximately 99.5 feet depth.
4. N-values for boring B-2 ranged from $N = 9$ to $N = 24$ within the upper 10 feet of drilling. No weight-of-rod or weight-of-hammer conditions were experienced in boring B-2. Refusal conditions were recorded in limestone at the 65, 95, and 100 feet depth sample intervals. Complete loss of drilling fluid circulation, without recovery, was experienced at 72 feet depth.
5. Boring B-3 was located 11 feet west and 20 feet south of the northwest corner of the structure (see Site Plan map), near the southern depression and an area of distress. This boring penetrated 78.5 feet of sandy and clayey materials overlying limestone. Boring B-3 was terminated in limestone at 100 feet depth.
6. N-values for boring B-3 ranged from $N = 8$ to $N = 31$ within the upper 10 feet of drilling. Numerous weight-of-rod conditions (1 to 2 feet) were recorded between 53.5 and 84.5 feet depth. Refusal conditions were not recorded in boring B-3. Complete loss of drilling fluid circulation, without recovery, was experienced at 50 feet depth.

CONCLUSIONS

The Killin residence is located at 172 NW Kelley Lake Court, Lake City, Florida. This site includes a single story, wood frame structure, built in 2000. Mr. Killin reportedly first noticed minor distress in 2006. He stated that he discovered cracks in the concrete slab in the living room when he removed the carpeting in May, 2008. Minor widespread distress was observed in the interior and exterior of the Killin residence. Shallow surface depressions were present to the west and north of the residence. Standard penetration test borings B-1 and B-3 were located to further investigate the nature of the depressions.

Hand auger borings penetrated sands and clayey materials within the upper 5 feet depth in the four borings. Laboratory analyses also identified highly plastic clayey materials in two of the hand auger borings (HA-1 and HA-4). These materials are considered to have a significant potential for unstable behavior. Static hand cone penetrometer results indicate that very loose to loose soils are present within the upper four feet around the perimeter of the structure.

Electrical resistivity results are indicative of sands and clayey materials overlying limestone at approximately 60 feet depth. No GPR signals recorded at the site were interpreted as indicative of dipping reflectors, disturbed sediments, cavities or other features consistent with possible sinkhole activity.

The floor elevation survey revealed a total interior elevation difference of 1.2 inches for the living area. The test pit excavations revealed the foundation embedment in accordance with current construction codes (at least 16 inches in TP-1 and 16 inches in TP-2). The structural evaluation yielded no evidence of significant loss of structural integrity.

Three SPT borings were conducted at the Killin residence. Limestone was initially encountered at depths ranging from 59.5 to 78.5 feet in the three borings. The variability in depth to limestone is indicative of a paleosink environment underlying the Killin property. Multiple weight-of-rod conditions, ranging from 1 to 2 feet of vertical extent, were recorded above the upper limestone surface in boring B-3. These loose conditions are interpreted as indicative of possible raveling. Raveling is the vertical or lateral migration of sediments into cavities in more distant or deeper limestone. It is a mechanism for sinkhole formation. Raveling is also evidence that the paleosink may be in a state of reactivation. Weight-of-rod conditions also defined a cavity in limestone in boring B-1 from

83.5 to 85.5 feet depth. Complete loss of drilling fluid circulation was experienced in all three SPT borings.

Based on the results of this investigation, Geohazards, Inc. is of the opinion that the distress at the Killin residence is due to natural aging of the structure, including material shrinkage and expansion, and to differential movements associated with the unstable behavior of near-surface highly plastic clayey materials and to the presence of tree roots in close proximity to the foundation. However, evidence of possible sinkhole activity (surface depressions, cavity in limestone, raveling, and loss of circulation) was detected at the Killin residence and sinkhole activity can not be eliminated as a contributing cause of distress.

CERTIFICATION

Compliance with Florida Statutes Section 627.707

In compliance with the above stated Florida Statute, this report was prepared under the direction and supervision of a Registered Professional Geologist, licensed in the State of Florida, whose field of expertise is geology and sinkhole evaluation, and with the participation of a Professional Engineer, licensed in the State of Florida. The geologist(s) and engineer(s) signature(s) and seal(s) with Florida Registration Number appear on the report.

It is our professional opinion, based on the information generated by this investigation, and by testing conducted in compliance with generally accepted scientific practices and with Chapter 627.7072, that the analyses conducted were of sufficient scope to determine that sinkhole activity can not be eliminated as a cause of damage within a reasonable professional probability.

LIMITATIONS

While due care has been exercised in the performance of these measurements and their interpretation, Geohazards, Inc. can make no representations, warranties, or guarantees with respect to latent or concealed conditions which may exist that may be beyond the limits of detection with the methodologies used. This report is prepared for the exclusive use of our clients and their assigns. Any use by other parties for any purposes is not authorized.

Marylea H. Kibilko
Marylea H. Kibilko, P.G. 10-17-08

Geologist

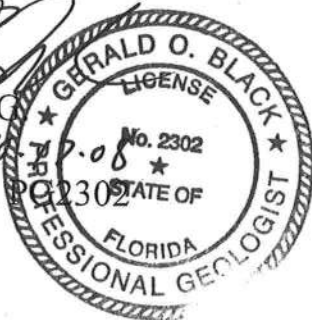
Florida License No. PG2506



Gerald O. Black
Gerald O. Black, P.G. 10-17-08

Geologist

Florida License No. PG2302



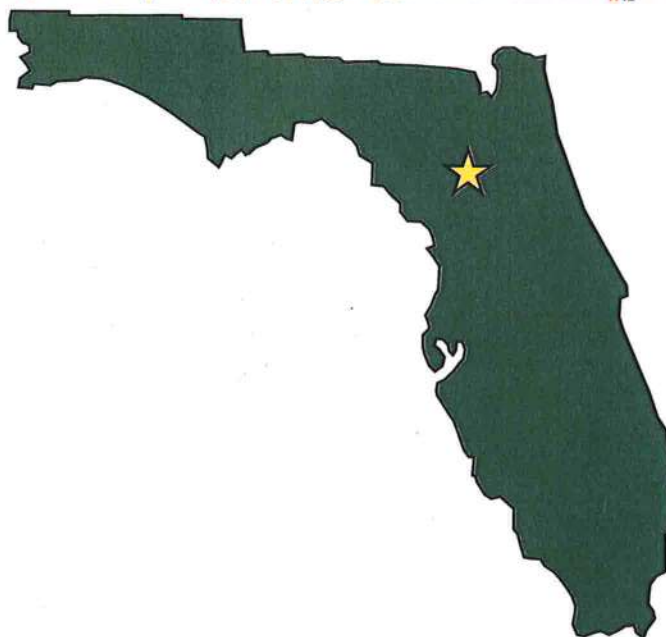
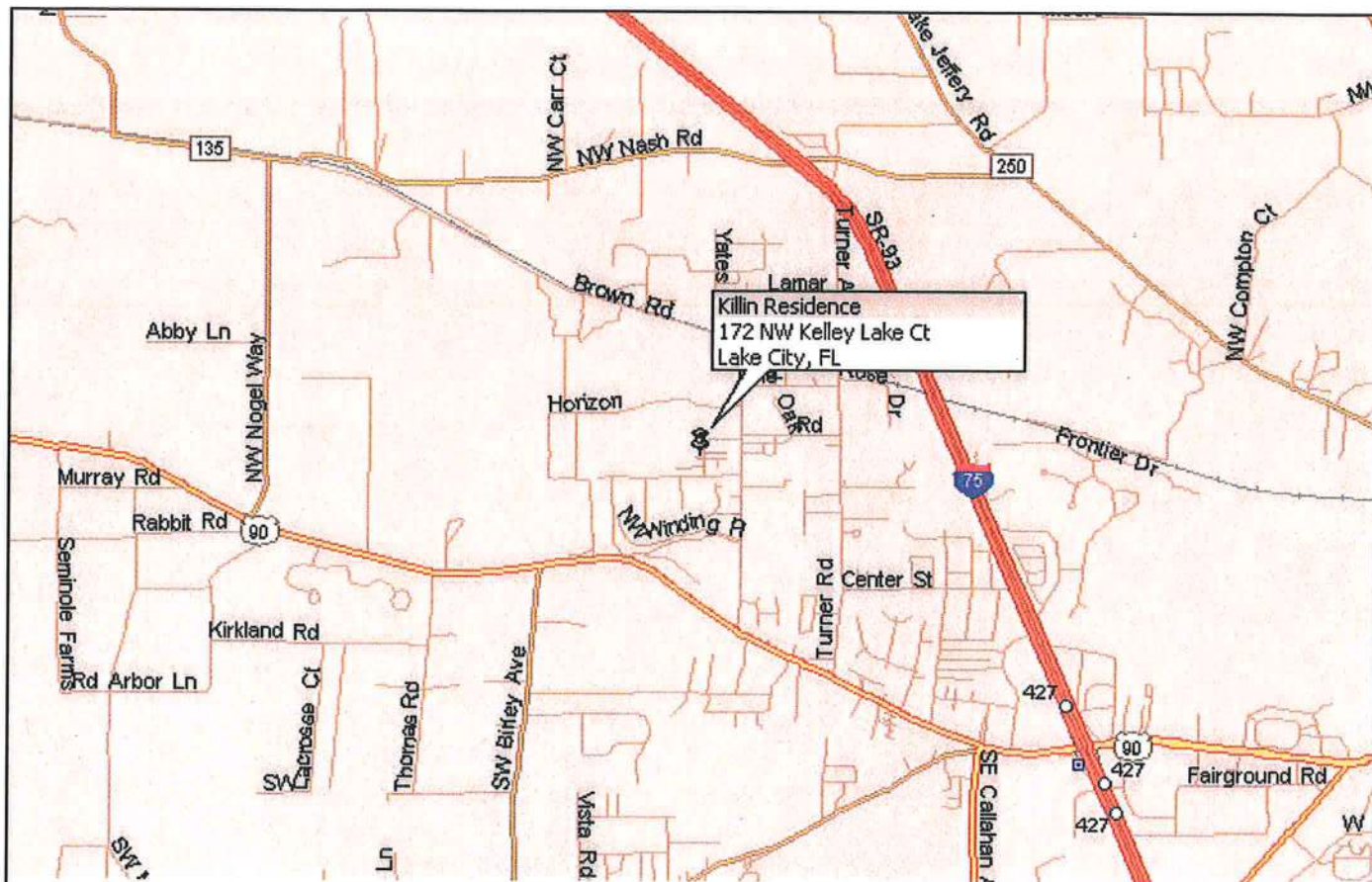
Attila A. Bodo
Attila A. Bodo, P.E. 10-16-08

Structural Engineer

Florida License No. PE15834

SELECTED REFERENCES

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SITE LOCATION MAP

Killin Residence
172 NW Kelley Lake Court
Lake City, Florida

Killin Residence

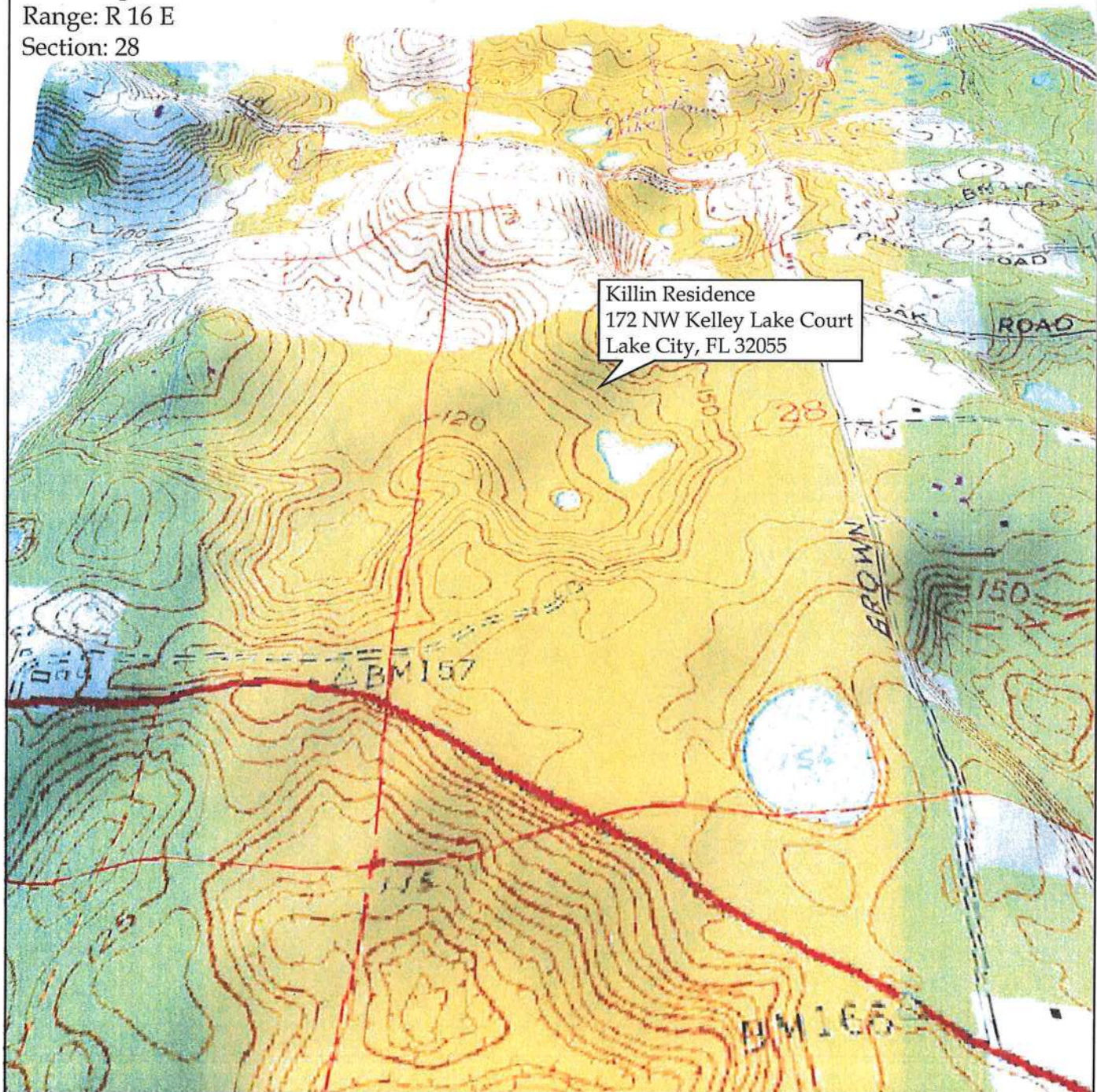
Elevation: 135 ft.

Quadrangle: Lake City West

Township: T 3 S

Range: R 16 E

Section: 28



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Three Dimensional Topographic Map

Killin Residence
172 NW Kelley Lake Court
Lake City, Florida

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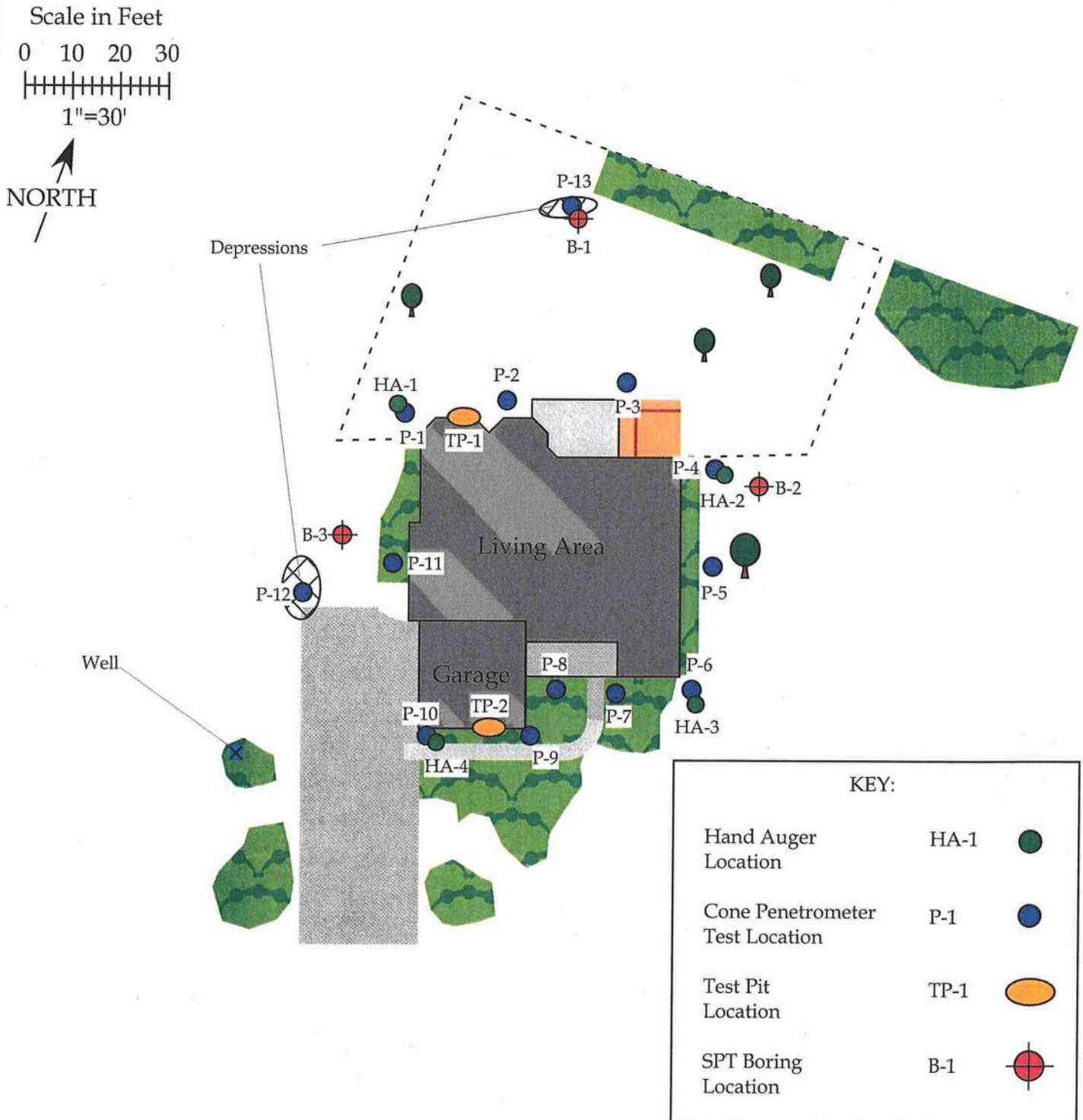
SITE PLAN

Killin Residence
172 NW Kelley Lake Court
Lake City, Florida

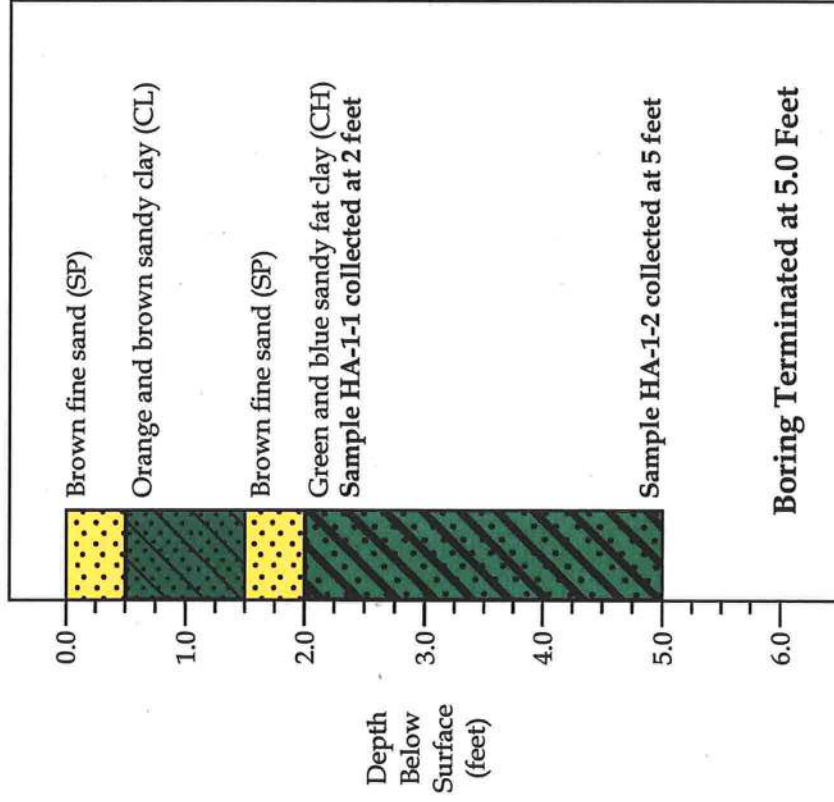
FOR: Florida Farm Bureau

DATE: 7-5-08

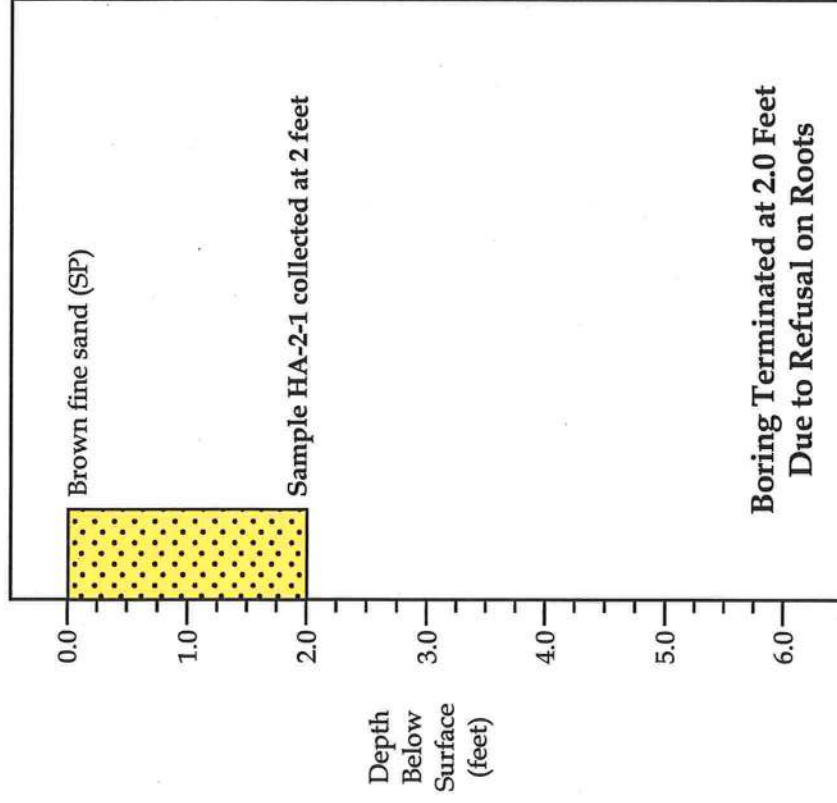
BY: W. Wrenn, Geologist
Investigation# 2008385



HA-1



HA-2



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HAND AUGER INVESTIGATION

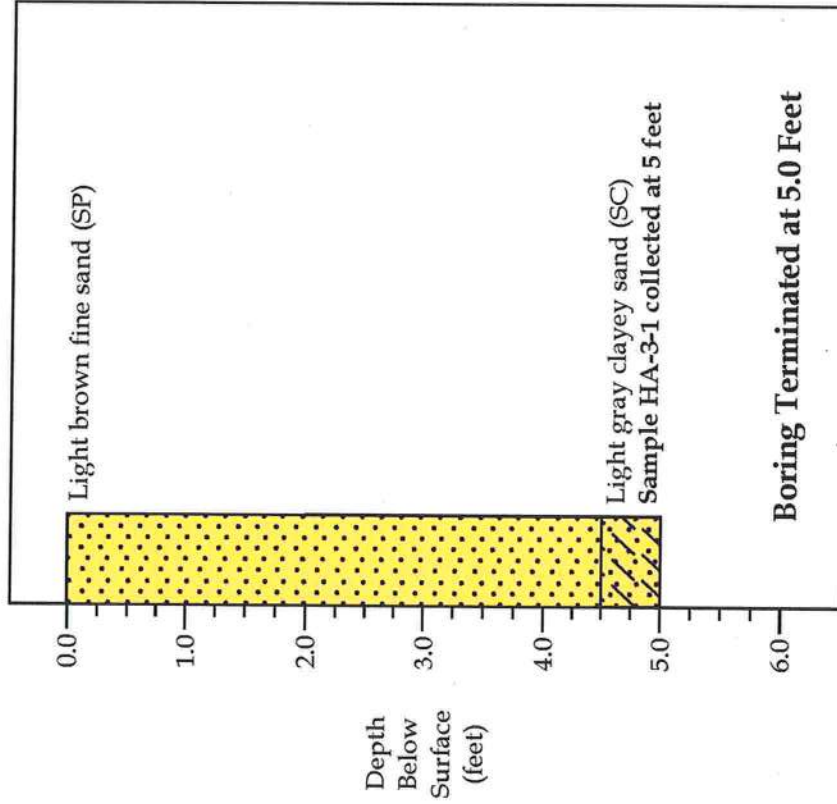
Killin Residence
172 NW Kelley Lake Court
Lake City, Florida

FOR: Florida Farm Bureau

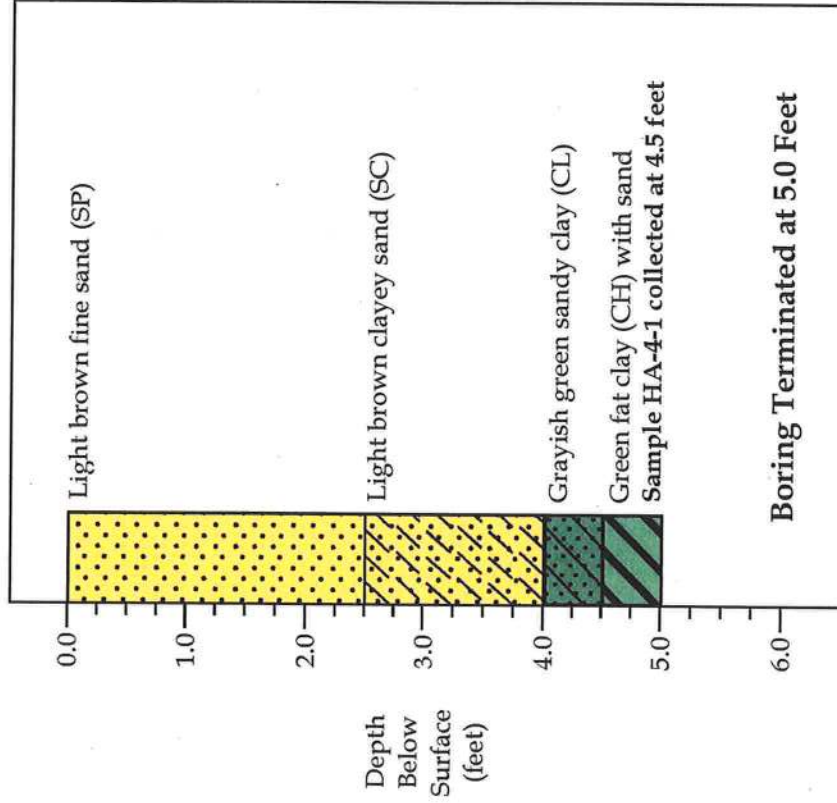
DATE: 6-18-08

BY: W. Wrenn, Geologist
Investigation# 2008385

HA-3



HA-4



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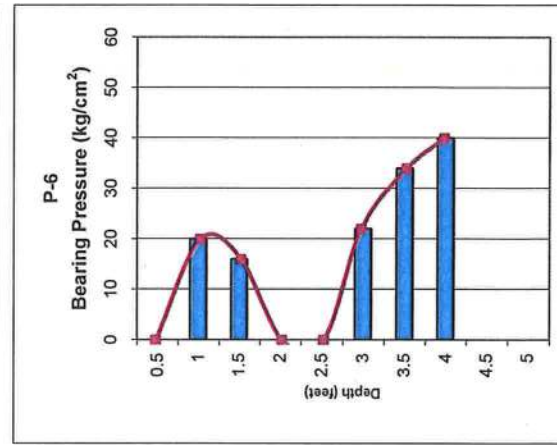
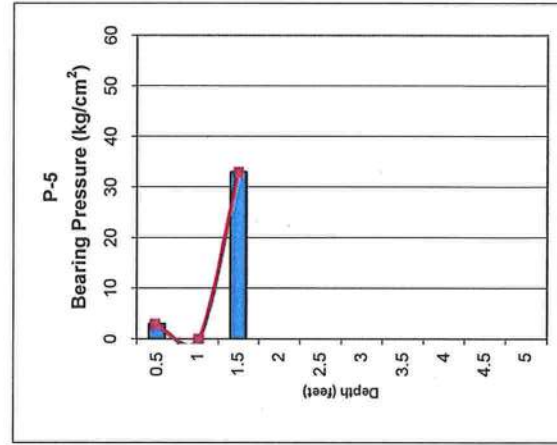
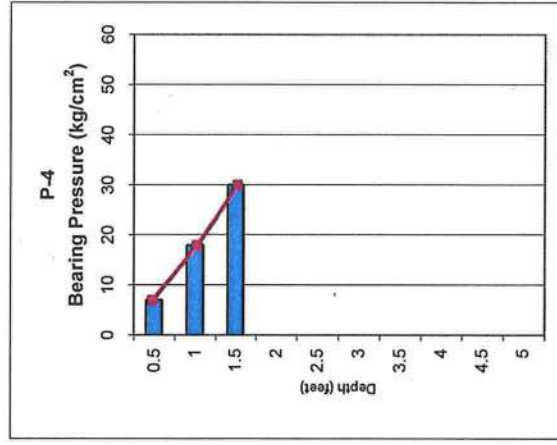
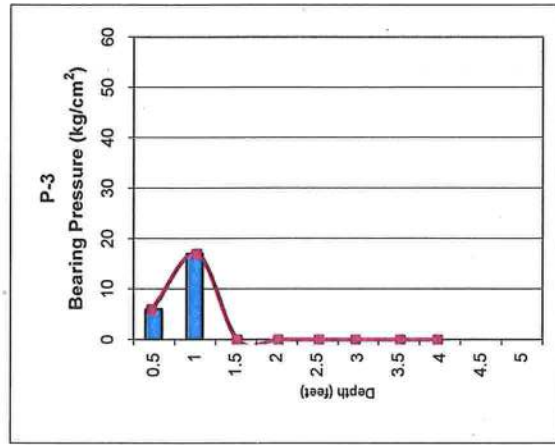
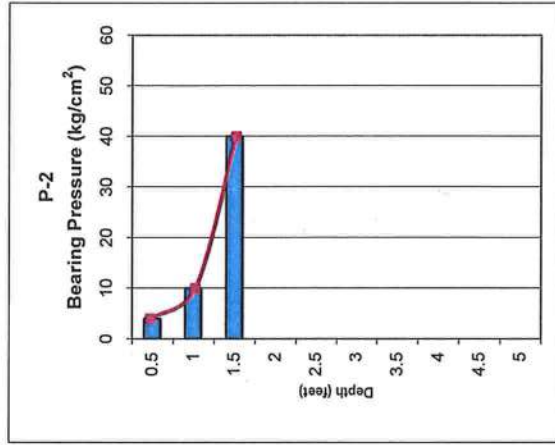
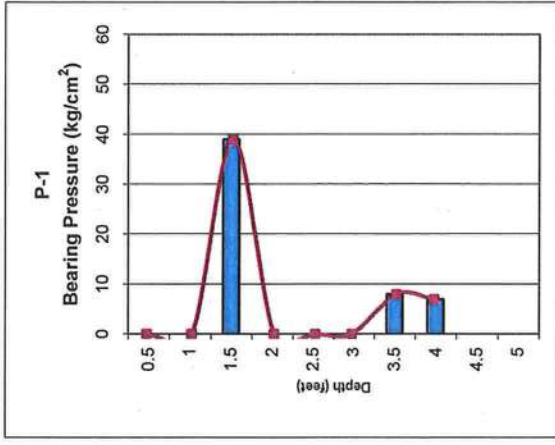
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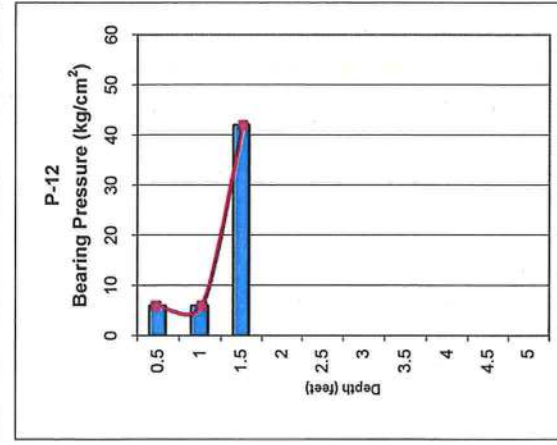
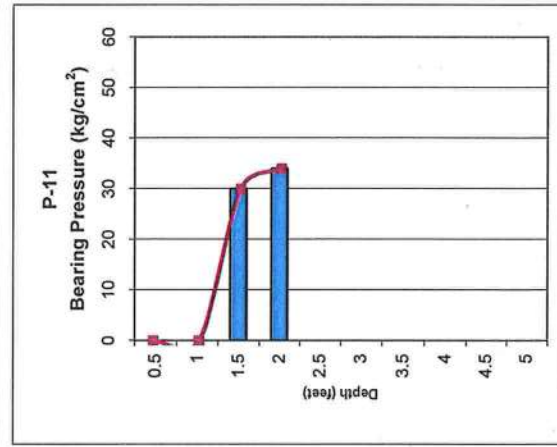
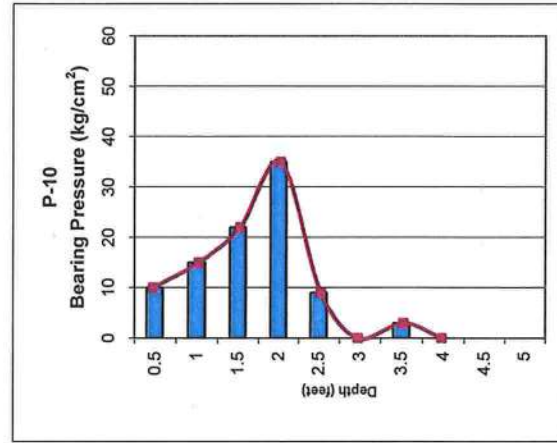
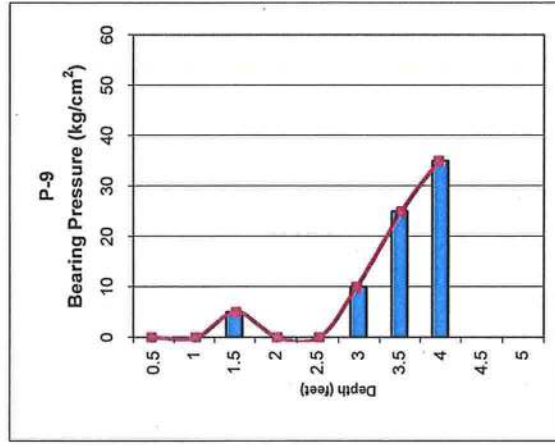
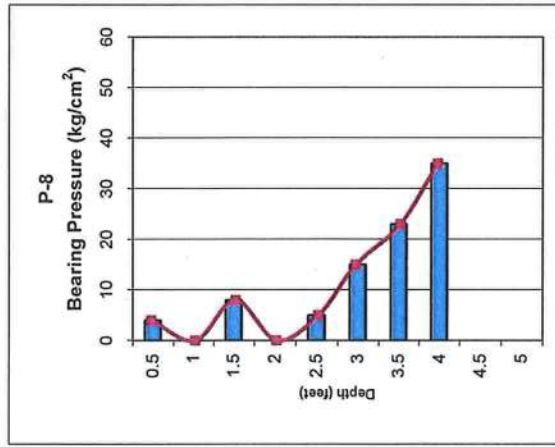
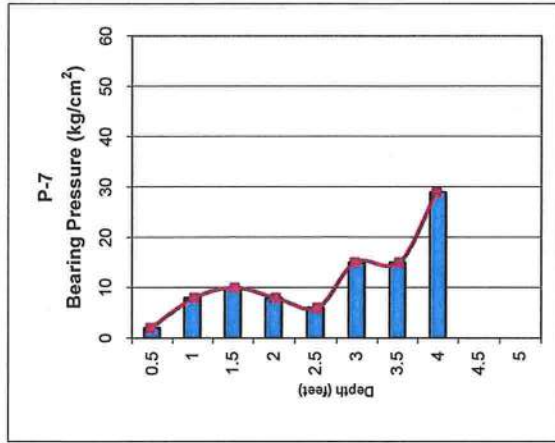
Killin Residence
172 NW Kelley Lake Court
Lake City, Florida

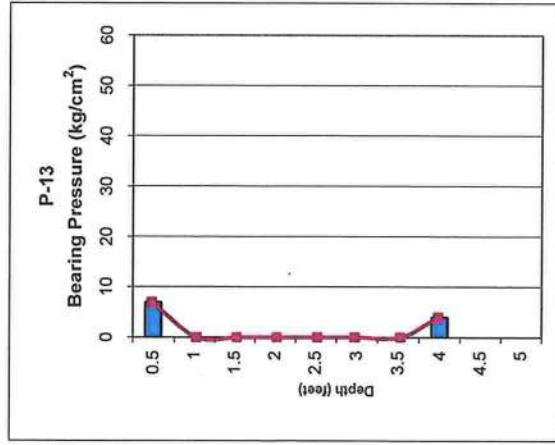
FOR: Florida Farm Bureau

DATE: 6-18-08

BY: W. Wrenn, Geologist
Investigation# 2008385







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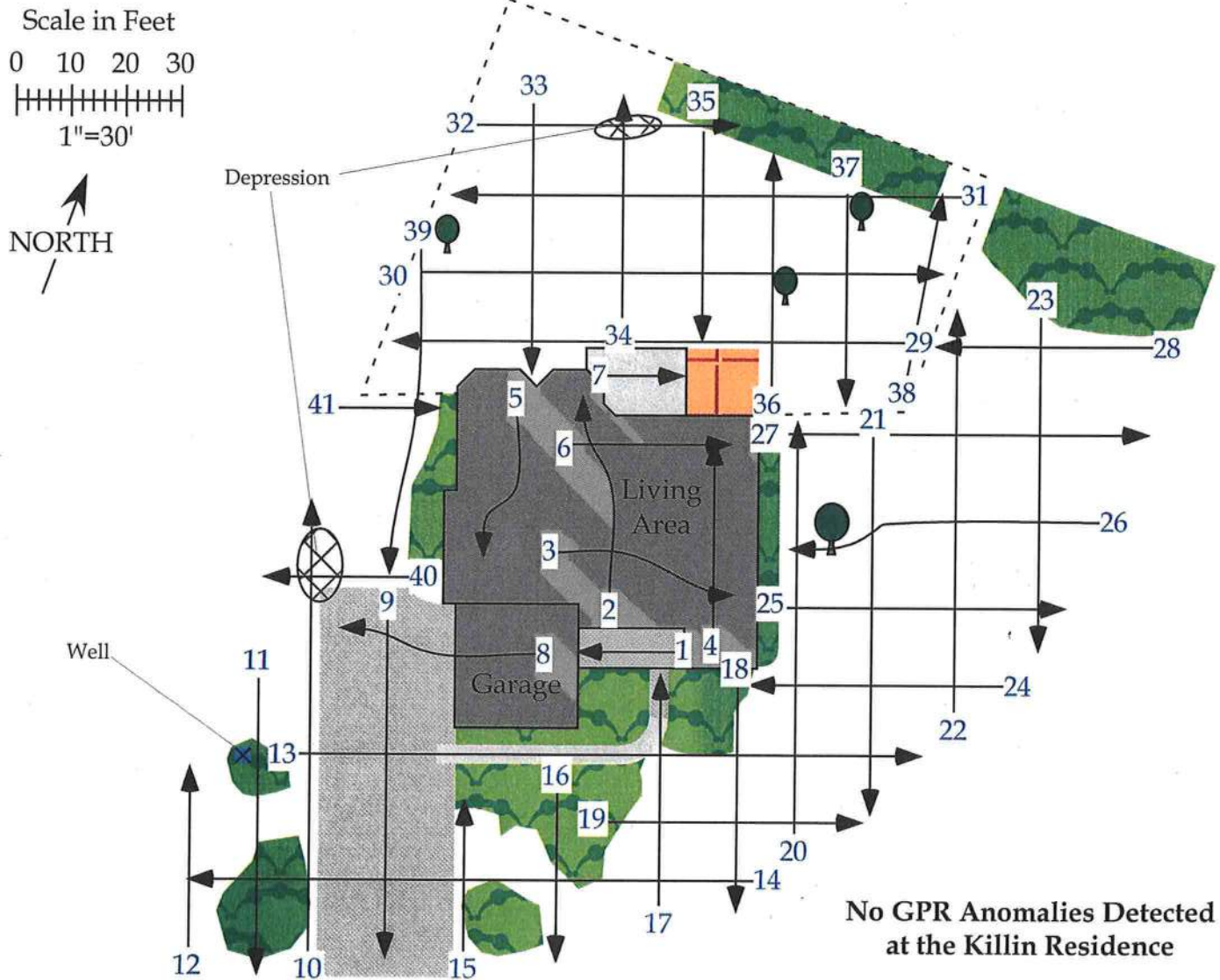
SITE PLAN OF GEOPHYSICAL INVESTIGATION GROUND PENETRATING RADAR SURVEY

Killin Residence
172 NW Kelley Lake Court
Lake City, Florida

FOR: Florida Farm Bureau

DATE: 6-19-08

BY: W. Wrenn, Geologist
Investigation# 2008385





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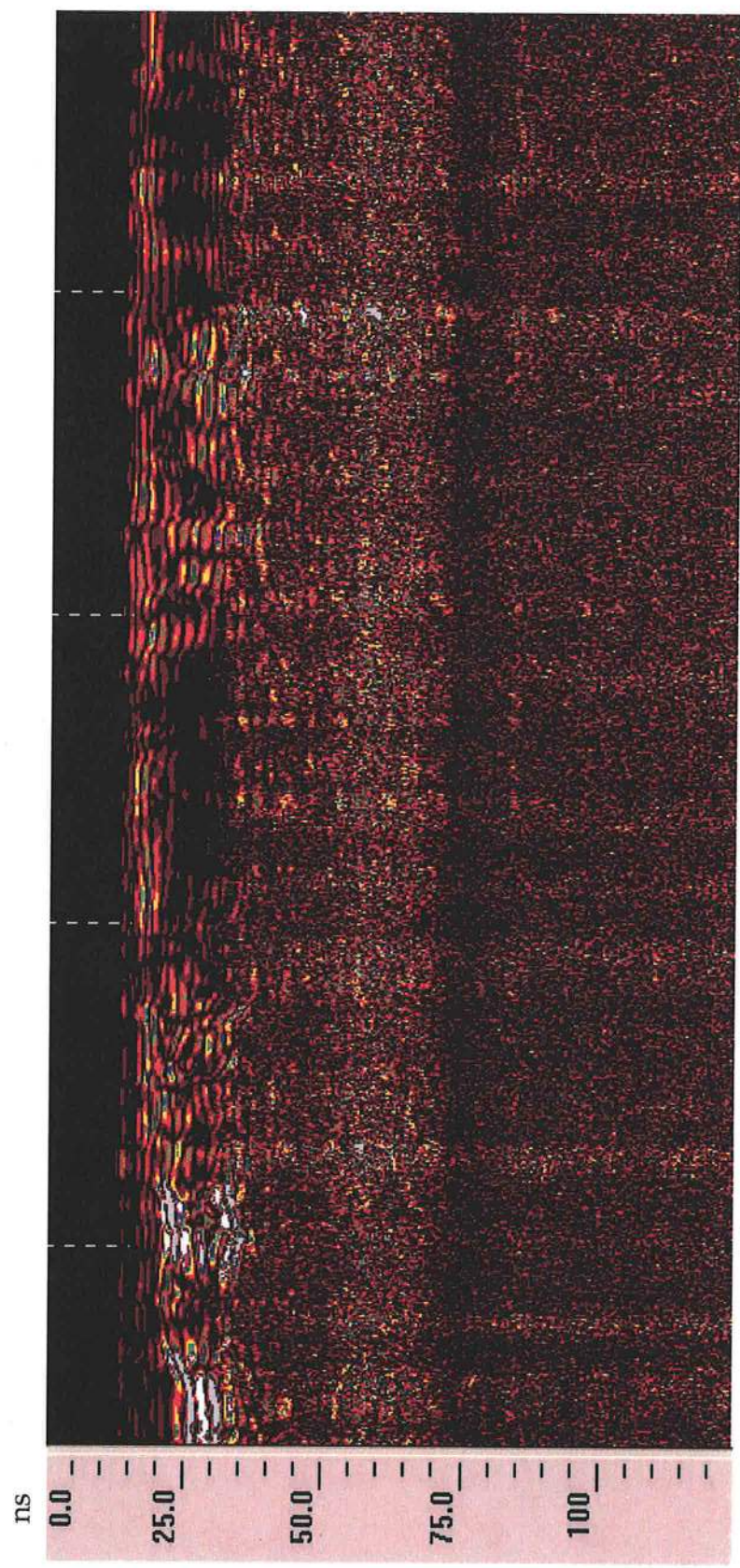
**GROUND PENETRATING
RADAR TRAVERSE #13**

Killin Residence
172 NW Kelley Lake Court
Lake City, Florida

Typical GPR Traverse at the
Killin Residence

System: SIR 3000
Antenna: 400 MHz
Range: 125 ns

Date: 6-19-08 Investigation #2008385



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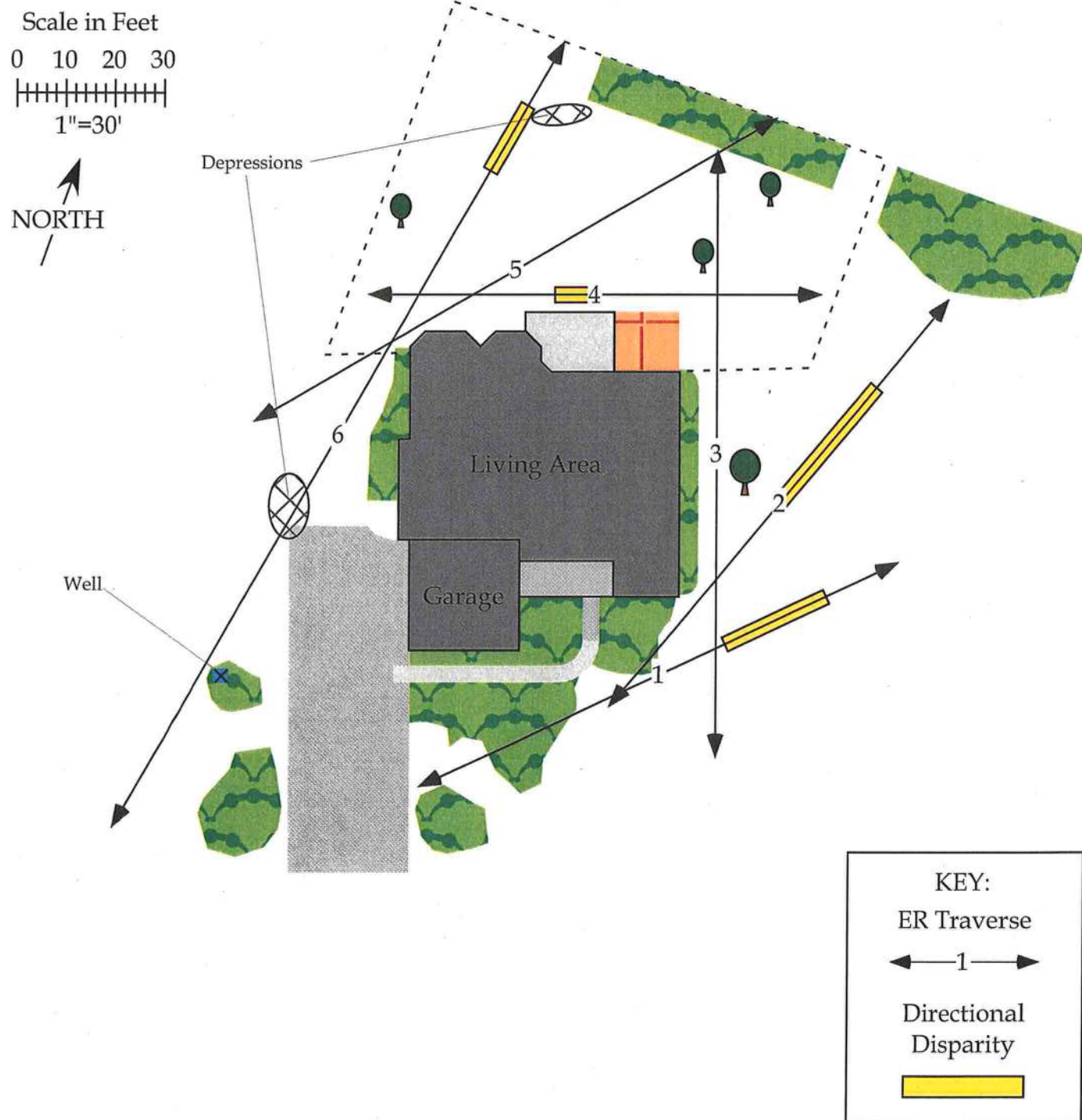
SITE PLAN OF GEOPHYSICAL INVESTIGATION ELECTRICAL RESISTIVITY SURVEY

Killin Residence
172 NW Kelley Lake Court
Lake City, Florida

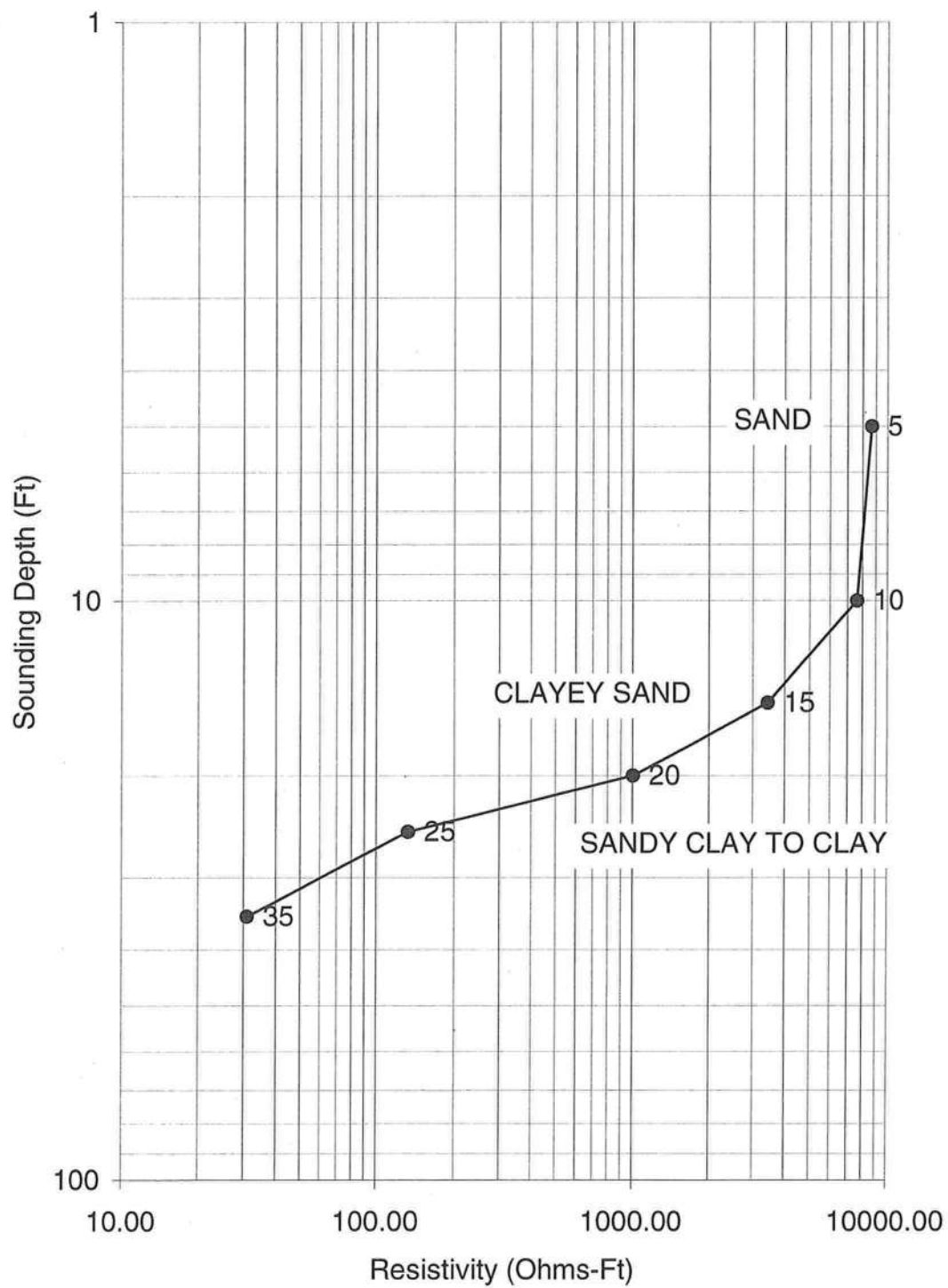
FOR: Florida Farm Bureau

DATE: 6-19-08

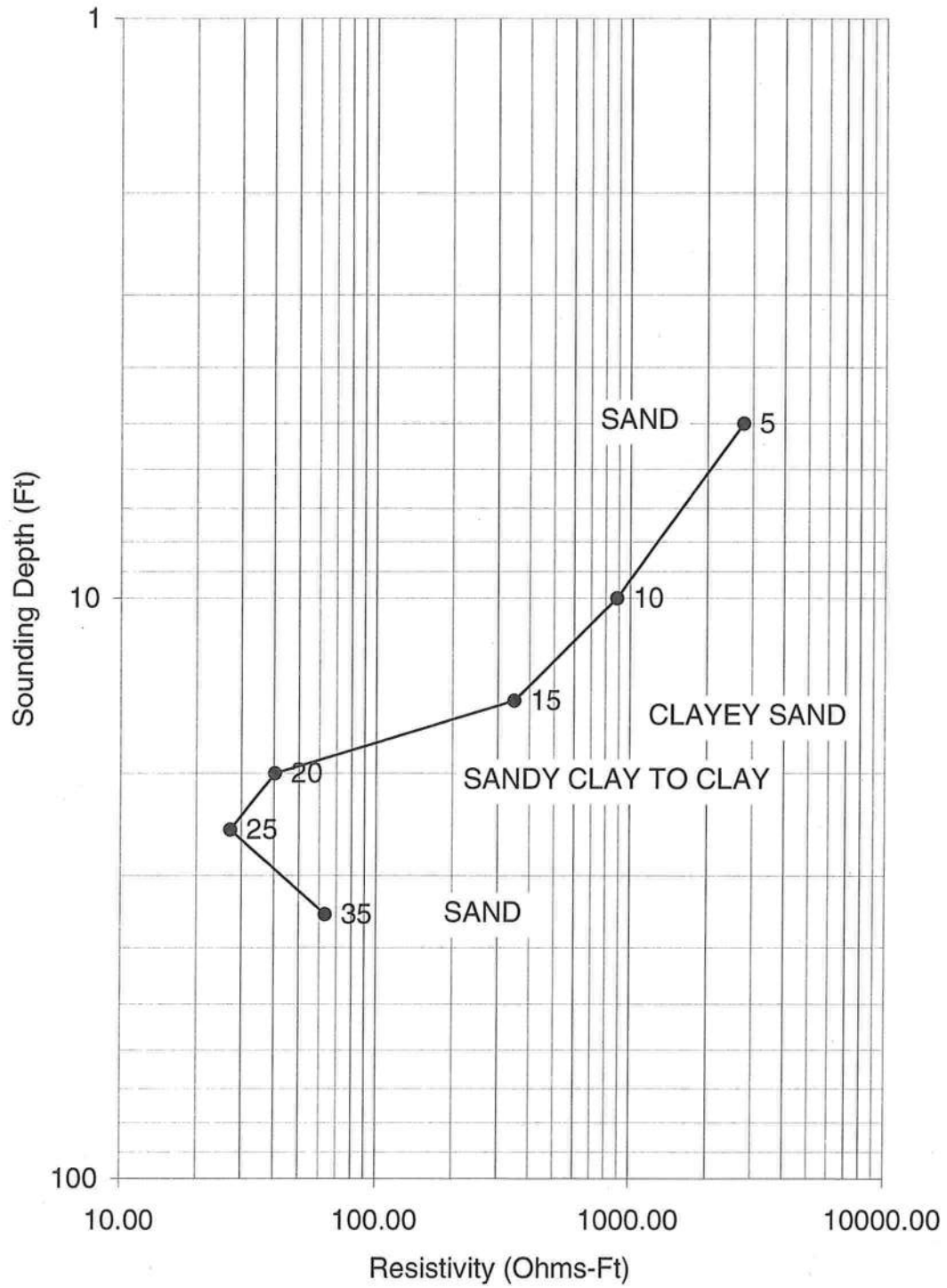
BY: W. Wrenn, Geologist
Investigation# 2008385

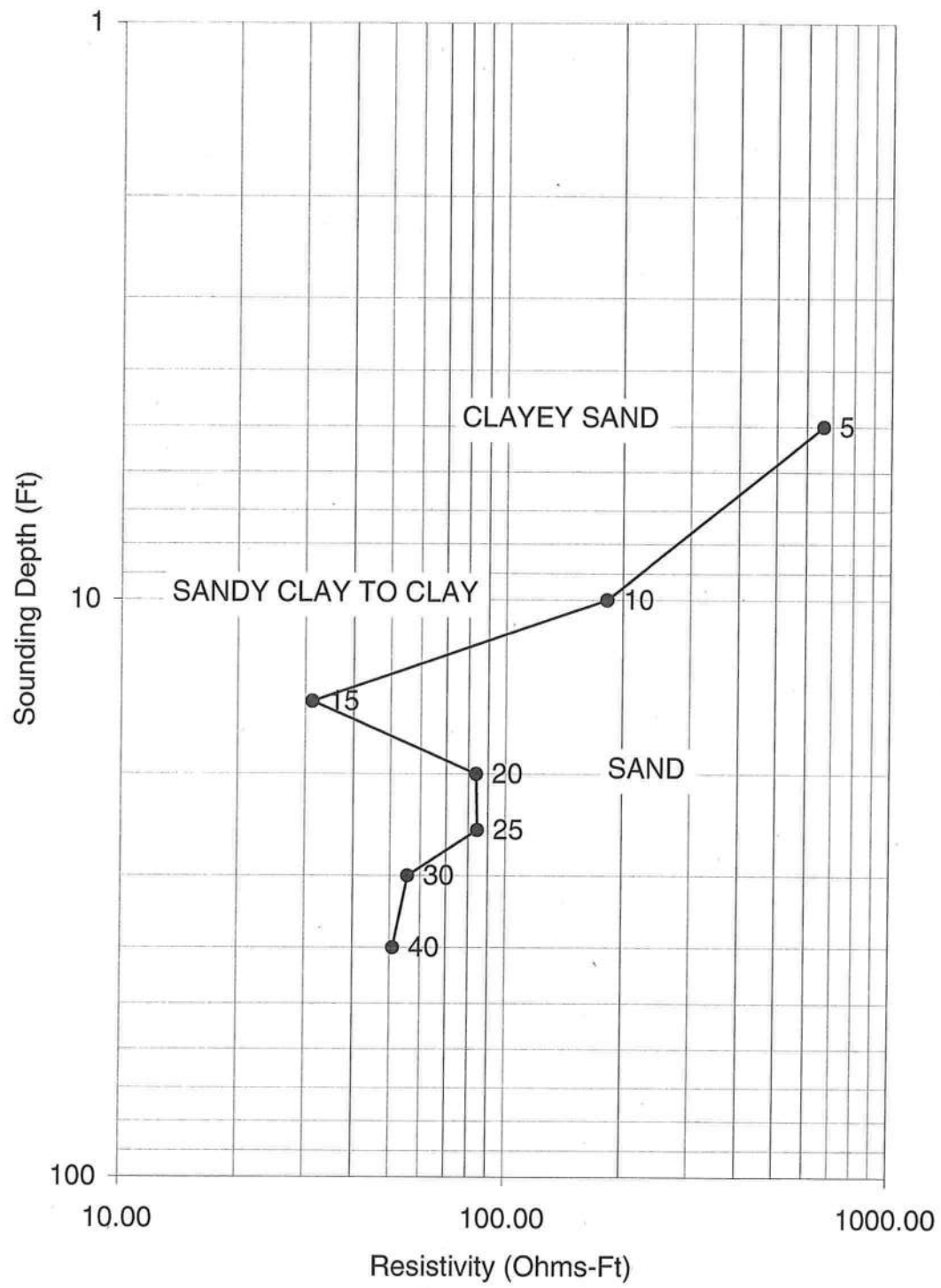


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Electrical Resistivity Survey
Investigation#:2008385
Array Orientation:N45E
Station Number: 1

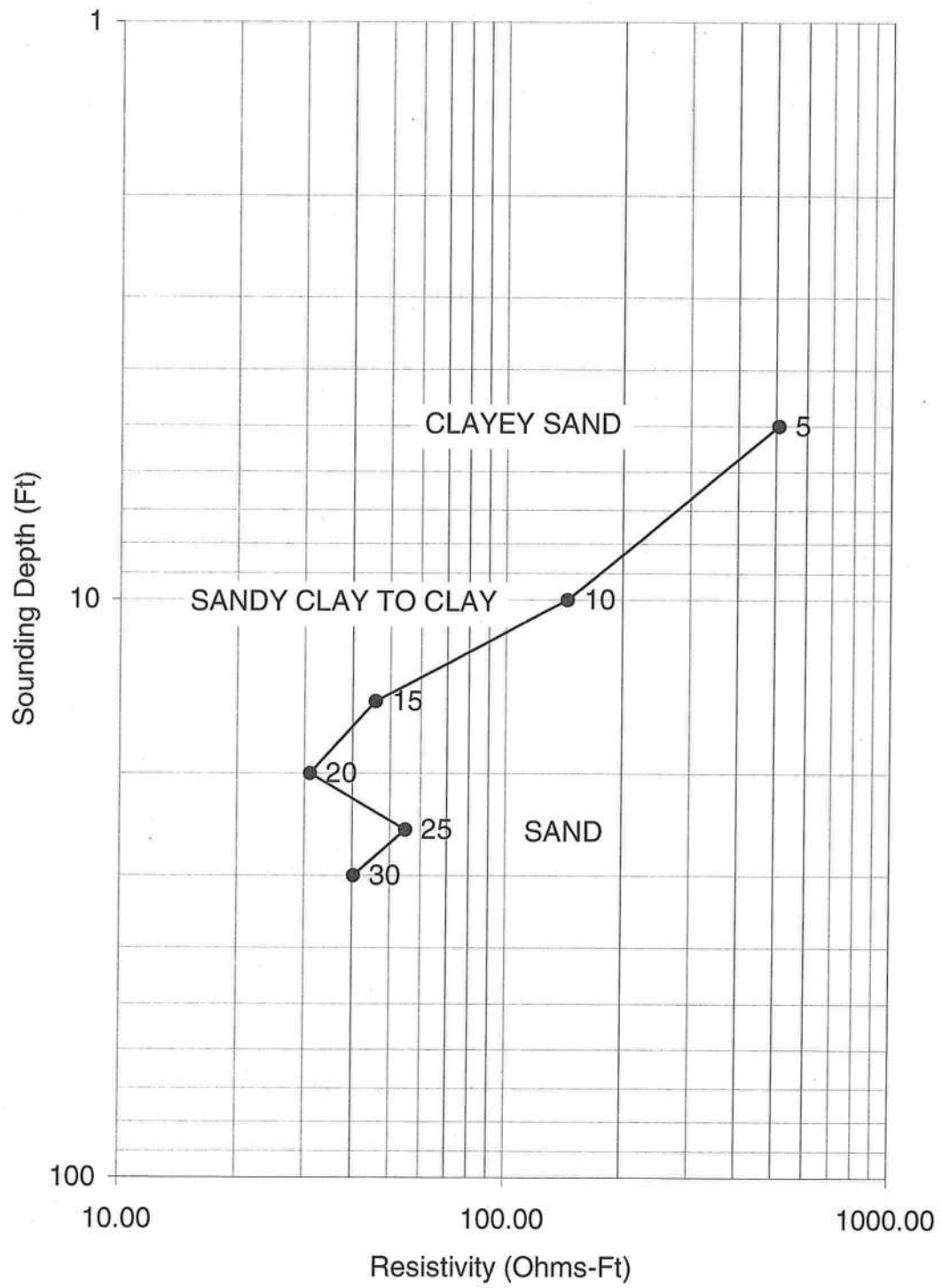


GEOHAZARDS INC.
Electrical Resistivity Survey
Investigation#:2008385
Array Orientation:N20E
Station Number: 2

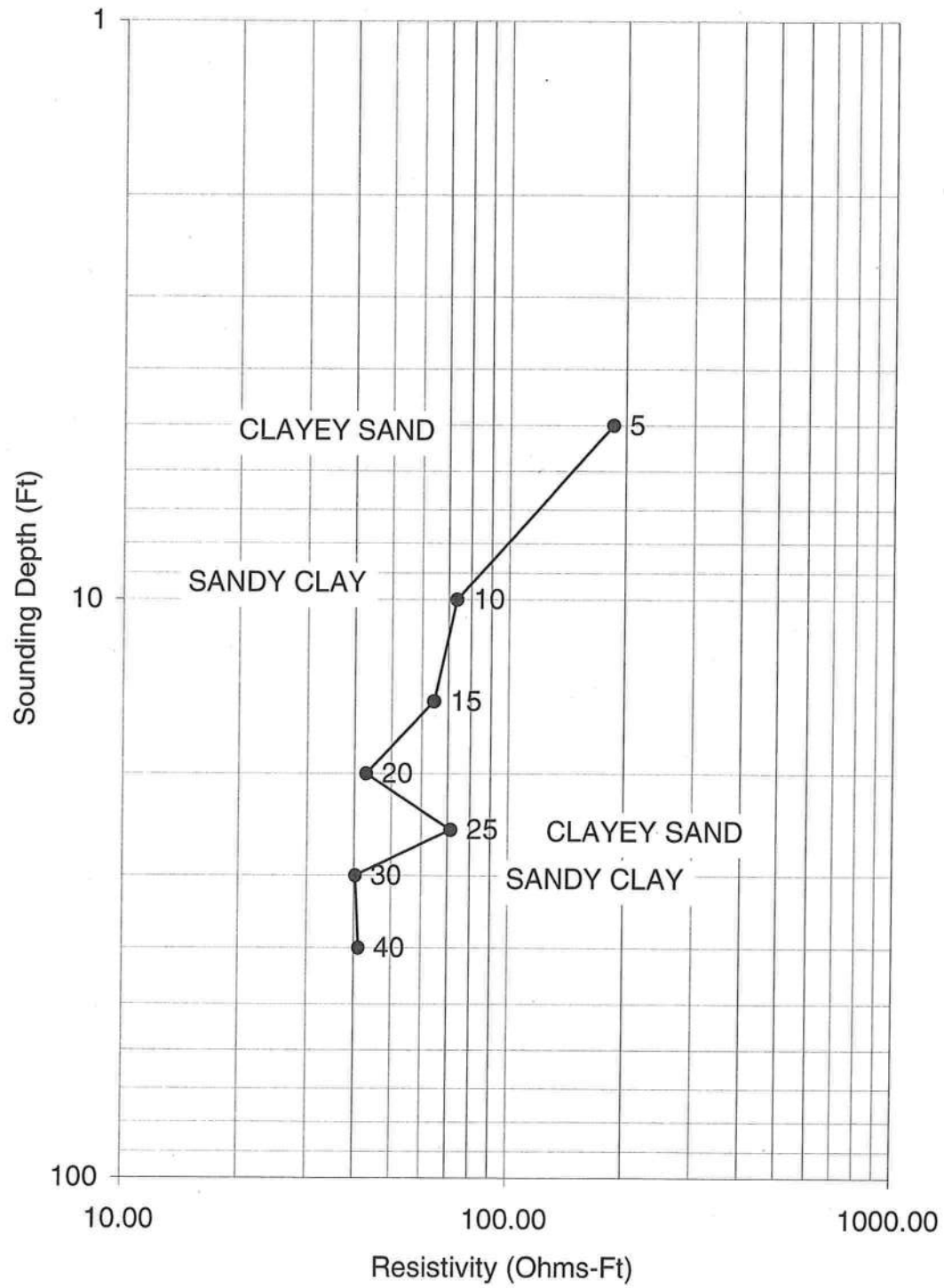


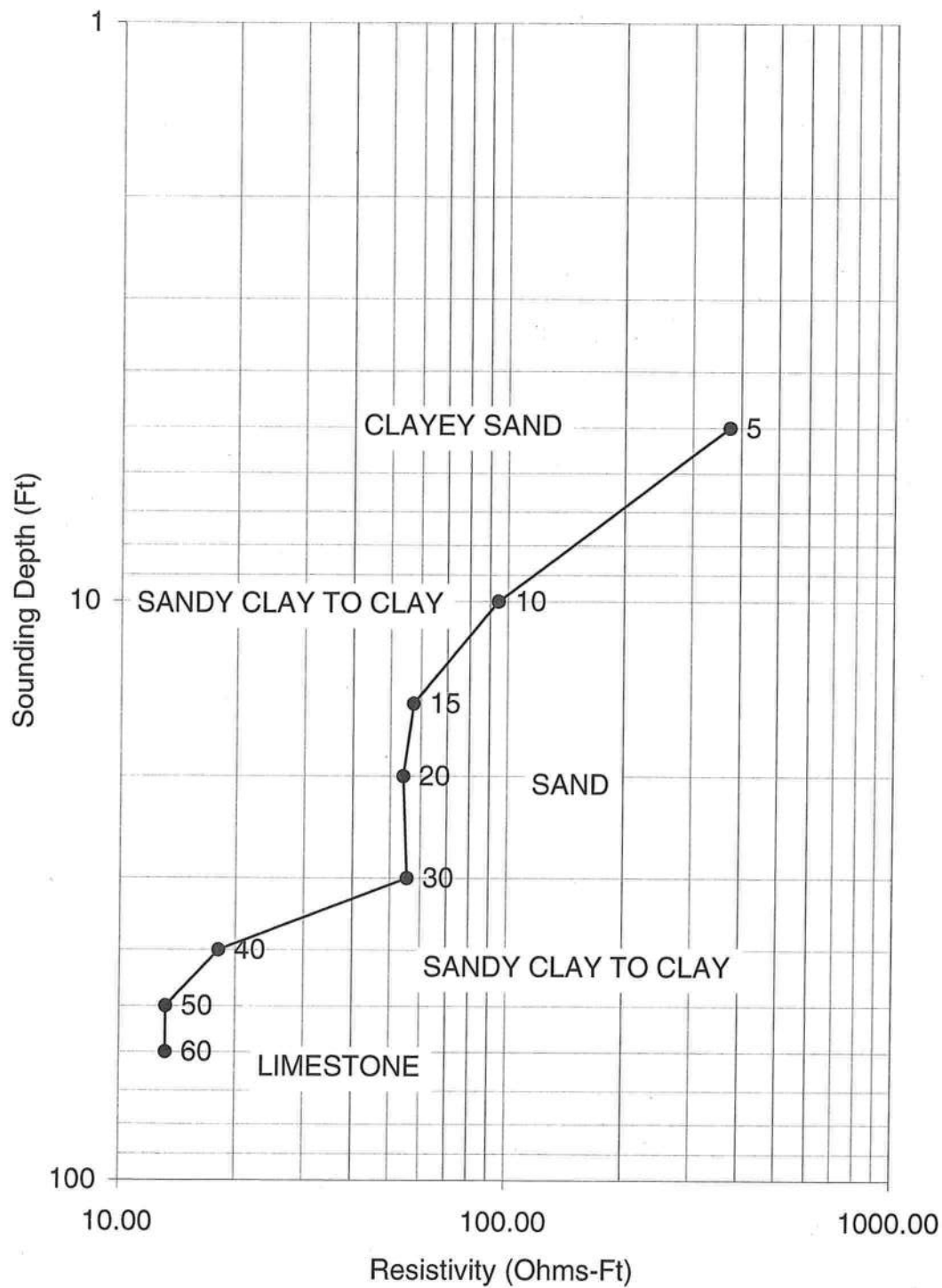


GEOHAZARDS INC.
Electrical Resistivity Survey
Investigation#:2008385
Array Orientation:N70E
Station Number: 4



GEOHAZARDS INC.
Electrical Resistivity Survey
Investigation#:2008385
Array Orientation:N40E
Station Number: 5





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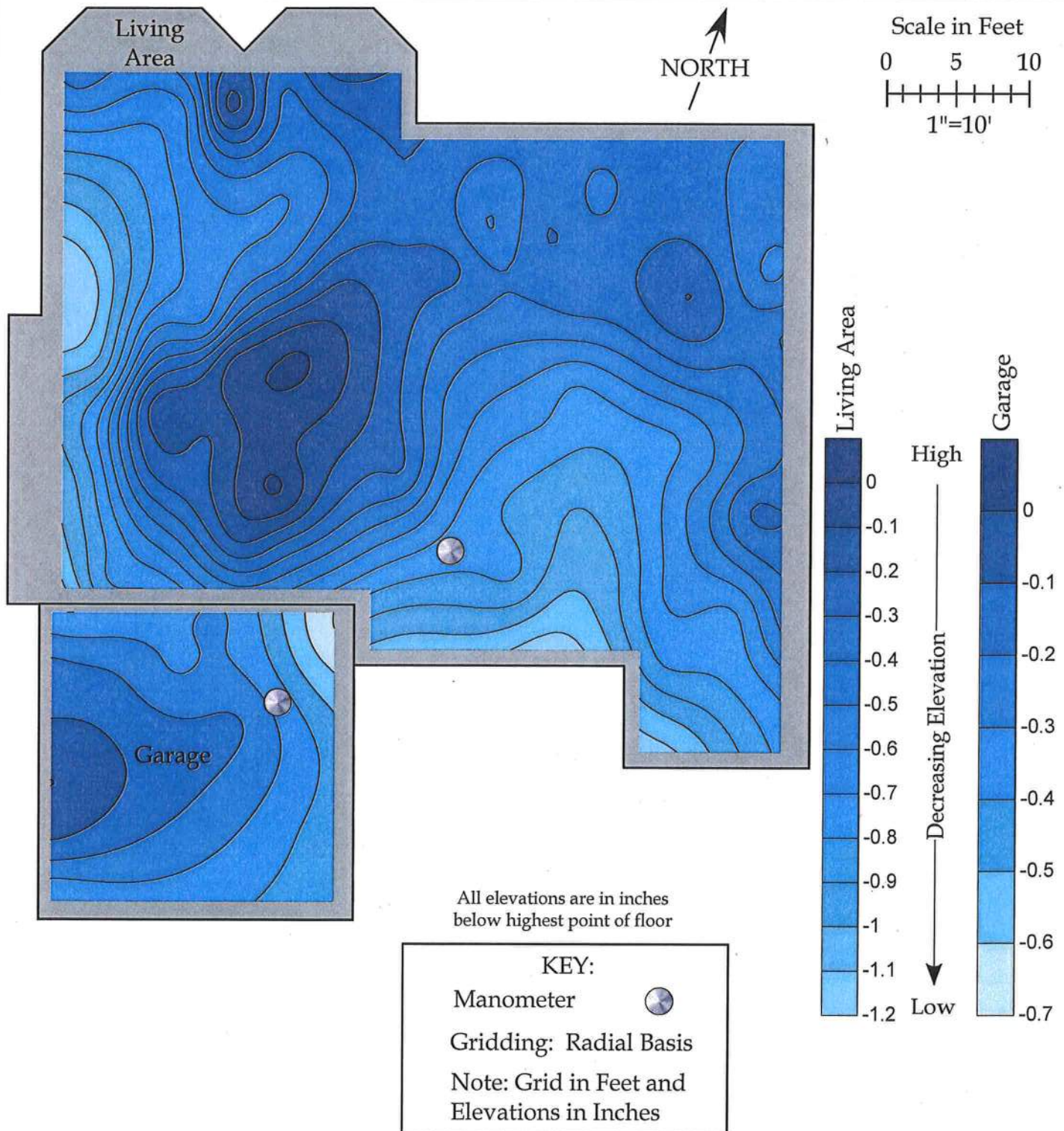
FLOOR ELEVATION SURVEY

Killin Residence
172 NW Kelley Lake Court
Lake City, Florida

FOR: Florida Farm Bureau

DATE: 6-19-08

BY: W. Wrenn, Geologist
Investigation# 2008385



GEOHAZARDS, INC.

Sinkholes • Expansive Clays • Land Subsidence

STANDARD PENETRATION TEST BORING

Project: Killin Residence

Lake City, Florida

Report No: 2008385

Geologist on Site: K. Crockett

Date Started: 6-26-08

Date Finished: 6-26-08

Drilled By: Race Drilling, Inc.










Boring Designation: B-1

Sheet 1 of 3

Water Table (ft.): 3.0 ft.

Type of Sampling: SPT-Mud Rotary

Location: 50 feet north and 22 feet west of the northeast corner of the structure

| DEPTH (ft.) | S A M P L E | BLOWS per 6 in. increment | N-value (blows/ft.) | W.T. | S Y M B O L | DESCRIPTION |
|----------------|----------------------------|---------------------------------|------------------------|--|---|---|
| 0 | | | | | | |
| | 1 | HA | NA |  3.0 ft. |  | Brown sandy clay (CL) |
| | 2 | HA | NA | |  | Brown fine sand (SP) |
| 5 | NS | 3,3,4,5 | 7 | | | No sample recovered - Presumed loose fine sand (SP) |
| | NS | 8,8,10,10 | 18 | | | No sample recovered - Presumed medium dense fine sand (SP) |
| 10 | 3 | 4,5,7,7 | 12 | |  | Brown medium dense clayey sand (SC) |
| | | | | | | |
| 15 | 4 | 5,5,5 | 10 | |  | Light grey loose clayey sand (SC) |
| | | | | | | |
| 20 | 5 | 2,3,3 | 6 | |  | Grey and orange firm sandy clay (CL) |
| | | | | | | |
| 25 | 6 | 4,4,5 | 9 | |  | Gray-orange stiff sandy clay (CL) |
| | | | | | | |
| 30 | 7 | 4,5,7 | 12 | |  | Grey medium dense silty sand (SM) |
| | | | | | | |
| 35 | 8 | 5,5,9 | 14 | |  | Grey medium dense silty sand (SM) |

GEOHAZARDS, INC.

Sinkholes • Expansive Clays • Land Subsidence

STANDARD PENETRATION TEST BORING

Project: Killin Residence

Lake City, Florida

Report No: 2008385

Geologist on Site: K. Crockett

Boring Designation: B-1 Sheet 2 of 3

| DEPTH (ft.) | S A M P L E | BLOWS per 6 in. increment | N-value (blows/ft.) | W.T. | S Y M B O L | DESCRIPTION |
|----------------|----------------------------|---------------------------------|------------------------|------|----------------------------|---|
| 35 | | | | | | |
| 40 | 9 | 7,8,9 | 17 | | | Grey and orange medium dense silty sand (SM) |
| 45 | 10 | 6,8,9 | 17 | | | Orange medium dense silty sand (SM) |
| 50 | 11 | 9,9,11 | 20 | | | Orange medium dense silty sand (SM) |
| 55 | 12 | 5,9,50/5 in. | R | | | Grey very dense silty sand (SM) |
| 60 | 13 | 16,20,33 | 53 | | | Grey silty sand (SM) Light tan medium hard limestone (LS) |
| 65 | 14 | 26,18,42 | 60 | | | Light tan medium hard limestone (LS) |
| 70 | 15 | 10,12,13 | 25 | | | 100% Loss of Circulation (LOC) at 68 ft. Light tan soft limestone (LS) |

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STANDARD PENETRATION TEST BORING

Project: Killin Residence

Lake City, Florida

Report No: 2008385

Geologist on Site: K. Crockett

Boring Designation: B-1 Sheet 3 of 3

| DEPTH (ft.) | S A M P L E | BLOWS per 6 in. increment | N-value (blows/ft.) | W.T. | S Y M B O L | DESCRIPTION |
|----------------|----------------------------|---------------------------------|------------------------|------|----------------------------|--|
| 70 | | | | | | |
| 75 | 16 | 50/5 in. | R | | | Light tan moderately hard limestone (LS) |
| 80 | 17 | 16,24,26 | 50 | | | Light tan medium hard limestone (LS) |
| 85 | | WOR/2 ft. | WOR | | | Weight-of-Rod (WOR) from 83.5 to 85.5 ft. |
| | 18 | 7,7,6 | 13 | | | Light tan very soft limestone (LS) |
| 90 | 19 | WOR,7,5 | 12 | | | Light tan very soft limestone (LS) |
| 95 | 20 | 15,16,8 | 24 | | | Light tan soft limestone (LS) |
| 100 | 21 | 6,13, 50/5 in. | R | | | Light tan moderately hard limestone (LS) Boring terminated at approximately 100 ft. 100% LOC at 68 ft., without recovery |

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STANDARD PENETRATION TEST BORING

Project: Killin Residence

Lake City, Florida

Report No: 2008385

Geologist on Site: K. Crockett

Date Started: 6-26-08

Date Finished: 6-26-08

Drilled By: Race Drilling, Inc.

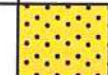









Boring Designation: B-2

Sheet 1 of 3

Water Table (ft.): 3.0

Type of Sampling: SPT-Mud Rotary

Location: 6 feet south and 16 feet east of the northeast corner of the structure

| DEPTH (ft.) | S A M P L E | BLOWS per 6 in. increment | N-value (blows/ft.) | W.T. | S Y M B O L | DESCRIPTION |
|----------------|----------------------------|---------------------------------|------------------------|---------|---|-----------------------------------|
| 0 | | | | | | |
| | 1 | HA | NA | 3.0 ft. |  | Grey fine sand (SP) |
| | 2 | HA | NA | |  | Grey sandy clay (CL) |
| 5 | 3 | 4,4,5,6 | 9 | |  | Grey stiff clay (CL) |
| | 4 | 8,10,9,10 | 19 | |  | Grey very stiff clay (CL) |
| 10 | 5 | 7,12,12,12 | 24 | |  | Grey medium dense sand (SP) |
| | | | | | | |
| 15 | 6 | 7,7,9 | 16 | |  | Grey medium dense silty sand (SM) |
| | | | | | | |
| 20 | 7 | 3,3,4 | 7 | |  | Green firm clay (CL) |
| | | | | | | |
| 25 | 8 | 6,12,14 | 26 | |  | Grey medium dense silty sand (SM) |
| | | | | | | |
| 30 | 9 | 8,10,13 | 23 | |  | Grey medium dense silty sand (SM) |
| | | | | | | |
| 35 | 10 | 4,8,9 | 17 | |  | Grey medium dense silty sand (SM) |

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STANDARD PENETRATION TEST BORING

Project: Killin Residence

Lake City, Florida

Report No: 2008385

Geologist on Site: K. Crockett

Boring Designation: B-2 Sheet 2 of 3

| DEPTH (ft.) | S A M P L E | BLOWS per 6 in. increment | N-value (blows/ft.) | W.T. | S Y M B O L | DESCRIPTION |
|----------------|----------------------------|---------------------------------|------------------------|------|----------------------------|---------------------------------------|
| 35 | | | | | | |
| 40 | 11 | 8,8,6 | 14 | | | Grey medium dense silty sand (SM) |
| 45 | 12 | 4,3,4 | 7 | | | Grey and orange loose silty sand (SM) |
| 50 | 13 | 4,4,3 | 7 | | | Grey and orange loose silty sand (SM) |
| 55 | 14 | 5,4,4 | 8 | | | Grey loose silty sand (SM) |
| 60 | 15 | 10,14,15 | 29 | | | Grey medium dense silty sand (SM) |
| 65 | 16 | 21,47,35 | R | | | Light tan medium hard limestone (LS) |
| 70 | 17 | 13,15,35 | 50 | | | Light tan medium hard limestone (LS) |

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STANDARD PENETRATION TEST BORING

Project: Killin Residence

Lake City, Florida

Report No: 2008385

Geologist on Site: K. Crockett

Boring Designation: B-2 Sheet 3 of 3

| DEPTH (ft.) | S A M P L E | BLOWS per 6 in. increment | N-value (blows/ft.) | W.T. | S Y M B O L | DESCRIPTION |
|----------------|----------------------------|---------------------------------|------------------------|------|----------------------------|---|
| 70 | | | | | | 100% Loss of Circulation (LOC) at 72 ft. |
| 75 | 18 | 8,7,6 | 13 | | | Light tan very soft limestone (LS) |
| 80 | 19 | 9,12,19 | 31 | | | Light tan soft limestone (LS) |
| 85 | 20 | 15,16,16 | 32 | | | Light tan soft limestone (LS) |
| 90 | 21 | 26,32,23 | 55 | | | Light tan medium hard limestone (LS) |
| 95 | 22 | 41,26,35 | R | | | Light tan medium hard limestone (LS) |
| 100 | 23 | 12,50/6 in. | R | | | Light tan medium hard limestone (LS) |
| | | | | | | Boring terminated at approximately 99.5 ft. 100% LOC at 72 ft., without recovery |

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STANDARD PENETRATION TEST BORING

Project: Killin Residence

Lake City, Florida

Report No: 2008385

Geologist on Site: J. Miller

Date Started: 7-2-08

Date Finished: 7-2-08

Drilled By: All County Drilling, LLC.











Boring Designation: B-3

Sheet 1 of 3

Water Table (ft.): Not Observed

Type of Sampling: SPT-Mud Rotary

Location: 11 feet west and 20 feet south of the northwest corner of the structure

| DEPTH (ft.) | S A M P L E | BLOWS per 6 in. increment | N-value (blows/ft.) | W.T. | S Y M B O L | DESCRIPTION |
|----------------|----------------------------|---------------------------------|------------------------|------|---|---|
| 0 | | | | NA | | |
| | 1 | HA | NA | |  | Brown fine sand (SP) |
| | 2 | HA | NA | |  | Gray sandy clay (CL) |
| 5 | 3 | 3,3,5,7 | 8 | |  | Gray firm sandy clay (CL) |
| | 4 | 6,10,12,17 | 22 | |  | Gray very stiff clay (CL) |
| 10 | 5 | 12,15,16,24 | 31 | |  | Tan dense clayey sand (SC) |
| | 6 | 5,9,8 | 17 | |  | Tan medium dense fine sand (SP) with trace silt |
| 15 | | | | | | |
| | 7 | 4,5,4 | 9 | |  | Tan stiff sandy clay (CL) |
| 20 | | | | | | |
| | 8 | 4,5,6 | 11 | |  | Tan medium dense fine sand (SP) with trace silt |
| 25 | | | | | | |
| | 9 | 4,5,5 | 10 | |  | Tan loose fine sand (SP) with trace silt |
| 30 | | | | | | |
| | 10 | 5,5,6 | 11 | |  | Tan medium dense fine sand (SP) with trace silt |
| 35 | | | | | | |

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STANDARD PENETRATION TEST BORING

Project: Killin Residence

Lake City, Florida

Report No: 2008385

Geologist on Site: J. Miller

Boring Designation: B-3 Sheet 2 of 3

| DEPTH (ft.) | S A M P L E | BLOWS per 6 in. increment | N-value (blows/ft.) | W.T. | S Y M B O L | DESCRIPTION |
|----------------|----------------------------|---------------------------------|------------------------|------|----------------------------|---|
| 35 | | | | | | |
| 40 | 11 | 4,5,6 | 11 | | | Tan medium dense fine sand (SP) with trace silt |
| 45 | 12 | 5,6,6 | 12 | | | Tan medium dense fine sand (SP) |
| 50 | 13 | 4,3,4 | 7 | | | Tan loose fine sand (SP) 100% Loss of circulation (LOC) at 50 ft. |
| 55 | | WOR/1.5 ft. | WOR | | | Weight-of-rod (WOR) from 53.5 to 55 ft. |
| | 14 | 4,4,5 | 9 | | | Tan loose fine sand (SP) with trace silt |
| 60 | | WOR/2 ft. | WOR | | | WOR from 58.5 to 60.5 ft. |
| | 15 | 2,2,2 | 4 | | | Tan loose fine sand (SP) with trace silt |
| 65 | | WOR/2 ft. | WOR | | | WOR from 63.5 to 65.5 ft. |
| | 16 | 4,6,4 | 10 | | | Tan loose fine sand (SP) with trace silt |
| 70 | | WOR/2 ft. | WOR | | | WOR from 68.5 to 70.5 ft. |

GEOHAZARDS, INC.

Sinkholes • Expansive Clays • Land Subsidence

STANDARD PENETRATION TEST BORING



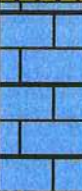




Project: Killin Residence

Lake City, Florida

Report No: 2008385

Geologist on Site: J. Miller

Boring Designation: B-3 Sheet 3 of 3

| DEPTH (ft.) | S A M P L E | BLOWS per 6 in. increment | N-value (blows/ft.) | W.T. | S Y M B O L | DESCRIPTION |
|----------------|----------------------------|---------------------------------|------------------------|------|---|--|
| 70 | 17 | 4,7,7 | 14 | |  | Orange stiff sandy clay (CL) |
| 75 | 18 | WOR/1 ft., 3 | 3 | |  | Tan very loose fine sand (SP) |
| 80 | 19 | 10,9,3 | 12 | |  | Light tan very soft limestone (LS) |
| 85 | 20 | WOR/1 ft., 10 | 10 | |  | Light tan very soft limestone (LS) |
| 90 | 21 | 14,13,12 | 25 | |  | Light tan soft limestone (LS) |
| 95 | 22 | 30,9,10 | 19 | |  | Light tan very soft limestone (LS) |
| 100 | 23 | 32,3,23 | 26 | |  | Light tan soft limestone (LS) |
| | | | | | | Boring terminated at 100 ft. 100% LOC at 50 ft., without recovery |

GEOHAZARDS, INC.

Professional Geological, Geophysical and Geotechnical Engineering Services

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PROPOSED REMEDIATION PROGRAM ESTIMATE

Killin Residence
172 NW Kelley Lake Court, Lake City, Florida
Florida Farm Bureau Insurance Claim No. 441215 ---- Geohazards, Inc. Project No. 2008385

Geohazards, Inc. has conducted a site investigation at the above location. Based on the WOR zones, including the cavity in limestone identified in the SPT borings, and observed surface depressions, sinkhole activity cannot be eliminated as a contributing source of distress. Subsurface compaction grouting, a common ground modification technique, is indicated to mitigate raveling and fill void spaces adjacent to and below the structure. The following basic grouting plan has been developed to remediate the sinkhole conditions.

| Task | Description | Estimated Quantity Survey | Unit Cost | Extended Cost |
|----------------------------|---|---------------------------|--------------|---------------------|
| 1 | Mobilization/Demobilization/Permits | 1 ea. | L.S. | \$1,500 |
| 2 | Site Preparation | 1 ea. | L.S. | \$1,500 |
| 3 | Injection Pipe Installation; 23 grout points, to competent limestone estimated approximately 90 ft. below the surface | 2,070 ft. | \$16/ft. | \$33,120 |
| 4 | Grout Injection | 200 - 300 cy. | \$155/cy. | \$31,000 - \$46,500 |
| 5 | On-site Monitoring | 8 -10 days (8 hours/day) | \$60/hour | \$3,840 - \$4,800 |
| 6 | Certification Reports | 1 | \$450/report | \$450 |
| Total Estimated Cost Range | | | | \$71,410 - \$87,870 |

GEOHAZARDS, INC.

Sinkholes • Expansive Clays • Land Subsidence

P.O. Box 14956
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(352) 371-7243 1-800-770-9990
Fax: (352) 371-4410

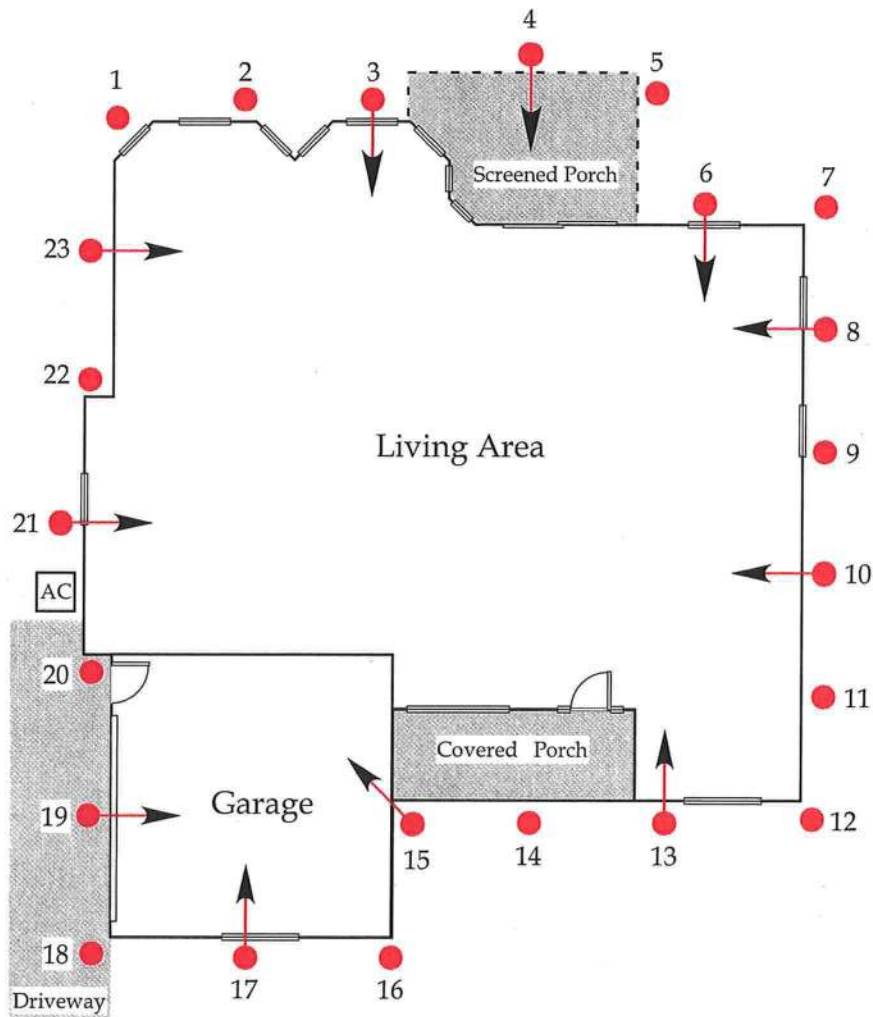
PROPOSED GROUT INJECTION LOCATIONS

Killin Residence
172 NW Kelley Lake Court
Lake City, Florida

FOR: Florida Farm Bureau

DATE: 6-19-08

BY: David Bloomquist, PhD, PE
Investigation#2008385



23 Injection Point Locations

Approximately 8' - 10' between points
Estimated average insertion depth: 90 feet

Injection Point



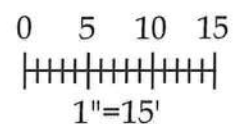
Angled Injection Point



Note: Some injection point locations may be inaccessible due to obstructions and minor relocation at the discretion of the contractor may be required.



Scale in Feet



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TECHNICAL SPECIFICATIONS FOR SUBSURFACE STABILIZATION PRESSURE GROUTING AT THE

Killin Residence
172 NW Kelley Lake Court, Lake City, Florida
Florida Farm Bureau Insurance Claim No. 441215 ---- Geohazards, Inc. Project No. 2008385

1.0 DESCRIPTION

The following specifications are for stabilization and remediation of subsoil conditions. The work consists of furnishing all labor, equipment and materials required to inject cementitious grout to an estimated average depth of 90 feet. Do not drill beyond 100 feet unless prior permission is obtained by the Engineer of Record. The stabilization program is intended to stabilize possible unstable subsurface soils by compacting any loose soils via densification, where present, sealing the limestone surface, voids and any partially in-filled cavities, and to minimize the potential for future ground subsidence due to raveling activity.

2.0 SCOPE

The scope of the stabilization program includes vertical and/or angled grout injections. The total estimated grout quantity, injection pipe footage and grout point locations are attached. However, the grouting program may be modified by the Contractor and Geotechnical Engineer (or his or her representative) as dictated by the actual field conditions. In these specifications, "Geotechnical Engineer" refers to Geohazards, Inc.'s geotechnical engineer.

If directed by the Geotechnical Engineer or his or her representative, additional grout locations may be required based on the site conditions encountered. Injection point locations are planned around the perimeter of the structure and screen enclosed porch on 8 - 10 foot centers. Alternative grout locations may be required. However, the Contractor or Geotechnical Engineer (or his or her representative) will establish the final grout injection locations in the field.

3.0 CONTRACTOR

The pressure grouting Contractor shall submit his or her qualifications to the Geotechnical Engineer. The Contractor shall have at least three years of experience in cement pressure grouting jobs, and shall submit references of his or her activities if requested.

Much of the interior and exterior distress observed in the structure is most probably the result of movements caused by the near-surface active clays identified in our investigation. Our recommendation of compaction grouting is intended to remediate the possible sinkhole conditions present at the property. However, compaction grouting does not mitigate the effects of the clays, and distress to the structure caused by the expansive clays is likely to continue.

The above plan does not include any remedial repair of the structure's interior or exterior, walks, slabs on grade, nor vegetation removal/replacement. Any cracks in the slab on grade should be repaired as part of the cosmetic repair program. Cosmetic repairs should begin no sooner than 60 days after the conclusion of the subsurface remediation program.

It is important to note that one of the three SPT borings did not terminate in competent material. Additionally, Geohazards, Inc. has limited historical data for the region where the structure is located. Therefore, drill depths and grout quantities are more difficult to estimate.

This grouting and underpinning program is not necessarily intended to be used solely as the final mitigation design. The suggested plan provided by Geohazards, Inc. should be used by the contractor as a basis for bidding, since site conditions may require the relocation, addition, or deletion of insertion points (e.g., septic tanks, drain fields, underground sprinkler pipes, utilities, etc.).

10-17-08


David Bloomquist, PhD, PE
Geotechnical Engineer
Florida License Number 37235



Attila Bodo, PE
Structural Engineer 10.16.08
Florida License Number 15834

4.0 EQUIPMENT

Grout Injection Equipment

A continuous flow, positive displacement model capable of pumping cement grout with a slump (ASTM C-143) of 3 to 6 inches maximum and pressures up to 600 psi (i.e., Schwing Model BPA 750D-15R or equivalent) shall be used. A pressure gauge shall be located in-line at the top of the casing or immediately before the top of the casing. The gauge shall be capable of reading pressures up to 600 psi in increments of 25 psi or smaller. Alternate equipment may be used at the discretion of the Geotechnical Engineer or his or her representative. Approval of any and all onsite equipment does not infer final acceptance.

Injection Pipes

Minimum inside diameter: 2 inches, Maximum inside diameter: 3 inches. Use of reducing nipples is not allowed.

5.0 GROUT MIXTURE

General

The materials used in this work shall conform to standard grouting practices as follows:

- Portland cement will conform to ASTM C-150. Aggregate will be natural sand material with percent passing the No. 200 sieve not greater than 30 percent. No maximum grain size is specified, however, it must not create sand blocking at the nozzle at the specified operating pressures.
- Lime will be hydrated if utilized.
- Mix water shall be potable.
- Once mixed, the cement/sand grout (including approved additives) shall obtain a minimum 48-hour compressive strength of 200 psi.

Grout Mix

The mixture used for grouting shall be a creamy consistency which will permit the grout to flow. If requested, when samples of the grout mixture are set aside for at least 12 hours in a standard concrete test mold, the resulting free surface water height shall be less than one percent of the initial sample height. Slump shall not exceed 6 inches. However, the slump may be varied throughout the grouting operation at the discretion of the Geotechnical Engineer or his or her representative. The grout mix shall not contain more than 0.6% by weight (22 lbs/cy) of bentonite. If bentonite is to be used, it must be hydrated prior to the addition of cement to minimize bleeding and segregation. The use of bentonite in compaction grouting can cause a loss of compressive strength of the grout mixture.

6.0 GROUT MIXING & PLACING

If on site mixing is used, facilities shall be provided for accurately measuring the ingredients in each batch of grout. The ingredients shall be thoroughly mixed and immediately pumped to the grout pipes through a flexible hose not more than 250 feet long.

7.0 PRESSURE GROUTING PROCEDURE

Pipe Installation

Grout pipes shall be installed to a depth sufficient to encounter bearing limestone or other bearing material (e.g., dense sand), approximately 90 feet on average below the ground surface. If this estimated average depth is exceeded by more than 10 feet, the drilling procedure shall cease and the Geotechnical Engineer notified. Drilling may continue at the Geotechnical Engineer's discretion. The Contractor may rotary drill or drive the injection pipes to the refusal depth. However, the method of installation shall ensure a good seal between the pipe and the surrounding soil. The installation method may be modified subject to the Geotechnical Engineer or his or her representative's approval if grout seeps up around the outside of the pipe during injection.

Grout Injection

Following satisfactory installation of an injection pipe, grouting operations may begin. During the grouting operation the injection pipes shall be incrementally raised to inject the entire zone between depths of approximately 90 feet and 10 feet below the ground surface. If feasible, the sequence of grouting should be performed at alternating locations to allow sufficient time for the mix to set prior to drilling and grouting adjacent points. The rate of pumping shall not exceed twelve cubic feet per minute. The pumping pressure at the top of the casing is planned to be in the range of 200 to 300 psi or as required by the Geotechnical Engineer or his or her representative. Unless otherwise directed by the Geotechnical Engineer or his or her representative, pumping shall cease for at least a 24-hour period if a 1-foot zone takes 20 or more cubic yards of grout at a slump of 4 inches. If this excessive pumping occurs, the grout pipe shall be raised and flushed to prevent the pipe from being cemented in place. Pumping can then proceed at another grout pipe location. Pumping may resume at the excessive grout pipe location and depth after a period of 24 hours has passed. The slump may be reduced further to 2 inches if a grout point fails to produce resistant pressure during the pumping operation. Once a resistance pressure of 250 – 300 psi is reached, the slump may be increased to not more than 6 inches to improve migration of the grout into the soil in order to compact loose zones adjacent to the pipe. Grouting procedures should be terminated once the grout point is filled to within 6 – 10 feet of the surface in order to minimize collateral damage to the structure.

Contractor Submittals

Methods of the work:

- a. Grout pipe installation procedures
- b. Proposed grout pipe locations, depths, and intervals
- c. Increments of depth for installation of grout
- d. Maximum grout quantities at each increment of depth
- e. Grout pressures at depths
- f. Equipment to be used in the work
- g. List of vendors and suppliers
- h. Daily records
- i. Grout mix design, design slump and tolerances

8.0 MONITORING BY THE GEOTECHNICAL ENGINEER OR HIS OR HER REPRESENTATIVE

General

The Geotechnical Engineer or his or her representative will monitor the pressure grouting operations to document compliance with the specifications outlined above and the duties discussed below. All injection pipe installations and grouting operations shall be performed in the presence of the Geotechnical Engineer's representative. The Geotechnical Engineer or his or her representative shall assume responsibility for verifying the quantity of grout pumped, intervals of grouting and deciding if additional or less grout is necessary.

Compliance

The Geotechnical Engineer or his or her representative may stop the grouting operation at any time if, in his or her judgment, the operation does not comply with these specifications or the work is unsuitable.

Daily Records

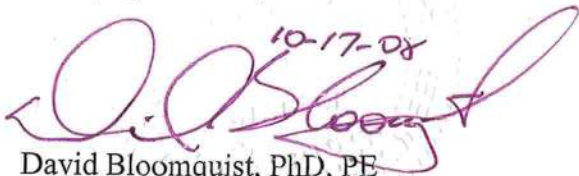
The Geotechnical Engineer or his or her representative will make all measurements of ground heave or settlement, installed pipe lengths and grout quantities pumped. Records of each day's grouting operation will be maintained for the benefit of the insurance company and Contractor. The grout and pipe quantities recorded by the Geotechnical Engineer's representative shall be considered the final amounts for pay purposes.

Ground/House Movement

During grouting, the Contractor and Geotechnical Engineer or his or her representative shall observe any vertical movement of the ground and house using a transit/level. If a downward movement of the ground surface is observed, the grouting operation shall cease and observations shall continue for 30 minutes. Likewise if there is any upward movement of the house, grouting should be temporarily suspended. If the ground does not return to its original grade, pumping shall be resumed at a lower rate of injection. If upward movement is observed, the grouting operation shall cease.

Existing Utilities/Structures

The Contractor shall exercise care when grouting beneath and adjacent to any underground utilities. The Contractor is responsible for ensuring the grouting operation does not damage existing utilities, wells, septic tanks, etc.



David Bloomquist, PhD, PE
Geotechnical Engineer
Florida License Number 37235



1. South (front) side of the Killin residence.



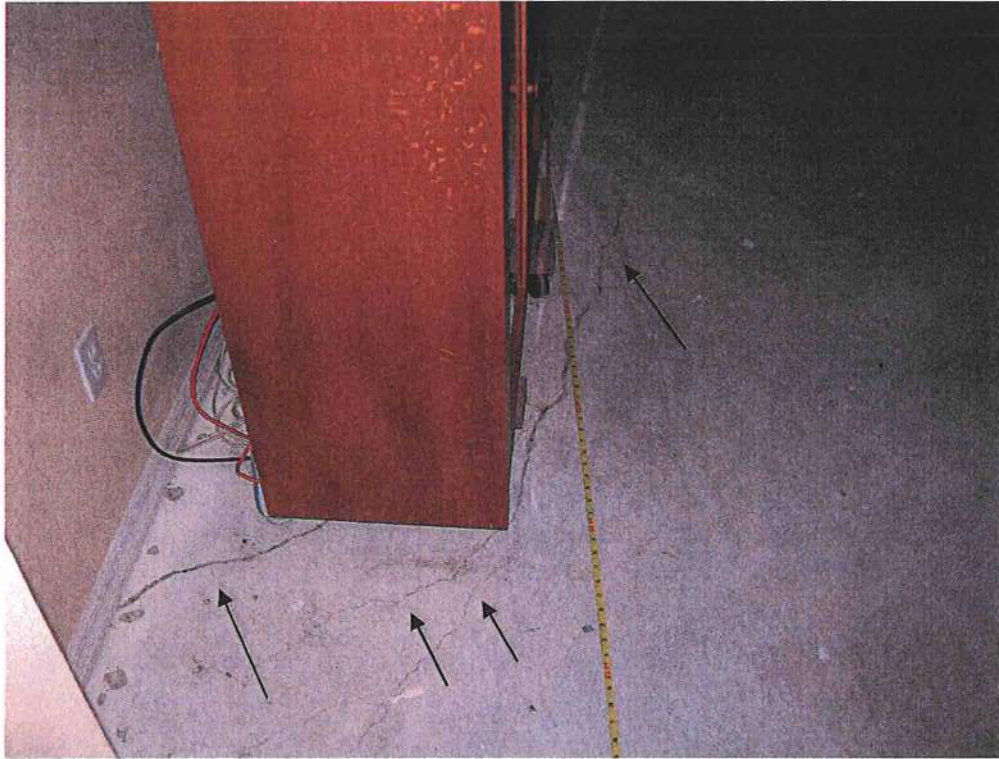
2. North side of the Killin residence.



3. West side of the Killin residence.



4. East side of the Killin residence.



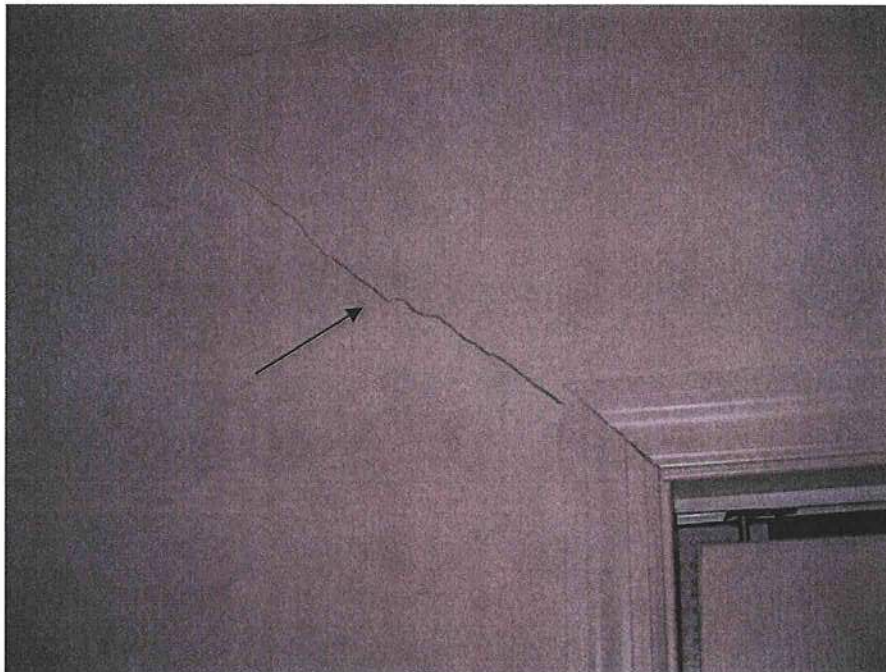
5. Slab cracks (hairline to $\frac{3}{8}$ inch) in the west portion of the living room.



6. Slab cracks (hairline to $\frac{1}{2}$ inch) with up to $\frac{1}{4}$ inch vertical displacement in the north portion of the living room.



7. Slab crack (1/4 inch) beneath the air conditioner handler.



8. Wall crack (1/16 inch) in the west wall of the laundry room.



9. Hairline tile crack in the east bathroom.



10. Stair-step crack (1/8 inch) in the east exterior wall.



11. Shifted pavers north of the structure.



12. Driveway cracks with up to 1/8 inch vertical displacement.



13. Test pit one (TP-1), located along the north wall of the structure (shown on site plan map), revealed a total foundation embedment of at least 16 inches below grade.



14. Test pit two (TP-2), located along the south wall of the garage (shown on site plan map), revealed a total foundation embedment of approximately 16 inches below grade.

GEOHAZARDS, INC.

Permit #-
27467

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GROUT PROCEDURE CERTIFICATION REPORT

Killin Residence
172 NW Kelly Lake Court
Lake City, Florida

December 5, 2008

Geohazards, Inc. Project No. 2008385B

Florida Farm Bureau Insurance
Claim No. 441215

Geotechnical Engineer:
David Bloomquist, PhD, PE
Florida License No. 37235

Onsite Representative:
Tammy Henry

Background

Compaction grouting was performed at the Killin Residence, 172 NW Kelly Lake Ct, Lake City, Florida by C&N Foundation Technologies, Inc. The objective was to stabilize the subsurface, thereby reducing the potential for future damage to the structure and surrounding appurtenances.

Geohazards, Inc. representative Tammy Henry monitored the grouting operation, which began on November 24, 2008, and concluded on December 5, 2008.

The grout pipe installation involved water injection drilling down and into competent limestone. This method inserts the grout casing as the point is drilled. A total of 23 grout

points were drilled requiring 1,696 linear feet of injection pipe. A Geohazards, Inc. monitor was not present during the grout pipe installation; therefore Geohazards, Inc. cannot confirm any observations or conclusions regarding details of the drilling effort.

Grouting Process

A crew of C&N Foundation Technologies, Inc. performed the pressure grouting operation which began at 10:41 AM on November 24, 2008. The automatic grout pump was connected to the injection pipe via a flexible hose. Grout pressures were monitored with an in-line pressure gauge. Grout was typically injected using a pump and pull technique that injected grout while the pipe was extracted over five-foot intervals via a hydraulic jack.



Grout delivery setup with piston pump



Injection pipe with the flexible hose connected to a hydraulic ram unit

The grout pumping process continued until one of the following events occurred:

- The grout line pressure exceeded 250 - 400 psi. This signifies that proper compaction of the soil at that specific depth was achieved.
- House movement, detected either by surveying transit or level. Movement of the structure also requires that the grouting be stopped at that location.
- Ground movement, detected either by surveying transit or level. Any movement of the ground (heave) requires that the grouting cease.
- Grout flows from the base of the pipe. Grouting ceased if grout was observed flowing from the base of the pipe injection point. This occurs if grout channels up the outside of the pipe.

For any of the above conditions, the contractor would subsequently raise the pipe between 4 and 8 feet and continue pumping. Grouting was terminated when grouting depths reached 12 feet or less below the surface.



Level to monitor structure movement

Another situation that requires cessation of pumping occurs when the pipe operator notices that excessive force is required to raise the grout pipe. This could result in the pipe breaking at a fitting. In order to prevent this occurrence, the contractor would stop grouting, pull the pipe up until the pulling force was reduced, and then resume pumping. This reduction in force usually occurs after pulling the pipe up two to four feet.

Observations

The depth to competent limestone varied at the site, ranging from 62 to 92 feet. Injection point 16 accepted the largest volume of grout, at 20.8 cubic yards (cy). Other injection points that accepted relatively large quantities were points 21 (16.7 cy) and 22 (13.1 cy). Injection point 18 accepted less than one cubic yard. Slight structural lift (less than 1/8") was observed at most points. These occurrences are noted in the field logs.

Heavy backflow at points 5, 6, and 10 necessitated raising the pipes twelve feet or more at various depths. Tight casing at point 8 necessitated raising the pipe twelve feet. These occasions are noted in the grout logs

There were no other anomalous instances observed during the grouting procedure.

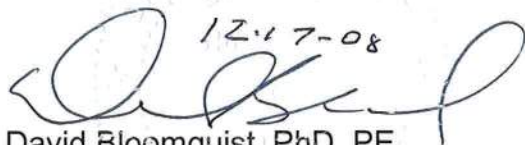
The grouting program was completed on December 5, 2008. The total grout delivered to the site was 170 cy. Trucks 5, 12, and 18 were returned to the batch plant with an unused load of 2.3, 1.5, and 1.8 cubic yards. Thus, 164.4 cy of grout was placed into the injection points. Complete grout logs are attached at the end of this report.

Conclusions

The figures cited in the table below represent our proposed estimate and the actual quantities used at the Killin residence grout remediation site. Based on the drill depths and the quantity of grout injected, at this time Geohazards, Inc. opines that the sinkhole conditions have been remediated. In addition, a review of the procedures employed by C&N Foundation Repair, Inc. indicates that the grouting operation was performed in accordance with the proposed Geohazards, Inc. program, technical specifications and foundation grouting industry practices.

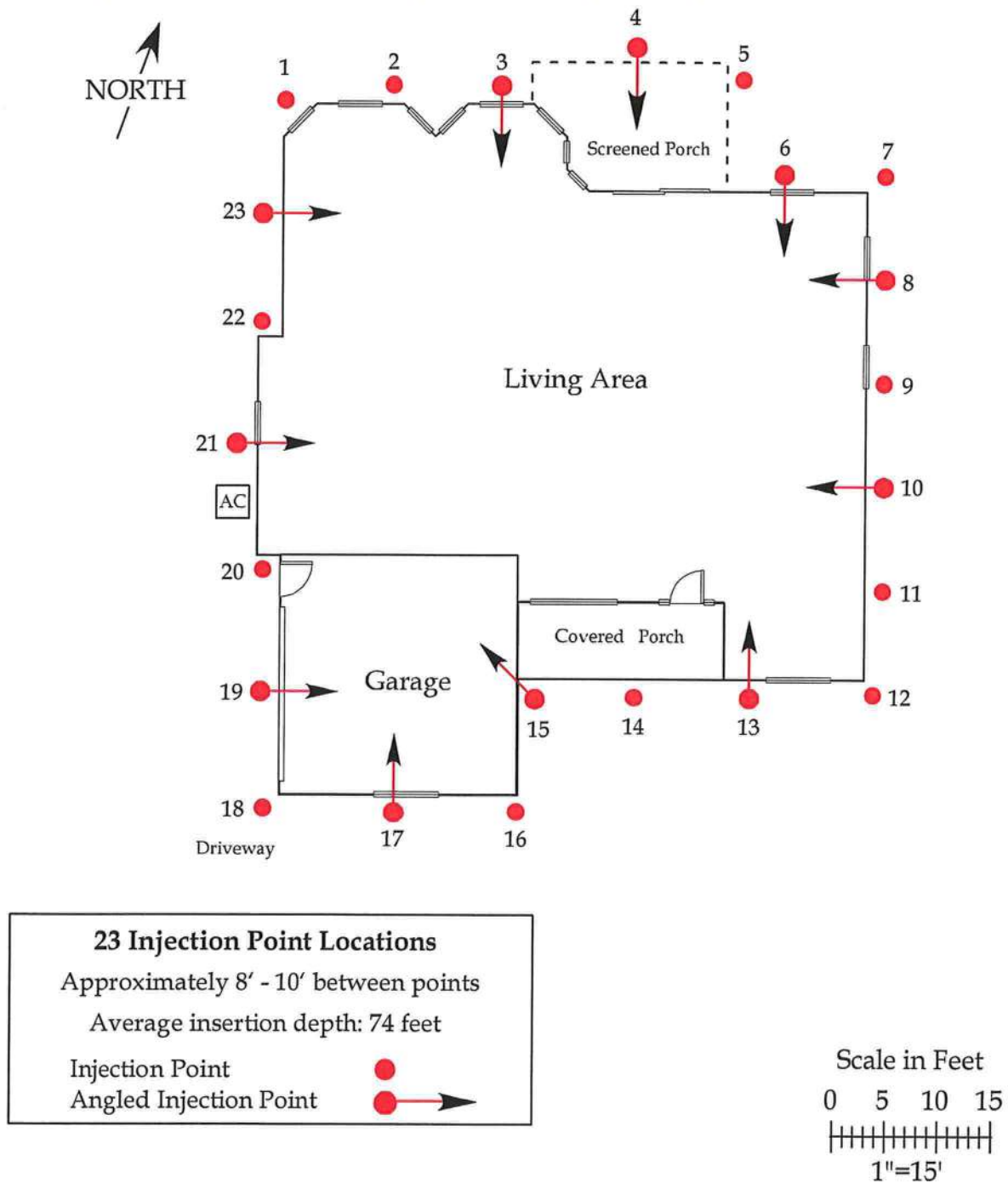
| ITEM NUMBER | ITEM | ESTIMATE | FINAL QUANTITY |
|-------------|-----------------------------|--------------|----------------|
| 1 | Linear feet of grout pipe | 2,070 lf | 1,696 lf |
| 2 | Cubic yards of grout pumped | 200 – 300 cy | 164.4 cy |

Respectfully submitted,

A handwritten signature in black ink, appearing to read 'David Bloomquist', with the date '12.17-08' written above it.

David Bloomquist, PhD, PE
Geotechnical Engineer
Florida License No. 37235

Schematic of final grout locations at the Killin Residence, Lake City, Florida.



Final Grout Totals
Project: Killin Residence
Project Number: 2008385B

| Station | Depth (feet) | Grout Injected (cubic yards) | Injection Angle (° from vertical) |
|--|--------------|------------------------------|-----------------------------------|
| 1 | 78 | 10.8 | 0 |
| 2 | 75 | 10.7 | 0 |
| 3 | 62 | 1.8 | 16 |
| 4 | 64 | 1.3 | 12 |
| 5 | 92 | 11 | 0 |
| 6 | 72 | 8.6 | 12 |
| 7 | 66 | 1 | 0 |
| 8 | 78 | 9.7 | 15 |
| 9 | 86 | 1.2 | 0 |
| 10 | 90 | 4.9 | 18 |
| 11 | 66 | 7.3 | 0 |
| 12 | 74 | 3.7 | 0 |
| 13 | 90 | 7.2 | 14 |
| 14 | 62 | 7.2 | 0 |
| 15 | 68 | 4.6 | 13 |
| 16 | 84 | 20.8 | 0 |
| 17 | 65 | 1.4 | 12 |
| 18 | 66 | 0.9 | 0 |
| 19 | 64 | 2.5 | 14 |
| 20 | 78 | 12.9 | 0 |
| 21 | 76 | 16.7 | 16 |
| 22 | 72 | 13.1 | 0 |
| 23 | 68 | 5.1 | 19 |
| Totals | 1,696 ft | 164.4 cy | |
| Average Insertion Depth = 74 ft | | | |

Total Grout Delivered: 164.4 cy
Total Grout Returned: 5.6 cy
Total Grout Injected: 170 cy

ATTACHMENTS

Grout Logs

| | | | | | | | |
|----------------------------------|------------|-------------------------|----------|--|--------------|-------|---|
| Project: Killin Residence | | Date: November 24, 2008 | | Sheet 1/10 of | | | |
| Contractor: C+N Foundation Tech. | | Notes: 4' casings | | Instrument: Bergier 80x | | | |
| Foreman: Kevin | | | | Pump: Putzmeister T240 (asked them to brk 8' vs 12') | | | |
| Station: | Time: | Depth: | Pressure | Strokes | Grout Placed | Slump | Observations |
| 4 | Start Stop | From To | | | | | |
| 4 | 1041 1043 | 64 56 | 300* | 21 | 0.3 | 5 | T1 @ 1035, start PT 4; HP, Brk 12 |
| 4 | 1048 1049 | 52 48 | 300* | 8 | 0.1 | 5 | HP, Brk 8 |
| 4 | 1053 1054 | 44 40 | 300* | 9 | 0.1 | 5 | HP, Brk 8 |
| 4 | 1059 1101 | 36 32 | 300* | 23 | 0.1 | 5 | HP, Brk 8 |
| 4 | 1106 1107 | 28 24 | 300* | 11 | 0.2 | 5 | HP, Brk 8 |
| 4 | 1111 1112 | 20 16 | 300* | 5 | 0.1 | 5 | HP, Brk 8 |
| 4 | 1116 1116 | 12 10 | 300* | 3 | 1.3 | 5 | HP, Brk 8 Pull + end PT 4 |
| 5 | 1130 1132 | 90 86 | 300* | 37 | 0.6 | 5 | start PT 5; HP, Brk 8 |
| 5 | 1136 1137 | 82 78 | 300* | 7 | 0.1 | 5 | HP, Brk 8 |
| 5 | 1140 1142 | 74 70 | 300* | 30 | 0.5 | 5 | HP, Brk 8 |
| 5 | 1144 1149 | 66 62 | 250* | 111 | 1.8 | 5 | HP, Brk 8, BF Brk 4 |
| 5 | 1155 1158 | 60 54 | 250* | 54 | 0.8 | 5 | HP, Brk 8, BF |
| 5 | 1202 1200 | 52 50 | 250* | 310 | 8.7 | 5 | Empty, Flush, 2 |
| 5 | 1309 1312 | 92 48 | 200* | 689 | 10/10cy | 5 | Grout Returned, left @ 1226 |
| 5 | 1317 1317 | 44 40 | 225* | 56 | 0.3 | 5 | T2 @ 1303, HP, Brk 8 |
| 5 | 1322 1325 | 36 32 | 250* | 10 | 0.2 | 5 | HP, Brk 8 |
| 5 | 1331 1332 | 28 24 | 250* | 54 | 0.3 | 5 | HP, Brk 8, BF |
| 5 | 1336 1337 | 20 16 | 300* | 6 | 0.1 | 5 | HP, Brk 8 |
| 5 | 1340 1340 | 12 10 | 275* | 7 | 0.1 | 5 | GT 5, Brk 8 |
| 6 | 1349 1357 | 72 10 | 275* | 7 | 0.1 | 5 | GT 5, SL, Pull + end PT 5 (asked about not) |
| | | | 200 | 169 | 2.7 | | T2 empty, Flush Brk 8 |
| | | | | 309 | 5/5cy | | Grout Returned, left @ 1410 |
| | | | | | | | Plant closing @ 3, needed to be done prior |
| | | | | | | | - end day - |

PT 4 = 1.3

PT 5 = 11cy

asked about not

[illegible]

| | | | | | | | | | |
|-----------------------------------|-------|------|---------------------|----|------------------------|---------|--------------|-------|---------------------------------|
| Project: Killin Residence | | | Date: Nov. 26, 2008 | | Sheet 3/10 | | | | |
| Contractor: C+N Foundations Tech. | | | Notes: | | Instrument: Berger 20X | | | | |
| Foreman: Jose | | | | | Pump: Putzmeister TK40 | | | | |
| Station: | Time: | | Depth: | | Pressure | Strokes | Grout Placed | Slump | Observations |
| | Start | Stop | From | To | | | | | |
| 8 | 0838 | 0840 | 34 | 30 | 250+ | 36 | | 5 | TS @ 0812, Cont PT 8; HP, Brk 8 |
| 8 | 0844 | 0844 | 26 | 21 | 250 | 2 | | 5 | PL; Brk 8 |
| 8 | 0847 | 0847 | 18 | 12 | 250 | 2 | 40 / 0.6 | 5 | PL; GTS, Pulltend PT 8 |
| 7 | 0902 | 0904 | 66 | 62 | 300+ | 16 | | 5 | Start PT 6; HP, Brk 8 |
| 7 | 0908 | 0908 | 58 | 54 | 300+ | 8 | | 5 | HP, Brk 8 |
| 7 | 0912 | 0913 | 50 | 46 | 300+ | 5 | | 5 | HP, Brk 8 |
| 7 | 0915 | 0916 | 42 | 38 | 300+ | 7 | | 5 | HP, Brk 8 |
| 7 | 0920 | 0920 | 34 | 30 | 300+ | 6 | | 5 | HP, Brk 8 |
| 7 | 0925 | 0926 | 26 | 22 | 300+ | 15 | | 5 | HP, Brk 8 (BF) |
| 7 | 0931 | 0931 | 18 | 14 | 250 | 6 | 63 / 1.0 | 5 | GTS, Pulltend PT 7 |
| 10 | 0951 | 0952 | 90 | 86 | 275+ | 24 | | 5 | Start PT 10; HP, Brk 8 |
| 10 | 0956 | 0957 | 82 | 78 | 300+ | 9 | | 5 | HP, Brk 8 |
| 10 | 1000 | 1002 | 74 | 70 | 300+ | 10 | | 5 | HP, Brk 8 |
| 10 | 1005 | 1006 | 66 | 62 | 300+ | 12 | | 5 | HP, Brk 8 |
| 10 | 1010 | 1012 | 58 | 54 | 300+ | 14 | | 5 | HP, Brk 8 |
| 10 | 1015 | 1018 | 50 | 46 | 250+ | 14 | | 5 | HP, Brk 8 (BF) Brk 4 |
| 10 | 1030 | 1033 | 38 | 34 | 250+ | 55 | | 5 | HP, Brk 8 (BF) |
| 10 | 1037 | 1039 | 30 | 26 | 275+ | 26 | | 5 | HP, Brk 8 (BF) |
| 10 | 1043 | 1044 | 22 | 18 | 275+ | 16 | | 5 | HP, Brk 8 (BF) |
| 10 | 1047 | 1047 | 14 | 12 | 300 | 2 | 310 / 4.9 | 5 | GTS, Pulltend PT 10 |
| 9 | 1059 | 1101 | 86 | 82 | 275+ | 11 | | 5 | HP, Brk 8 |
| 9 | 1105 | 1106 | 78 | 74 | 200+ | 3 | | 5 | HP, Brk 8 |
| 9 | 1111 | 1113 | 70 | 66 | 300+ | 6 | | 5 | HP, Brk 8 |
| 9 | 1119 | 1120 | 62 | 58 | 300+ | 7 | | 5 | HP, Brk 8 |
| 9 | 1124 | 1125 | 54 | 50 | 300+ | 5 | | 5 | HP, Brk 8 |
| 9 | 1130 | 1131 | 46 | 42 | 300+ | 4 | | 5 | HP, Brk 8 |
| 9 | 1135 | 1136 | 38 | 34 | 300+ | 5 | | 5 | HP, Brk 8 |
| 9 | 1142 | 1143 | 30 | 26 | 300+ | 4 | | 5 | HP, Brk 8 |
| 9 | 1149 | 1150 | 22 | 16 | 300+ | 2 | 24 / 1.2 | 5 | HP, Pulltend PT 9 |

487 77/1004

2,3 cy Ret., TS left @ 1200

— End day —

| | | | | | | | |
|--------------------------------------|----------------------|--|------------------|--|-----------------|-------|-----------------------------------|
| Project: Killin Residence 2008385 | | Date: December 1 st , 2008 Mon | | Sheet of 4/10 | | | |
| Contractor: C&N Foreman: Jose | | Notes: | | Instrument: CST Berger 200 Pump: Patzmeister TK40 | | | |
| Station: | Time: | Depth: | Pressure | Strokes | Grout Placed | Slump | Observations |
| 11 | Start 1135 Stop 1144 | From 66 To 62 | 300 ⁺ | 165 | | | TG @ 1130, Start PT 11; HP, Brk 8 |
| 11 | 1146 1152 | 58 54 | 300 ⁺ | 147 | | | HP, Brk 8 (BF) |
| 11 | 1156 1157 | 50 46 | 300 ⁺ | 27 | | | HP, Brk 8 |
| 11 | 1200 1201 | 42 38 | 300 ⁺ | 12 | | | HP, Brk 8 |
| 11 | 1203 1205 | 34 30 | 300 ⁺ | 31 | | | HP, Brk 8 |
| 11 | 1208 1211 | 28 24 | 275 ⁺ | 24 | | | GTS, Brk 8 |
| 11 | 1216 1217 | 20 16 | 300 | 14 | 400 / 7.3 | | GTS, Pull end PT 11 |
| 13 | 1235 1236 | 90 86 | 300 ⁺ | 25 | | | Start PT 13, HP, Brk 8 |
| 13 | 1238 1240 | 82 78 | 300 ⁺ | 8 | | | HP, Brk 8 |
| 13 | 1242 1243 | 74 70 | 300 ⁺ | 12 | | | HP, Brk 8 |
| 13 | 1248 1250 | 68 64 | 300 ⁺ | 64 | | | HP, Brk 8 (BF) |
| 13 | 1257 1259 | 60 60 | 275 | 50 | 159 / 2.7 | | TG empty, flush |
| 13 | 1353 1354 | 60 56 | 300 ⁺ | 579 | 10/100g | | dry Ret. TG left @ 1310 |
| 13 | 1358 1359 | 52 48 | 300 ⁺ | 366 | | | T7 @ 1342, HP, Brk 8 |
| 13 | 1403 1409 | 44 40 | 250 ⁺ | 4 | | | HP, Brk 8 |
| 13 | 1415 1419 | 36 32 | 275 ⁺ | 125 | | | HP, Brk 8 |
| 13 | 1425 1429 | 28 24 | 275 ⁺ | 73 | | | HP, Brk 8 ((rock 4" diam)) |
| 13 | 1433 1433 | 20 16 | 275 ⁺ | 36 | | | HP, Brk 8 |
| 15 | 1447 1449 | 68 64 | 300 ⁺ | 4 | 278 / 4.5 | | HP, Pull end PT 13 |
| 15 | 1452 1453 | 60 56 | 300 ⁺ | 23 | | | HP, Brk 8 |
| 15 | 1456 1457 | 52 48 | 300 ⁺ | 11 | | | HP, Brk 8 |
| 15 | 1501 1505 | 44 40 | 300 ⁺ | 27 | | | HP, Brk 8 |
| 15 | 1510 1516 | 36 32 | 300 ⁺ | 60 | | | HP, Brk 8 |
| 15 | 1520 1522 | 28 24 | 275 | 128 | | | SL, Brk 8 |
| 15 | 1529 1530 | 20 16 | 275 | 25 | | | SL, Brk 8 |
| 12 | 1546 1551 | 74 74 | 300 | 10 | 284 / 4.6 | | SL, Pull end PT 15 |
| | | | 250 | 57 | 6.9 | | T7 empty, flush |
| | | | | 619 | 10/100g | | dry Ret. left @ 1600 |
| | | | | | | | 1 - END DAY - |

PT 11 =
7.3

PT 13 =
7.6

PT 15 =
4.6

| Project: Killin Residence 2008385 | | | Date: Dec. 3, 2008 | | Sheet of 6/10 | |
|---|-------|------|--------------------|----|--|---------|
| Contractor: C+N Foreman: JOSE | | | Notes: | | Instrument: Berger 20X Pump: Putzmeister TK40 | |
| Station: | Time: | | Depth: | | Pressure | Strokes |
| | Start | Stop | From | To | | |
| 16 | 0844 | 0845 | 2440 | 28 | 300+ | 12 |
| 16 | 0849 | 0851 | 24 | 20 | 275+ | 33 |
| 16 | 0855 | 0856 | 16 | 14 | 300 | 18 |
| 18 | 0920 | 0923 | 66 | 62 | 300+ | 15 |
| 18 | 0926 | 0927 | 58 | 54 | 300+ | 7 |
| 18 | 0931 | 0932 | 50 | 46 | 300+ | 6 |
| 18 | 0936 | 0936 | 42 | 38 | 300+ | 2 |
| 18 | 0941 | 0942 | 34 | 30 | 300+ | 15 |
| 18 | 0945 | 0947 | 26 | 22 | 300+ | 10 |
| 18 | 0956 | 0957 | 18 | 18 | 300 | 2 |
| 17 | 1010 | 1012 | 65 | 61 | 275+ | 31 |
| 17 | 1017 | 1017 | 57 | 53 | 300+ | 8 |
| 17 | 1021 | 1021 | 49 | 45 | 300+ | 9 |
| 17 | 1026 | 1027 | 41 | 37 | 300+ | 10 |
| 17 | 1031 | 1032 | 33 | 29 | 300+ | 14 |
| 17 | 1036 | 1037 | 25 | 21 | 300+ | 7 |
| 17 | 1041 | 1041 | 17 | 13 | 300 | 4 |
| 20 | 1105 | 1107 | 78 | 74 | 250+ | 34 |
| 20 | 1113 | 1121 | 70 | 66 | 275 | 168 |
| 20 | 1125 | 1136 | 66 | 66 | | 224 |
| 20 | | | 54 | | | 617 |
| 20 | 1312 | 1325 | 66 | 62 | 275-300 | 283 |
| 20 | 1331 | 1332 | 58 | 54 | 300+ | 21 |
| 20 | 1337 | 1339 | 50 | 46 | 300+ | 10 |
| 20 | 1343 | 1345 | 42 | 38 | 300+ | 18 |
| 20 | 1352 | 1353 | 34 | 30 | 300+ | 8 |
| 20 | 1359 | 1403 | 26 | 22 | 300+ | 8 |
| 20 | 1410 | 1411 | 18 | 14 | 300+ | 4 |
| | | | | | | 7 |
| Observations: T11 @ 35, Cont @ 16, HP, Brk 8 HP, Brk 8 GL, Pull + end RT 16 PL, HP, Brk 8 (Stacked PT 18) HP, Brk 8 HP, PL, Brk 8 PL, Brk 8 HP, Brk 8 HP, Brk 8 PL, Pull + end RT 18 HP, Brk 8 (Stacked PT 17) HP, Brk 8 HP, Brk 8 HP, Brk 8 PL, HP, Brk 8 GL, Pull + end RT 17 Start PT 20, HP, Brk 8 HP, Brk 8 T11 Empty, Flush 0 cy. Refused, Ref @ 1150 T12 @ 1305, GL, Brk 8 HP, Brk 8 HP, Brk 8 HP, Brk 8 HP, Brk 8 HP, Brk 8 HP, Pull + end RT 20 see next → | | | | | | |

332

6

PT 16
20

PT 18
20

PT 17
1.4

PT 20
13.6

[illegible]

| | | | | | | | |
|--------------------------------------|------------------------------|---|----------|---------|-----------------|-------|------------------------------------|
| Project: Killin Residence 2008385 | Date: Thurs. Dec. 4, 2008 | Sheet of 8/10 | | | | | |
| Contractor: C+N Foreman: Jose | Notes: | Instrument: CST Berger 20X Pump: Putzmeister TK 40 | | | | | |
| Station: | Time: | Depth: | Pressure | Strokes | Grout Placed | Slump | Observations |
| 21 | Start Stop | From To | | | | | |
| 21 | 0838 0850 | 76' 72 | 250* | 210 | 3.1/100g | 5 | T13 @ 0815, start PT 21; HP; Brk 8 |
| 21 | 0853 0906 | 68 64 | 250* | 191 | 3.2/100g | 5 | HP, Brk 8 |
| 21 | 0909 0920 | 60 60 | 275 | 218 | 3.5/100g | 5 | T13 empty, Flush |
| 21 | 1025 1030 | 60 56 | 275* | 629 | 10/100g | | Occy returned, left @ 0936 |
| 21 | 1033 1039 | 52 48 | 300* | 80 | 1.2/100g | 5 | T14 @ 1018, HP; 8F Brk 8 |
| 21 | 1042 1051 | 44 41 | 250 | 97 | 1.5 | 5 | HP, Brk 8 |
| 21 | 1054 1101 | 36 33 | 250 | 142 | 2.2/100g | 5 | SL, Brk 8 |
| 21 | 1105 1106 | 28 25 | 300 | 107 | 1.6 | 5 | SL, Brk 8 |
| 21 | 1111 1112 | 20 15 | 250 | 15 | 0.2 | 5 | SL, Brk 8 |
| 21 | 1116 1116 | 12 12 | 250 | 3 | 0 | 5 | PL, Brk 8 |
| 21 | 1133 1113 | 78 78 | 250 | 218 | 6.7 | 5 | GTS, Pull + end PT 21 |
| 1 | 1239 1243 | 78 73 | 250* | 664 | 10/100g | 5 | T14 empty, Flush |
| 1 | 1257 1303 | 70 66 | 275 | 270 | 1.3 | 5 | Occy Ret; left @ 1153 |
| 1 | 1301 1308 | 62 58 | 275 | 77 | 0.5 | 5 | T15 @ 1234; TC, Brk 8 |
| 1 | 1313 1315 | 54 50 | 275 | 29 | 0.4 | 5 | GL, Brk 8 |
| 1 | 1317 1318 | 46 42 | 300* | 23 | 0.2 | 5 | GL, Brk 8 |
| 1 | 1322 1323 | 38 34 | 300* | 13 | 0.2 | 5 | GL, Brk 8 |
| 1 | 1327 1328 | 30 26 | 300 | 14 | 0.2 | 5 | HP, Brk 8 |
| 1 | 1333 1333 | 22 18 | 300* | 32 | 0.5 | 5 | HP, Brk 8 |
| 1 | 1339 1341 | 14 10 | 300 | 9 | 0.2 | 5 | GL, Brk 8 |
| 2 | 1350 1400 | 75' 73 | 250 | 246 | 7.5 | 5 | PL, Pull + end PT 1 |
| 2 | 1506 1526 | 75' 71 | 275 | 155 | 3.5 | 5 | Start PT 2; T15 empty, Flush |
| 2 | 1528 1529 | 67 63 | 300* | 624 | 10/100g | | Occy Ret; left @ 1409 |
| 2 | 1532 1533 | 59 55 | 300* | 401 | | 5 | T16 @ 1456, GL, Brk 8 |
| 2 | 1536 1538 | 51 47 | 300* | 11 | | 5 | HP, Brk 8 |
| 2 | 1541 1543 | 43 39 | 300* | 20 | | 5 | HP, Brk 8 |
| 2 | 1541 1543 | 43 39 | 300* | 20 | | 5 | HP, Brk 8 |

See next sheet →

See next sheet →

[illegible]

| Project: | Killin Residence | Date: | Dec. 5, 2008 | Sheet | 10/10 | | |
|-------------|------------------|--------|--------------|---------------|-------------------|----------|--------------------------------------|
| Contractor: | CAN | Notes: | | Instrument: | Bergier 20X | | |
| Foreman: | JOSE | | | Pump: | Putzmeister TK 40 | | |
| Station: | Time: | Depth: | Pressure | Strokes | Grout Placed | Slump | Observations |
| | Start | From | To | | | | |
| 22 | 0818 | 72 | 70 | 250 | 646 | 10/10cy | T17 @ 0800, start PT 22; Truck Empty |
| 22 | 0910 | 72 | 68 | 250 | 61 | | 0.4y Ret, left @ 0858 |
| 22 | 0915 | 64 | 60 | 275 | 20 | | T18 @ 0908, GL, Brk 8 |
| 22 | 0922 | 56 | 52 | 275 | 20 | | GL, Brk 8 |
| 22 | 0927 | 48 | 44 | 300 | 24 | | GL, Brk 8 |
| 22 | 0932 | 40 | 36 | 300 | 23 | | SL, Brk 8 |
| 22 | 0939 | 32 | 28 | 300 | 32 | | GL, Brk 8 |
| 22 | 0946 | 24 | 19 | 300 | 6 | | GL, Brk 8 |
| 22 | 0951 | 16 | 12 | 300 | 2 | | PL, Brk 8 |
| 23 | 1003 | 68 | 64 | | 35 | | PL, Brk 8 Pull + end PT 22 |
| 23 | 1007 | 60 | 56 | 250 | 167 | | Start PT 23; Brk 8 |
| 23 | 1011 | 52 | 48 | 275 | 23 | | SL, Brk 8 |
| 23 | 1017 | 44 | 40 | 300 | 13 | | SL, Brk 8 |
| 23 | 1022 | 36 | 32 | 300 | 46 | | SL, Brk 8 |
| 23 | 1027 | 28 | 24 | 300 | 12 | | SL, Brk 8 |
| 23 | 1032 | 20 | 16 | 300 | 10 | | SL, Brk 8 |
| 23 | 1038 | 12 | 8 | 300 | 3 | | SL, Brk 8 |
| 23 | 1043 | 4 | 0 | 300 | 497 | 5.1 | PL, Pull + end PT 23 |
| 23 | 1048 | 0 | 0 | 300 | 497 | 8.2/10cy | 1.8 cy Ret, left @ 1100 |
| | | | | ave | | | |
| | | | | last 9 | | | |
| | | | | trucks | | | |
| | | | | (full trucks) | | | |

PT20
13.1

Q20
367
PT 23
571

4.

WOOD DESTROYING ORGANISM

Notice of Inspection
and/or Treatment

Wallace

27468

ASPEN
Pest Control, Inc.

LAKE CITY, FLORIDA

225 SW Louis Glen
property address

inspection date

2-3-09

treatment date - Full Treatment / Spot Treatment

Bifen X13.069
pesticide used

wood destroying organism treated

Aspen

PEST CONTROL, INC.

LAKE CITY, FLORIDA

HOME SERVICES

PEST - TERMITES - LAWNS

CALL 755-3611

P.O. Box 1795

Lake City, FL 32056

GEOHAZARDS, INC.

Permit #
27467

Professional Geological, Geophysical and Geotechnical Engineering Services

P.O. Box 14566
Gainesville, Florida 32604

Anthony F. Randazzo, Ph. D.
Geologist
Florida PG# 0003
Georgia PG#1136

David Bloomquist, Ph. D.
Geotechnical Engineer
Florida PE# 37235

Attila A. Bodo, P.E.
Structural Engineer
Florida PE# 15834

Douglas L. Smith, Ph.D.
Geophysicist
Florida PG# 0018
Georgia PG# 1140

GROUT PROCEDURE CERTIFICATION REPORT

Killin Residence
172 NW Kelly Lake Court
Lake City, Florida

December 5, 2008

Geohazards, Inc. Project No. 2008385B

Florida Farm Bureau Insurance
Claim No. 441215

Geotechnical Engineer:
David Bloomquist, PhD, PE
Florida License No. 37235

Onsite Representative:
Tammy Henry

Background

Compaction grouting was performed at the Killin Residence, 172 NW Kelly Lake Ct, Lake City, Florida by C&N Foundation Technologies, Inc. The objective was to stabilize the subsurface, thereby reducing the potential for future damage to the structure and surrounding appurtenances.

Geohazards, Inc. representative Tammy Henry monitored the grouting operation, which began on November 24, 2008, and concluded on December 5, 2008.

The grout pipe installation involved water injection drilling down and into competent limestone. This method inserts the grout casing as the point is drilled. A total of 23 grout

points were drilled requiring 1,696 linear feet of injection pipe. A Geohazards, Inc. monitor was not present during the grout pipe installation; therefore Geohazards, Inc. cannot confirm any observations or conclusions regarding details of the drilling effort.

Grouting Process

A crew of C&N Foundation Technologies, Inc. performed the pressure grouting operation which began at 10:41 AM on November 24, 2008. The automatic grout pump was connected to the injection pipe via a flexible hose. Grout pressures were monitored with an in-line pressure gauge. Grout was typically injected using a pump and pull technique that injected grout while the pipe was extracted over five-foot intervals via a hydraulic jack.



Grout delivery setup with piston pump

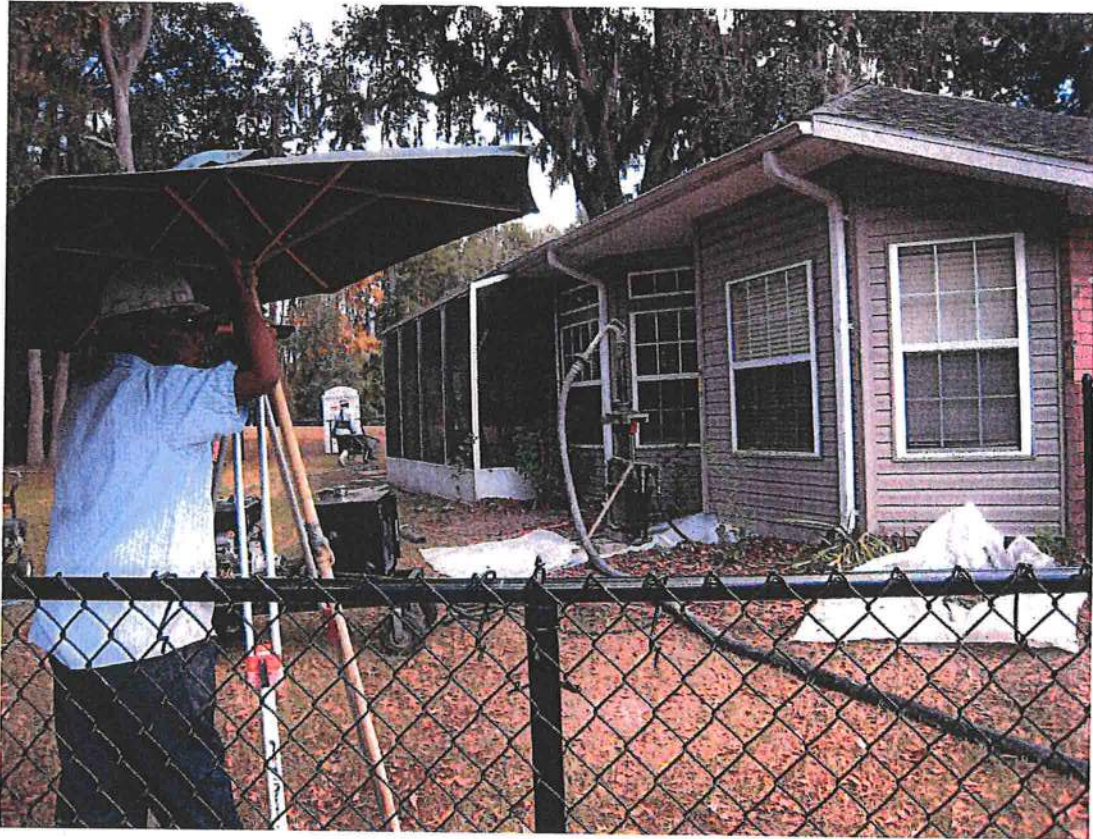


Injection pipe with the flexible hose connected to a hydraulic ram unit

The grout pumping process continued until one of the following events occurred:

- The grout line pressure exceeded 250 - 400 psi. This signifies that proper compaction of the soil at that specific depth was achieved.
- House movement, detected either by surveying transit or level. Movement of the structure also requires that the grouting be stopped at that location.
- Ground movement, detected either by surveying transit or level. Any movement of the ground (heave) requires that the grouting cease.
- Grout flows from the base of the pipe. Grouting ceased if grout was observed flowing from the base of the pipe injection point. This occurs if grout channels up the outside of the pipe.

For any of the above conditions, the contractor would subsequently raise the pipe between 4 and 8 feet and continue pumping. Grouting was terminated when grouting depths reached 12 feet or less below the surface.



Level to monitor structure movement

Another situation that requires cessation of pumping occurs when the pipe operator notices that excessive force is required to raise the grout pipe. This could result in the pipe breaking at a fitting. In order to prevent this occurrence, the contractor would stop grouting, pull the pipe up until the pulling force was reduced, and then resume pumping. This reduction in force usually occurs after pulling the pipe up two to four feet.

Observations

The depth to competent limestone varied at the site, ranging from 62 to 92 feet. Injection point 16 accepted the largest volume of grout, at 20.8 cubic yards (cy). Other injection points that accepted relatively large quantities were points 21 (16.7 cy) and 22 (13.1 cy). Injection point 18 accepted less than one cubic yard. Slight structural lift (less than 1/8") was observed at most points. These occurrences are noted in the field logs.

Heavy backflow at points 5, 6, and 10 necessitated raising the pipes twelve feet or more at various depths. Tight casing at point 8 necessitated raising the pipe twelve feet. These occasions are noted in the grout logs

There were no other anomalous instances observed during the grouting procedure.

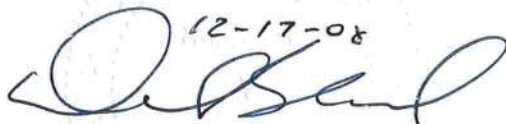
The grouting program was completed on December 5, 2008. The total grout delivered to the site was 170 cy. Trucks 5, 12, and 18 were returned to the batch plant with an unused load of 2.3, 1.5, and 1.8 cubic yards. Thus, 164.4 cy of grout was placed into the injection points. Complete grout logs are attached at the end of this report.

Conclusions

The figures cited in the table below represent our proposed estimate and the actual quantities used at the Killin residence grout remediation site. Based on the drill depths and the quantity of grout injected, at this time Geohazards, Inc. opines that the sinkhole conditions have been remediated. In addition, a review of the procedures employed by C&N Foundation Repair, Inc. indicates that the grouting operation was performed in accordance with the proposed Geohazards, Inc. program, technical specifications and foundation grouting industry practices.

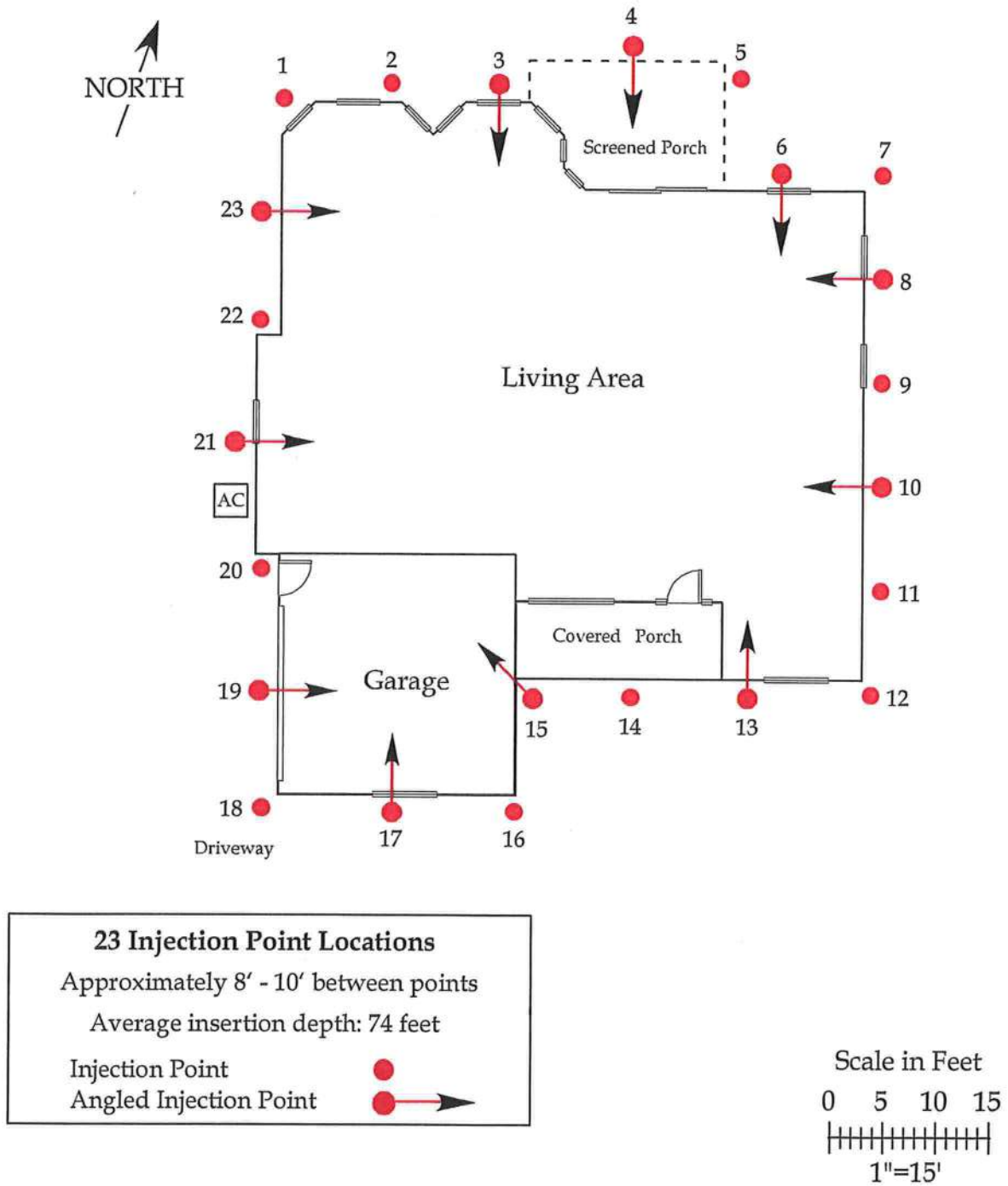
| ITEM NUMBER | ITEM | ESTIMATE | FINAL QUANTITY |
|-------------|-----------------------------|--------------|----------------|
| 1 | Linear feet of grout pipe | 2,070 lf | 1,696 lf |
| 2 | Cubic yards of grout pumped | 200 – 300 cy | 164.4 cy |

Respectfully submitted,

A handwritten signature in blue ink, appearing to read 'David Bloomquist', with the date '12-17-08' written above it.

David Bloomquist, PhD, PE
Geotechnical Engineer
Florida License No. 37235

Schematic of final grout locations at the Killin Residence, Lake City, Florida.



Final Grout Totals
Project: Killin Residence
Project Number: 2008385B

| Station | Depth (feet) | Grout Injected (cubic yards) | Injection Angle (° from vertical) |
|--|-----------------|---------------------------------|--------------------------------------|
| 1 | 78 | 10.8 | 0 |
| 2 | 75 | 10.7 | 0 |
| 3 | 62 | 1.8 | 16 |
| 4 | 64 | 1.3 | 12 |
| 5 | 92 | 11 | 0 |
| 6 | 72 | 8.6 | 12 |
| 7 | 66 | 1 | 0 |
| 8 | 78 | 9.7 | 15 |
| 9 | 86 | 1.2 | 0 |
| 10 | 90 | 4.9 | 18 |
| 11 | 66 | 7.3 | 0 |
| 12 | 74 | 3.7 | 0 |
| 13 | 90 | 7.2 | 14 |
| 14 | 62 | 7.2 | 0 |
| 15 | 68 | 4.6 | 13 |
| 16 | 84 | 20.8 | 0 |
| 17 | 65 | 1.4 | 12 |
| 18 | 66 | 0.9 | 0 |
| 19 | 64 | 2.5 | 14 |
| 20 | 78 | 12.9 | 0 |
| 21 | 76 | 16.7 | 16 |
| 22 | 72 | 13.1 | 0 |
| 23 | 68 | 5.1 | 19 |
| Totals | 1,696 ft | 164.4 cy | |
| Average Insertion Depth = 74 ft | | | |

Total Grout Delivered: 164.4 cy
Total Grout Returned: 5.6 cy
Total Grout Injected: 170 cy

ATTACHMENTS

Grout Logs

| | | | | | | | |
|--------------------------------------|------------|-------------------------|----------|---|--------------|-------|---|
| Project: Killin Residence 2008385 | | Date: November 24, 2008 | | Sheet of 1/10 | | | |
| Contractor: C+N Foundation Tech. | | Notes: 4" casings | | Instrument: Berger 80x | | | |
| Foreman: Kevin | | | | Pump: Putzmeister T240 (asked to turn brk 8 vs 12) | | | |
| Station: | Time: | Depth: | Pressure | Strokes | Grout Placed | Slump | Observations |
| | Start Stop | From To | | | | | |
| 4 | 1041 1043 | 64 56 | 300+ | 21 | 0.3 | 5 | T1 @ 1035, start PT 4; HP, Brk 12 |
| 4 | 1048 1049 | 52 48 | 300+ | 8 | 0.1 | 5 | HP, Brk 8 |
| 4 | 1053 1054 | 44 40 | 300+ | 9 | 0.1 | 5 | HP, Brk 8 |
| 4 | 1059 1101 | 36 32 | 300+ | 23 | 0.1 | 5 | HP, Brk 8 |
| 4 | 1106 1107 | 28 24 | 300+ | 11 | 0.2 | 5 | HP, Brk 8 |
| 4 | 1111 1112 | 20 16 | 300+ | 5 | 0.1 | 5 | HP, Brk 8 |
| 4 | 1116 1116 | 12 10 | 300+ | 3 | 1.3 | 5 | HP, Brk 8 Pull + end PT 4 |
| 5 | 1130 1132 | 90 86 | 300+ | 37 | 0.2 | 5 | start PT 5 HP, Brk 8 |
| 5 | 1136 1137 | 82 78 | 300+ | 7 | 0.1 | 5 | HP, Brk 8 |
| 5 | 1140 1142 | 74 70 | 300+ | 30 | 0.3 | 5 | HP, Brk 8 |
| 5 | 1144 1149 | 66 62 | 300+ | 11 | 1.8 | 5 | HP, Brk 8 BF Brk 4 |
| 5 | 1155 1158 | 60 54 | 300+ | 54 | 0.8 | 5 | HP, Brk 8, BF |
| 5 | 1202 1200 | 52 50 | 300+ | 310 | 8.7 | 5 | T1 empty, Flush, 2 |
| 5 | 1309 1312 | 52 48 | 200+ | 56 | 10/10cy | 5 | Grout Returned, left @ 1226 |
| 5 | 1317 1317 | 44 40 | 200+ | 10 | 0.3 | 5 | T2 @ 1303, HP, Brk 8 |
| 5 | 1322 1325 | 36 32 | 200+ | 54 | 0.3 | 5 | HP, Brk 8 |
| 5 | 1331 1332 | 28 24 | 200+ | 6 | 0.1 | 5 | HP, Brk 8, BF |
| 5 | 1336 1337 | 20 16 | 200+ | 7 | 0.1 | 5 | HP, Brk 8 |
| 5 | 1340 1340 | 12 10 | 200 | 7 | 0.1 | 5 | GT 5, Brk 8 |
| 6 | 1349 1357 | 72 70 | 200 | 169 | 2.7 | 5 | GT 5, SL, Pull + end PT 5 (asked to backflow) |
| | | | | 309 | 5/5cy | | T2 empty, Flush Brk 8 |
| | | | | | | | Grout Returned, left @ 1410 |
| | | | | | | | Plant closing @ 3, needed to be done prior |
| | | | | | | | - end day - |

PT 4 = 1.3

PT 5 = 1.1cy

backflow
not

[illegible]

| Project: Killin Residence | | Date: Nov. 26, 2008 | | Sheet 3/10 | | | | |
|-----------------------------------|-------|---------------------|--------|------------------------|---------|--------------|-------|---------------------------------|
| Contractor: C+N Foundations Tech. | | Notes: | | Instrument: Berger 20X | | | | |
| Foreman: Jose | | Notes: | | Pump: Putzmeister TK40 | | | | |
| Station: | Time: | | Depth: | Pressure | Strokes | Grout Placed | Slump | Observations |
| | Start | Stop | | | | | | |
| 6 | 0838 | 0840 | 34 | 30 | 36 | | 5 | T5 @ D812, Cont PT 8; HP, Brk 8 |
| 6 | 0844 | 0844 | 26 | 21 | 2 | | 5 | PL; Brk 8 |
| 6 | 0847 | 0847 | 18 | 12 | 2 | 40 / 0.6 | 5 | PL; GTS, Pull end PT 8 |
| 7 | 0908 | 0904 | 66 | 62 | 16 | | 5 | Start PT 6; HP, Brk 8 |
| 7 | 0908 | 0908 | 58 | 54 | 8 | | 5 | HP, Brk 8 |
| 7 | 0912 | 0913 | 50 | 46 | 5 | | 5 | HP, Brk 8 |
| 7 | 0915 | 0916 | 42 | 38 | 7 | | 5 | HP, Brk 8 |
| 7 | 0920 | 0920 | 34 | 30 | 6 | | 5 | HP, Brk 8 |
| 7 | 0925 | 0926 | 26 | 22 | 15 | | 5 | HP, Brk 8 (BF) |
| 7 | 0931 | 0931 | 18 | 14 | 6 | 6 / 1.0 | 5 | GTS, Pull end PT 7 |
| 10 | 0951 | 0952 | 90 | 86 | 24 | | 5 | Start PT 10; HP, Brk 8 |
| 10 | 0956 | 0957 | 82 | 78 | 9 | | 5 | HP, Brk 8 |
| 10 | 1000 | 1002 | 74 | 70 | 10 | | 5 | HP, Brk 8 |
| 10 | 1005 | 1006 | 66 | 62 | 12 | | 5 | HP, Brk 8 |
| 10 | 1010 | 1012 | 58 | 54 | 14 | | 5 | HP, Brk 8 |
| 10 | 1015 | 1018 | 50 | 46 | 14 | | 5 | HP, Brk 8 (BF) |
| 10 | 1030 | 1033 | 38 | 34 | 55 | | 5 | HP, Brk 8 (BF) |
| 10 | 1037 | 1039 | 30 | 26 | 26 | | 5 | HP, Brk 8 (BF) |
| 10 | 1043 | 1044 | 22 | 18 | 16 | | 5 | HP, Brk 8 (BF) |
| 10 | 1047 | 1047 | 14 | 12 | 2 | 310 / 4.9 | 5 | GTS, Pull end PT 10 |
| 9 | 1059 | 1101 | 86 | 82 | 11 | | 5 | HP, Brk 8 |
| 9 | 1105 | 1106 | 78 | 74 | 11 | | 5 | HP, Brk 8 |
| 9 | 1111 | 1113 | 70 | 66 | 6 | | 5 | HP, Brk 8 |
| 9 | 1119 | 1120 | 62 | 58 | 4 | | 5 | HP, Brk 8 |
| 9 | 1124 | 1125 | 54 | 50 | 3 | | 5 | HP, Brk 8 |
| 9 | 1130 | 1131 | 46 | 42 | 4 | | 5 | HP, Brk 8 |
| 9 | 1135 | 1136 | 38 | 34 | 5 | | 5 | HP, Brk 8 |
| 9 | 1142 | 1143 | 30 | 26 | 4 | | 5 | HP, Brk 8 |
| 9 | 1149 | 1150 | 22 | 16 | 4 | 74 / 1.2 | 5 | HP, Pull end PT 9 |

487 77/1004

2, Bay Rot, TS left @ 1200

—enday—

| | | | | | | | |
|--------------------------------------|---------------------------------------|--|------------------|---------|-----------------|-------|-----------------------------------|
| Project: Killin Residence 2008385 | Date: December 1 st , 2008 | Sheet of | 4/10 | | | | |
| Contractor: C&N Foreman: Jose | Notes: | Instrument: CST Berger box Pump: Patzmeister TK40 | | | | | |
| Station: | Time: | Depth: | Pressure | Strokes | Grout Placed | Slump | Observations |
| 11 | Start 1135 Stop 1144 | From 66 To 62 | 300 ⁺ | 165 | | | TG @ 1130, Start PT 11; HP, Brk 8 |
| 11 | 1146 1152 | 58 54 | 300 ⁺ | 147 | | | HP, Brk 8 (BF) |
| 11 | 1156 1157 | 50 46 | 300 ⁺ | 27 | | | HP, Brk 8 |
| 11 | 1200 1201 | 42 38 | 300 ⁺ | 12 | | | HP, Brk 8 |
| 11 | 1203 1205 | 34 30 | 300 ⁺ | 31 | | | HP, Brk 8 |
| 11 | 1208 1211 | 28 24 | 275 ⁺ | 24 | | | GTS, Brk 8 |
| 11 | 1216 1217 | 20 16 | 300 | 14 | 400 / 7.3 | | GTS Pull end PT 11 |
| 13 | 1235 1236 | 90 86 | 300 ⁺ | 25 | | | Start PT 13, HP, Brk 8 |
| 13 | 1238 1240 | 82 78 | 300 ⁺ | 8 | | | HP, Brk 8 |
| 13 | 1242 1243 | 74 70 | 300 ⁺ | 12 | | | HP, Brk 8 |
| 13 | 1248 1250 | 68 64 | 300 ⁺ | 64 | | | HP, Brk 8 (BF) |
| 13 | 1257 1259 | 60 60 | 275 | 50 | 150 / 2.7 | | TG empty, Flush |
| 13 | 1353 1354 | 60 56 | 300 ⁺ | 579 | 10/100g | | 8 cy Ret, TG left @ 1310 |
| 13 | 1358 1359 | 52 48 | 300 ⁺ | 36 | | | T7 @ 1342, HP, Brk 8 |
| 13 | 1403 1409 | 44 40 | 250 ⁺ | 4 | | | HP, Brk 8 |
| 13 | 1415 1419 | 36 32 | 275 ⁺ | 125 | | | HP, Brk 8 |
| 13 | 1425 1429 | 28 24 | 275 ⁺ | 73 | | | HP, Brk 8 ((rock 4" diam)) |
| 13 | 1433 1433 | 20 16 | 275 ⁺ | 36 | | | HP, Brk 8 |
| 15 | 1447 1449 | 68 64 | 300 ⁺ | 4 | 278 / 4.5 | | HP, Pull end PT 13 |
| 15 | 1452 1453 | 60 56 | 300 ⁺ | 23 | | | HP, Brk 8 |
| 15 | 1456 1457 | 52 48 | 300 ⁺ | 11 | | | HP, Brk 8 |
| 15 | 1501 1505 | 44 40 | 300 ⁺ | 27 | | | HP, Brk 8 |
| 15 | 1510 1516 | 36 32 | 300 ⁺ | 60 | | | HP, Brk 8 |
| 15 | 1520 1522 | 28 24 | 275 | 128 | | | SL, Brk 8 |
| 15 | 1529 1530 | 20 16 | 275 | 25 | 284 / 4.6 | | SL, Brk 8 |
| 12 | 1546 1551 | 74 74 | 300 | 10 | 284 / 4.6 | | SL, Pull end PT 15 |
| | | | 250 | 57 | 619 / 10/100g | | T7 empty, Flush |
| | | | | 619 | | | 8 cy Ret, left @ 1600 |
| | | | | | | | 1 - end day - |

PT 11 = 7.3

PT 13 = 7.2

PT 15 = 4.6

[illegible]

| Project: Killin Residence 2008385 | | | Date: Dec. 3, 2008 | | Sheet of 6/10 | | | | |
|--------------------------------------|-------|------|--------------------|----|------------------------|---------|-----------------|-------|-------------------------------|
| Contractor: C+N | | | Notes: | | Instrument: Berger 20X | | | | |
| Foreman: JOSE | | | | | Pump: Putzmeister TK40 | | | | |
| Station: | Time: | | Depth: | | Pressure | Strokes | Grout Placed | Slump | Observations |
| | Start | Stop | From | To | | | | | |
| 16 | 0844 | 0845 | 2440 | 28 | 300+ | 12 | | 5 | T11 @ 35, Cont @ 16, HP, Brk8 |
| 16 | 0849 | 0851 | 24 | 20 | 275+ | 33 | | 5 | HP, Brk8 |
| 16 | 0855 | 0856 | 16 | 14 | 300 | 16 | 51 / 0.8 | 5 | GL, Pull + end RT 16 |
| 18 | 0920 | 0923 | 66 | 62 | 300+ | 15 | | 5 | PL, HP, Brk8 (Stacked PT 18) |
| 18 | 0926 | 0927 | 58 | 54 | 300+ | 7 | | 5 | HP, Brk8 |
| 18 | 0931 | 0932 | 50 | 46 | 300+ | 6 | | 5 | HP, PL, Brk8 |
| 18 | 0936 | 0936 | 42 | 38 | 300+ | 2 | | 5 | PL, Brk8 |
| 18 | 0941 | 0942 | 34 | 30 | 300+ | 15 | | 5 | HP, Brk8 |
| 18 | 0945 | 0947 | 26 | 22 | 300+ | 10 | | 5 | HP, Brk8 |
| 18 | 0956 | 0957 | 18 | 18 | 300 | 2 | 57 / 6.9 | 5 | PL, Pull + end RT 18 |
| 17 | 1010 | 1012 | 65 | 61 | 275+ | 31 | | 5 | HP, Brk8 (Stacked PT 17) |
| 17 | 1017 | 1017 | 57 | 53 | 300+ | 8 | | 5 | HP, Brk8 |
| 17 | 1021 | 1021 | 49 | 45 | 300+ | 9 | | 5 | HP, Brk8 |
| 17 | 1026 | 1027 | 41 | 37 | 300+ | 10 | | 5 | HP, Brk8 |
| 17 | 1031 | 1032 | 33 | 29 | 300+ | 14 | | 5 | HP, Brk8 |
| 17 | 1036 | 1037 | 25 | 21 | 300+ | 7 | | 5 | PL, HP, Brk8 |
| 17 | 1041 | 1041 | 17 | 13 | 300 | 14 | 83 / 1.8 | 5 | GL, Pull + end PT 17 |
| 20 | 1105 | 1107 | 78 | 74 | 250+ | 34 | | 5 | Start PT 20, HP, Brk8 |
| 20 | 1113 | 1121 | 70 | 66 | 275 | 168 | | 5 | HP, Brk8 4 |
| 20 | 1125 | 1136 | 66 | 66 | | 224 | 230 / 6.9 | 5 | T11 Empty, Flush |
| 20 | | | 54 | | | 617 | 10 / 100y | | Occy Refused, Ref @ 1150 |
| 20 | 1312 | 1325 | 66 | 62 | 275-300 | 283 | | | T12 @ 1305; GL, Brk8 |
| 20 | 1331 | 1332 | 58 | 54 | 300+ | 21 | 203 | 5 | HP, Brk8 |
| 20 | 1337 | 1339 | 50 | 46 | 300+ | 10 | 211 | 5 | HP, Brk8 |
| 20 | 1343 | 1345 | 42 | 38 | 300+ | 18 | 225 | 5 | HP, Brk8 |
| 20 | 1352 | 1353 | 34 | 30 | 300+ | 9 | 230 | 5 | HP, Brk8 |
| 20 | 1359 | 1403 | 26 | 22 | 300+ | 8 | 245 | 5 | HP, Brk8 |
| 20 | 1410 | 1411 | 18 | 14 | 300+ | 4 | 359 / 6.0 | 5 | HP, Pull + end PT 20 |
| see next → | | | | | | | | | |

see next →

232

6

PT 16
20

PT 18
20

PT 17
14

PT 20
13.6

[illegible]

| | | | | | | | |
|--------------------------------------|------------------------------|----------------------------|----------|---------|-----------------|-------|------------------------------------|
| Project: Killin Residence 2068385 | Date: Thurs. Dec. 4, 2008 | Sheet of 8/10 | | | | | |
| Contractor: C+N | Notes: | Instrument: CST Berops 20X | | | | | |
| Foreman: Jose | | Pump: Putnam's TK 40 | | | | | |
| Station: | Time: | Depth: | Pressure | Strokes | Grout Placed | Slump | Observations |
| | Start | From | To | | | | |
| 21 | 0838 | 76' | 72 | 250* | 210 | 5 | T13 @ 0815, start PT 21; HP; Brk 8 |
| 21 | 0853 | 68 | 64 | 250* | 191 | 5 | HP, Brk 8 |
| 21 | 0909 | 60 | 60 | 275 | 218 | 5 | T13 empty, Flush |
| 21 | 1025 | 60 | 56 | 275* | 619 | 5 | OCy Returned, left @ 0936 |
| 21 | 1033 | 52 | 48 | 300* | 20 | 5 | T14 @ 1018, HP; BF Brk 8 |
| 21 | 1042 | 44 | 41 | 250 | 142 | 5 | HP, Brk 8 |
| 21 | 1054 | 36 | 33 | 300 | 107 | 5 | SL, Brk 8 |
| 21 | 1105 | 28 | 25 | 250 | 15 | 5 | SL, Brk 8 |
| 21 | 1111 | 20 | 16 | 250 | 3 | 5 | PL, Brk 8 |
| 21 | 1116 | 12 | 12 | 200 | 2 | 5 | OTS, Pull + end PT 21 |
| 1 | 1133 | 78 | 78 | 250 | 218 | 5 | +14 empty, Flush |
| 1 | 1239 | 78 | 73 | 250* | 614 | 5 | OCy Ret, left @ 1153 |
| 1 | 1257 | 70 | 66 | 275 | 270 | 5 | T15 @ 1234; TC, Brk 8 |
| 1 | 1307 | 62 | 58 | 275 | 77 | 5 | GL, Brk 8 |
| 1 | 1313 | 54 | 50 | 275 | 29 | 5 | GL, Brk 8 |
| 1 | 1317 | 46 | 42 | 300* | 23 | 5 | GL, Brk 8 |
| 1 | 1322 | 38 | 34 | 300* | 13 | 5 | HP, Brk 8 |
| 1 | 1327 | 30 | 26 | 300 | 14 | 5 | HP, Brk 8 |
| 1 | 1333 | 22 | 18 | 300* | 32 | 5 | GL, Brk 8 |
| 1 | 1339 | 14 | 10 | 300 | 9 | 5 | GL, Brk 8 |
| 2 | 1350 | 75' | 73 | 250 | 2 | 5 | PL, Pull + end PT 1 |
| 2 | 1506 | 75' | 71 | 275 | 155 | 5 | Start PT 2; T15 empty, Flush |
| 2 | 1528 | 67 | 63 | 300* | 624 | 5 | OCy Ret, left @ 1409 |
| 2 | 1532 | 59 | 55 | 300* | 401 | 5 | T16 @ 1456, GL, Brk 8 |
| 2 | 1536 | 51 | 47 | 300* | 11 | 5 | HP, Brk 8 |
| 2 | 1541 | 43 | 39 | 300* | 20 | 5 | HP, Brk 8 |
| 2 | 1541 | 43 | 39 | 300* | 20 | 5 | HP, Brk 8 |

See next sheet →

[illegible]

PT28
i3.1

220
367
PT 23
571

4.